Flap-Lag Stability Data for a Small-Scale Isolated Hingeless Rotor in Forward Flight

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April 1989



National Aeronautics and Space Administration

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SUMMARY

An isolated, hingeless rotor with discrete flap and lead-lag flexures and relatively rigid blades was tested in the Aeroflightdynamics Directorate's 7- by 10-Foot Wind Tunnel. The purpose of the test was to determine experimentally the lead-lag stability of a structurally simple rotor configuration in forward flight. The model tested had no cyclic pitch control, and was therefore operated untrimmed at several collective pitch angles, at shaft angles from 0° to -20° , and at advance ratios as high as 0.55. Two inplane natural frequencies, 0.61/rev and 0.72/rev, were tested for configurations both with and without structural flaplag coupling. Concomitant hover testing of the model was also conducted. Representative plots of the frequency and damping data are presented to show general trends, and complete tabular data and model properties information are included for use in detailed correlation studies. The most prominent feature of the forward flight data is an abrupt increase in damping with advance ratio at certain high-speed, high shaft-angle conditions, with high flapping loads. The hover data are consistent with previous experimental and theoretical results for hingeless rotors without kinematic couplings. Overall, the data quality is very good and the data are expected to be useful in the development and validation of rotor aeroelastic stability analyses.

NOMENCLATURE

B.S.	blade station, from center of rotation, in.
c_d	airfoil drag coefficient
c_{l}	airfoil lift coefficient
α	airfoil angle-of-attack, to chord line, rad
α_s	rotor shaft angle, negative for forward tilt, deg
μ	advance ratio
σ	damping exponent, 1/sec
$ heta_0$	blade collective pitch angle, to chord line, deg
ω	natural frequency, Hz
Ω	rotor speed, rpm

INTRODUCTION

The general problem of predicting rotorcraft aeromechanical and aeroelastic stability encompasses an array of analytical challenges. Structural dynamic complications include significant geometric nonlinearities, geometric stiffness, coupling between the rotor and the

nonrotating system, configurations with redundant load paths, and the widespread use of composite and elastomeric materials. Aerodynamic complications include rotor wake effects, nonlinear airfoil effects, transonic flows, and rotor-body aerodynamic interactions; all of which are, for the stability question, unsteady phenomena, and all of which may exist both in hover and forward flight. An additional complication whose importance promises to increase in the future is the effect of active controls. Developing an analysis which will accurately deal with all of these effects for an arbitrary rotorcraft configuration at any operating condition is a formidable task.

Specialized investigations of simple configurations and restricted flight conditions can emphasize the effects of one complicating factor and minimize the effects of others. For such cases, systematically comparing the results of various analyses with appropriate experimental data sets can give insights into the fundamental dynamic behavior of rotorcraft, as well as expose the specific strengths and weaknesses of the analyses. A number of such investigations have been conducted, and cases for which experimental data are available include: an isolated (i.e., the hub is fixed rigidly in space) torsionally soft elastic blade both in a vacuum (ref. 1), and in hover (ref. 2); an isolated hingeless rotor with rigid blades, flap- and lead-lag degrees of freedom, and various aeroelastic couplings in hover (refs. 3 and 4); a coupled hingeless rotor-body with rigid blades and discrete flap and lead-lag flexures, both under simulated vacuum conditions and in hover (ref. 5); and a simple isolated bearingless rotor in hover (ref. 6).

None of the investigations above deals with the effects of forward flight; the present work was intended to examine this area. Theoretical work has indicated that forward flight can have large effects on blade flap-lag stability (refs. 7 and 8), but a lack of experimental data has hampered the validation and refinement of those results. Coupled rotor-body stability data in forward flight are available (ref. 9), but isolated rotor flap-lag stability data are lacking. Although rotor-body testing more closely represents actual rotorcraft in flight, isolated rotor studies are probably even more valuable for examining the effects of forward flight because there are no body coupling effects present to obscure the results. Rotor-body coupling is a relatively tractable problem which can be dealt with separately. The primary objective of the research reported here was to obtain a set of isolated rotor flap-lag stability data in forward flight for correlation with existing and future analyses. Whereas all of the isolated rotor tests referred to above used two-bladed rotors, for this experiment a three-bladed rotor was chosen, in part so that the role of dynamic inflow (ref. 10) in isolated rotor flap-lag stability could be assessed.

This report presents an extensive set of experimental aeroelastic stability data and supporting documentation for the specialized case of an isolated rotor in forward flight. The model tested was a three-bladed, soft-inplane, hingeless rotor with discrete flap and lead-lag flexures and relatively rigid blades. The model structural configuration and control system were kept as simple as possible to more effectively isolate the effects of forward flight aerodynamics on lead-lag damping. The test was conducted in the Aeroflightdynamics Directorate's 7- by 10-Foot Low Speed Wind Tunnel at Ames Research Center. Two nominally identical rotor models were tested, Rotor I and Rotor II. Rotor I was tested extensively in hover, and

then tested in forward flight up to very high flapping conditions at a single rotor speed and a single collective pitch angle. When the flexures of Rotor I exceeded their fatigue life, a second set of flap and lead-lag flexures was installed with the blades on the hub, which gave Rotor II. Although Rotors I and II were identical in design, due to manufacturing differences the flap and lead-lag flexures of Rotor II gave slightly different fundamental frequencies than did Rotor I. Rotor II was tested in forward flight at two rotor speeds, and three collective pitch angles, both with and without structural flap-lag coupling, but it was restricted to less extreme flapping conditions than Rotor I. Only limited hover testing was conducted with Rotor II. Although the differences between Rotor I and Rotor II data are quite small for otherwise identical conditions, the rotor used is specified for each datum presented. Some of the data presented here have previously been published and compared to analytical predictions of lead-lag damping based on both linear (ref. 11) and nonlinear (ref. 12) quasi-steady aerodynamic theories.

This data report describes the model, instrumentation, test procedures, and data analysis techniques used for the experiment; presents representative plots of the data obtained; and includes complete tabulations of the data for use in future correlations with analyses.

EXPERIMENT DESCRIPTION

Model Description

A photograph of the rotor hub and blades installed on the model is shown in figure 1. Considerable analytical research has been conducted using the simplifying representation of a hingeless rotor as a set of rigid blades with offset, coincident, spring-restrained flap and lead-lag hinges, (ref. 7); the model tested was designed to closely approach this simple analytical idealization. To accomplish this the model used lead-lag and flap flexures, shown in an exploded-view drawing in figure 2. Two stiff "side beams" attached the outboard end of the single element lead-lag flexure to the inboard end of the double-element flap flexure so that the lead-lag and flap flexural we's were both centered at 11% of the rotor radius. The flap flexure was very stiff in the lead-lag direction and the lead-lag flexure was very stiff in the flap direction. Both flexures were designed to be as stiff as possible in torsion so as to minimize elastic pitch motion inboard of the blade root. The measured torsional stiffness of the flexure assembly was 215 in-lbs/radian, which gave a nonrotating fundamental blade-torsion frequency of 149 Hz. This value is equal to 9/rev at the highest rotor speed tested.

The model had no cyclic pitch control, and the collective pitch angle was set manually prior to operation. This resulted in trim conditions with unrestricted cyclic flapping, and which satisfied no particular force and moment requirements. Rotor flapping flexure strain allowables determined the limits of the shaft angle versus advance ratio test envelope at a given collective pitch. While these are not normal rotorcraft operating conditions, they do

represent well defined and challenging conditions for analytical validation and development exercises. Eliminating the swashplate and pitch bearings minimizes control slop and friction damping, which allows higher quality model-scale dynamic data to be obtained than would be possible otherwise.

The model incorporated means for varying the amount of structural coupling between the flap and lead-lag motions of the blade, an important factor in hingeless rotor aeroelastic stability (ref. 3). This was accomplished by setting the collective pitch either by rotating the blade relative to the blade socket, giving essentially no flap-lag structural coupling, or by rotating the entire flexure assembly and the blade along with it, relative to the hub adaptor, giving full flap-lag structural coupling. These two possible pitch-change locations are identified in figure 2. The flexure-blade assemblies were mounted to the hub so that, when the flap and lead-lag angles were zero, the line along the blade quarter-chord was normal to the rotor shaft and passed through its center.

Figure 3 shows the details of the blade planform and cross section. The blades were composed of stiff Kevlar spars with tantalum leading edge weights for chordwise mass balance, balsa wood cores, fiberglass reinforcement at the trailing edges, and fiberglass overwraps for torsional stiffness. The blades were untwisted and untapered, with the root cutout at 18.6% and the NACA 23012 airfoil section beginning at 24.8% of the radius and continuing to the tip. The elastic axis, pitch axis, and axis of section mass centers were all located at the quarter chord. The blades were much stiffer than the flexures in both the flap and lead-lag directions so that rigid-body blade motions about the flexures would accurately represent the rotor's fundamental flap and lead-lag modes. With the blade root socket clamped to a backstop, the first flap and lead-lag frequencies of the blades alone were measured as 9.5 and 33 Hz, respectively, and the second flap frequency was 59 Hz. The first torsion frequency of the blade without flexures was estimated to be greater than 200 Hz.

Previous model-rotor testing experience has shown that even relatively small differences in properties from one blade to another can result in very poor data quality in isolated blade stability tests of rotors with three or more blades. This problem was dealt with by very carefully matching the blade inertias and flexure stiffness to each other. Before being instrumented, the flexures for each rotor were honed by hand so that they all had the same flap and the same lead-lag frequencies when each was mounted with the same blade. Then, after the flexures were instrumented, a small variable tip mass in each blade, located on the quarter chord, (see fig. 3) was adjusted so that each flexure-blade assembly had the same lead-lag frequency as the others. The result was that with the model installed in the wind tunnel the maximum nonrotating frequency difference between blades was approximately 0.5%. Reference 13 examines the effects of blade-to-blade dissimilarities.

The principal geometric properties of the rotor and mass and stiffness properties suitable for use in rigid blade analyses are given in table 1. The values given are all measured, except for the torsional inertia and the flap and lead-lag inertia. The torsional inertia was computed from the measured torsional frequency and the measured stiffness. The flap and lead-lag inertia was calculated from the blade and flexure mass distribution. The given mass

properties include only the mass outboard of the center of the flapping flexure; no lead-lag flexure or side beam mass is included. The nonrotating frequency values in table 1 are the most reliable measurements of the set; it is therefore suggested that analysts adjust the flap and lead-lag flexure stiffnesses as needed to yield the given frequencies. The flap and lead-lag frequency differences between Rotor I to Rotor II are caused by variations in the manufacturing process. These frequency differences could be due to variations in the flexure web thicknesses of less than 0.001 inches. The change in nonrotating flap damping from Rotor I to Rotor II results from a change in the way the instrumentation leads were routed off the flexures. In general, the nonrotating damping measurements were quite variable, ranging from -0.070 to -0.120 for the lead-lag mode, dependent primarily on the amplitude of the excitation; the values given are averages for excitation levels typical of those used when the rotor was operating.

An exploded view of the flexure and blade assembly has been included as figure 2. Figures 4 through 6 show the details of the lead-lag flexures, the side beams, and the flap flexures, respectively. These drawings and material properties from reference 14 were used to calculate the running mass per unit length, torsional inertia per unit length, flap bending stiffness, lead-lag bending stiffness, and torsional stiffness for each of these components. The results are given in tables 2 through 4. The given torsional stiffness values include the effects of warping restraint at both ends of the thin webs of the flap and lead-lag flexures. The radial distributions of these properties for the blade, including the root socket, were taken from reference 15 and are included here as table 5.

Because actual lift and drag data for the NACA 23012 airfoil is unavailable at the low Reynolds numbers appropriate for a small-scale, low tip-speed test, steady-bending-moment data from a test with the same blades used in the present test has been used to estimate the airfoil characteristics (Bousman, William G., The Effects of Structural Flap-Lag and Pitch-Lag Coupling on Soft Inplane Hingeless Rotor Stability in Hover, NASA Technical Paper, to be published). The results are

$$c_d = 0.0079 + 1.7\alpha^2$$

 $c_l = 0.15 + 5.73\alpha$

These results apply for positive angles-of-attack below stall, and may be useful for correlations with the hover results of the present test. The forward flight conditions of the present test, however, often involve large negative angles-of-attack over significant portions of the rotor disk, and so the expressions above are less useful. Instead, published airfoil data for higher Reynolds numbers might be used, perhaps corrected for low Reynolds number effects.

A photograph of the model installed in the Aeroflightdynamics Directorate's 7- by 10-Foot Wind Tunnel is shown in figure 7. Side- and front-view diagrams of the installation are shown in figure 8. The rotor stand included a gimbal which allowed the upper stand, enclosed by the fuselage fairing, to roll relative to the lower stand. This roll motion results in lateral translation of the rotor hub which excites the blades' lead-lag motion. A push rod and an arm extending from the side of the upper stand connected it to a 50-lb electromechanical shaker, located next to the base of the lower stand, which could drive the gimbal roll motion. The gimbal motion could be locked out by a hydraulic brake. The stand and shaker were mounted on a base plate located under the tunnel floor. The base plate was attached to the wind tunnel structure by a hinge at the front and an electric actuator at the rear which could pitch the entire assembly forward, thereby controlling the rotor shaft angle. Shaft angles from 0° to -20° could be obtained. At a given collective pitch angle, rotor speed, and advance ratio, varying the shaft angle was the only means available to control the rotor loads. With the shaft vertical, the rotor plane was 38 inches above the wind tunnel floor.

The rotor stand was designed to be as stiff as possible so that the rotor dynamic data would be representative of isolated rotor results. The lowest natural frequency of the stand, with the brake locking out the roll gimbal, was found to be about 25 Hz. This is nearly four times greater than the rotor lead-lag regressing mode frequency at 1000 rpm, but is slightly less than the lead-lag progressing mode frequency at that rotor speed.

Instrumentation

For each blade, the flap and lead-lag bending moments at the flexure center were measured with strain gage bridges. Each flap flexure was also instrumented with a torsion moment bridge at the outboard end of the web. For Rotor II additional flap and chord bridges were installed at the inboard and outboard extremes of the webs of one flexure set so that the bending moment distributions could be monitored. These signals were routed from the rotor hub through a slip ring to the nonrotating system. A Hall-effect 1/rev sensor was used to determine the rotor speed and establish a blade azimuth reference. A 60/rev signal was also used to give the rotor operator a continuously updated rotor speed measurement. The wind tunnel dynamic pressure and the rotor shaft angle were also measured with standard instruments. Accelerometers were also installed in both the fixed and rotating systems to help resolve any uncertainties that might arise regarding rotor-body coupling.

The signals from the strain gages, accelerometers, 1/rev sensor, and, for Rotor II, the dynamic pressure and shaft angle transducers were low-pass filtered to 50 Hz for anti-aliasing, amplified, and then digitized by a computer controlled data aquisition system. For Rotor I data, the shaft angle and dynamic pressure were simply recorded manually. The strain gage signals were also displayed on oscilloscopes so that rotor loads could be continuously monitored.

Test Procedures

The pitch of each blade was set with the aid of a small bubble level before each run. Small adjustments to the pitch of each blade were then made until the rotor tracked at the

operating rotor speed in hover. In general, the track did not depend on the rotor speed, but it did deteriorate with increasing advance ratio. After the rotor was established at operating speed, the wind tunnel was started and the dynamic pressure increased to give the desired advance ratio. The rotor shaft angle was adjusted as needed to control the rotor loads during the process. With the rotor and wind tunnel stabilized at the test condition, the hydraulic gimbal brake was released and the shaker used to drive the upper stand in roll at the appropriate fixed system rotor lead-lag frequency, progressing or regressing as desired. When sufficient excitation was evident on the oscilloscope displays of the lead-lag bending gages, the shaker was stopped, the brake engaged to lock up the upper stand, and the data aquisition system triggered to record the ensuing transient. At least two separate records were taken at each test condition so that the repeatability of the measurements could be assessed. A total of over 2000 damping measurements were made.

Data Analysis

Each record consisted of 5.12 seconds of data, digitized at a sample rate of 100 Hz. The multiblade coordinate transform was then used to transform the recorded individual blade signals to the nonrotating system, using azimuth information from the 1/rev signal. The resulting multiblade sine or cosine lead-lag coordinate time history was then analyzed with spectral and moving-block techniques (ref. 16) to determine the frequency and damping of the progressing or regressing lead-lag mode. The details of the implementation of these analyses are described in reference 17. While the analyses could have been performed on any of the individual lead-lag signals, the use of the transformed signals generally resulted in a higher signal-to-noise ratio, and it clearly separated the rotor regressing and progressing modes from each other. The importance of this separation will be discussed below.

RESULTS

The set of lead-lag regressing mode frequency and damping data obtained in forward flight is the primary result of this investigaton. Data were also obtained in hover.

Hover

The collective pitches and rotor speeds that define the hover test points are shown in figures 9(a) and (b), for the configurations with and without structural flap-lag coupling, respectively. Complete tabulations of the regressing lead-lag mode stability data in hover are given in table 6 for the configuration without structural coupling and in table 7 for the configuration with structural coupling. The identifying number of the rotor tested, collective pitch, rotor speed, shaft angle, and an identifying data point number are given along with the measured regressing-mode frequency and damping. Each table is sorted by increasing

collective pitch and rotor speed, decreasing shaft angle, and increasing rotor number. At zero collective pitch the two rotor configurations are identical, so some data points are included in both tables 6 and 7.

The fixed system lead-lag frequencies and damping values at zero collective pitch are plotted as a function of rotor speed in figure 10. The 2/rev frequency separation between the progressing and regressing modes is as expected for isolated rotor data. The small difference in nonrotating frequency between Rotor I and Rotor II is the cause of the consistent spread in the regressing mode frequency data, but for each rotor the actual data scatter is practically zero. For a truly isolated rotor, any differences in damping between the progressing and regressing mode results can be caused only by blade-to-blade coupling through the rotor wake. The small damping differences seen in figure 10 between the progressing and regressing mode damping values at the lower rotor speeds may be due to wake effects, but the differences seen at the higher rotor speeds are clearly too great for this explanation. These damping differences at high rotor speeds indicate that the rotor lead-lag progressing mode was coupling with the stand. This is not surprising since the progressing mode frequency at 1000 rpm approximately equals the frequency of the lowest stand mode. For rotor speeds above approximately 600 rpm, the progressing mode data are not representative of an isolated rotor.

The most important conclusion from figure 10 is that the regressing mode data show no signs of contamination by rotor-body coupling at any rotor speed. This shows the advantages of using a rotor with three or more blades for isolated rotor dynamics tests. Distinct progressing and regressing modes do not exist for rotors with less than three blades, and, due to the periodic coefficients of the governing differential equations, a single blade mode with the frequency ω in the rotating system will appear in the nonrotating system at the two frequencies $\Omega + \omega$ and $\Omega - \omega$ simultaneously. Any blade motions therefore will couple with the stand at both these frequencies, and any proximity of the high frequency manifestation of the blade mode (at $\Omega + \omega$) to a stand natural frequency will equally contaminate the low frequency manifestation (at $\Omega - \omega$). For the present stand and blades, at rotor speeds above 600 rpm any two-bladed rotor data would have been contaminated regardless of whether the excitation was at $\Omega + \omega$ or $\Omega - \omega$. Bousman, in the paper mentioned earlier, suggests that, for a two-bladed rotor to represent the isolated rotor case, the lowest stand natural frequency should be several times $(\Omega + \omega)$. With three or more identical blades, distinct progressing and regressing rotor modes exist and so any coupling of the progressing mode with the rotor stand does not affect the regressing mode; therefore the necessary condition for a model to correctly represent an isolated rotor is that the the lowest stand frequency be several times greater than the regressing mode frequency. The present model fulfills this requirement.

Even with three blades, the impulsive locking of the roll degree of freedom following the shaker input excites the progressing mode to some degree, even when the model is excited in roll at exactly the regressing mode frequency. The pure regressing mode data can then be extracted only by making use of multiblade coordinates. In practice the single blade signals were usually found to give acceptable results when the excitation level was high relative to

the response to the locking impulse and to the background noise. The multiblade coordinate results were, however, consistently better, based on the appearance of the time histories and the moving-block functions, and were less sensitive to the details of the excitation. The only disadvantage associated with using the multiblade coordinates is the requirement that each blade be instrumented.

Only the regressing lead-lag mode data will be considered further. Figure 11 shows the regressing mode damping as a function of rotor speed for collective pitches of 0°, 4°, 6°, and 8° for the configuration without structural coupling. Figure 11(a) shows that at zero collective pitch the Rotor II damping is lower than that of Rotor I, but the differences are small except at the lower rotor speeds. Those differences may be related to the lower nonrotating flap damping in Rotor II. The damping is generally seen to increase with increasing rotor speed, except for the decrease between 350 and 400 rpm. This decrease grows with increasing collective pitch, and is associated with the coalescence of the flap and lead-lag frequencies (ref. 3).

The regressing mode frequency measured without structural coupling is shown to be essentially independent of the collective pitch angle in figure 12. The regressing mode frequency results obtained with full structural coupling (not shown here) are essentially identical.

The regressing mode damping as a function of the collective pitch is shown in figures 13 and 14 for the configurations without and with structural coupling. For each configuration data are given for both 750 and 1000 rpm; these are the rotor speeds at which the forward flight data were taken. The dimensionless rotating lead-lag frequencies at these rotor speeds are 0.72 and 0.61, respectively. The increase in damping with collective pitch is as expected for soft-inplane hingeless rotors, without kinematic couplings, away from the flap-lag frequency coalescence.

The hover testing was conducted in a relatively small test section with the rotor only 0.6 diameters above the floor. Even for this small separation, there are several factors that indicate that the influence of ground effect and recirculation on the damping data is minor. Most convincing are the model tests with ground planes reported in reference 2. These tests showed that the ground planes had little influence on lead-lag damping, even for very small separations between the rotor and the ground planes. The second factor is evident from a comparison of the Rotor I and the Rotor II hover results to each other. The Rotor I hover testing was conducted with the wind tunnel test-section doors open and the windows removed to reduce recirculation, while the Rotor II hover testing was conducted with the doors closed and the windows installed. The recirculation present is certainly very different for these two situations, although neither closely represents a free air hover test. If recirculation were a major factor, then the data from the two rotors would be expected to show differences that increase significantly with increasing blade pitch. Figure 13, however, shows such differences to be small.

In general, the hover data quality, as judged by the small scatter in the results and the appearance of the time histories and moving-block functions, is very good. Figure 15 shows sample time histories of the cosine lead-lag coordinate and the resulting moving-block functions at the regressing mode frequency for the hover cases at 1000 rpm, with collective pitches of 0°, 4°, and 8°. The ideal moving-block function is a straight line, whose slope is equal to the damping exponent, with small oscillations at twice the analysis frequency superimposed (ref. 17). The 0° and 4° cases (figs. 15(a) and (b)), show nearly ideal results, while the 8° case (fig. 15(c)) shows a somewhat degraded but still very good moving-block function. These results are typical of the hover data. The degradation of the moving-block function at higher collective pitches is the result of a decreased signal-to-noise ratio, due both to increased noise from recirculation, and a lower average signal, due to the higher damping of these cases. The degradation manifests itself in the damping data as increasing scatter with increasing collective pitch.

Forward Flight

Forward flight testing was conducted at rotor speeds of both 750 rpm and 1000 rpm, for the configurations both with and without structural coupling, at collective pitch angles of 0° , 3° , and 6° . The conditions tested without structural coupling are summarized in figures 16 and 17. Figures 18 and 19 summarize the conditions tested with structural coupling. At each advance ratio, the high negative-shaft-angle limits were set by large negative coning loads, while the low shaft angle limits were set by high cyclic flapping loads. The data available for $\theta_0 = 6^{\circ}$ are quite limited due to the high cyclic flapping loads, and therefore the effects of structural coupling in forward flight were not thoroughly explored by this test. Only the results for the configuration without coupling will be discussed herein, but the results obtained both with and without coupling are included in tabular form. Tables 8 and 9 present the data for the configuration without structural coupling at 750 and 1000 rpm respectively, sorted by collective pitch, advance ratio, and shaft angle. Tables 10 and 11 are the corresponding tables for the configuration with structural coupling.

Figures 20 through 25 show the regressing lead-lag mode damping as a function of the advance ratio for the 750 rpm rotor speed, for rotor shaft angles of 0°, -4°, -8°, -12°, -16°, and -20°, respectively. Figures 26 through 31 show the corresponding results at 1000 rpm. Each figure shows all of the data available at each collective pitch tested. The data for Rotor I are limited to the 1000-rpm, zero-collective cases, but includes advance ratio-shaft angle combinations that resulted in higher flapping conditions than Rotor II encountered. Overall the data scatter is small, and in all cases where data from both rotors are available, they agree very well with each other.

Significant changes in the damping at the high advance ratios are seen in figures 28 through 31 at zero collective pitch. The abrupt damping increases begin at lower advance ratios for more forward shaft angles, and are seen only at the high flap load conditions which only Rotor I encountered. In particular the increases appear related to high negative coning conditions, however, no flapping angle or thrust measurements are available for correlation. At these conditions large negative angles-of-attack are encountered over large regions of the rotor disk. The data at the higher collective pitch angles were limited to lower load levels, and do not show similar increases within the test envelope.

The effects of changing rotor shaft angle at fixed advance ratios are shown in figure 32. Results are shown for advance ratios of 0.05, 0.15, 0.25, 0.35, 0.45, and 0.55. Data from both rotors are included without distinction. The large damping increases with forward shaft tilt are again seen at the zero-collective pitch, high speed conditions. The higher advance ratio cases show the increase to begin at less extreme shaft angles.

No special problems were encountered using the moving-block analysis on the forward flight data, and in most cases very good results were obtained. As in hover, the more highly damped conditions tended to show more scatter in the results than did the less stable conditions. Wind tunnel turbulence was an additional noise source, but this was offset to some extent by the reduced recirculation. The addition of 1/rev and 2/rev lead-lag loads due to forward flight also restricted the excitation levels allowable within the lead-lag flexure load limits, but this was not a major factor. Sample transient time histories of the multiblade cosine coordinate of the lead-lag motion in forward flight and the resulting moving-block functions at the regressing mode frequency are shown in figure 33 for $\alpha_s = 0^{\circ}$, and in figure 34 for $\alpha_s = -10^{\circ}$. Both figures are for $\theta_0 = 0^{\circ}$ and advance ratios of 0.15, 0.35, and 0.55. All the moving-block results of figure 33, and those of figure 34(a) and 34(b) are very good. These are all relatively low-damping, low-flapping conditions, and the effects of forward flight alone are not troublesome. The $\mu = 0.55$, $\alpha_s = -10^\circ$ case of figure 34(c), however, shows a somewhat degraded moving-block function. This is a high flapping load case and was one of the most highly damped cases found in forward flight, so the degradation is not surprising. The moving-block function for this case is probably the worst encountered during the entire test, and it is still quite acceptable.

SUMMARY OF RESULTS

An isolated hingeless rotor with discrete flap and lead-lag flexures, relatively rigid blades, and high torsional stiffness was tested in the Aeroflightdynamics Directorate's 7- by 10-Foot Wind Tunnel. The objective of the test was to obtain a database of isolated rotor flap-lag stability in forward flight for correlation with current and future rotorcraft stability analyses. The model was tested at advance ratios up to 0.55, for three values of collective pitch, and for shaft angles from 0° to -20° . Two inplane natural frequencies, 0.61/rev and 0.72/rev, were tested for configurations with and without structural flap-lag coupling. Specific findings include

- 1. The use of a simple model with no swashplate or pitch bearings eliminated control system slop and reduced friction damping to a minimum, and this, together with careful blade-to-blade matching, was largely responsible for the high quality of the test data. The use of a three-bladed rotor, rather than a two-bladed rotor, also greatly eased the problem of unwanted rotor-test stand coupling.
- 2. The test procedures and data analyis techniques, which were originally developed for hover, worked very well in forward flight. The use of multiblade coordinate data for the

damping measurements generally gave better results than did analysis of single blade signals. No problems peculiar to rotor stability testing in forward flight were encountered during the test.

- 3. The hover data obtained are consistent with previous experimental and theoretical results for hingeless rotors without kinematic couplings.
- 4. The most prominent feature of the forward flight data is an abrupt increase in damping with advance ratio at high speed, high shaft-angle conditions, and zero collective pitch. This behavior begins at lower advance ratios for more forward shaft angles, and seems related to high negative coning.

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TABLE 1.-ROTOR PROPERTIES

Property	Rotor I	Rotor II
Number of blades	3	3
Airfoil section	NACA 23012	NACA 23012
Hover tip Mach number at 1000 rpm	0.25	0.25
Hover tip Reynolds number at 1000 rpm	240,000	240,000
Rotor radius, in.	31.92	31.92
Blade chord, in.	1.65	1.65
Radial location of the center of the flexures, in.	3.55	3.55
Radial location of the blade center of mass, in.	11.1	11.1
Mass outboard of the flexure center, slugs	0.0130	0.0130
Flap and lead-lag inertia about flexure center, slug-in ²	1.80	1.80
Torsional inertia, slug-in ²	0.00294	0.00294
Flexure assembly flap stiffness, in-lb/radian	66.0	66.0
Flexure assembly lead-lag stiffness, in-lb/radian	281	281
Flexure assembly torsional stiffness, in-lb/radian	215	228
Nonrotating flap frequency, Hz	3.09	3.21
Nonrotating lead-lag frequency, Hz	6.98	7.24
Nonrotating torsion frequency, Hz	149	a
Nonrotating flap damping, 1/sec	-0.15	-0.09
Nonrotating lead-lag damping, 1/sec	-0.09	-0.09

^a Not measured.

TABLE 2.-LEAD-LAG FLEXURE PROPERTIES

Blade	Mass,	Torsional	Flapping	Lead-lag	Torsional
station,	slug/in	inertia,	stiffness,	stiffness,	stiffness,
in.	J	slug-in ² /in	lb - in^2	$lb-in^2$	$lb-in^2$
2.431	0.013 118	0.003 127	5 087 300	5 087 300	4 000 000
2.581	.013 118	.003 127	5 087 300	5 087 300	4 000 000
2.581	.003 568	.000 593	1 845 300	84 202	25 700
2.601	.002 492	.000 405	1 288 600	28 670	25 700
2.621	.002 202	.000 356	1 138 500	19 773	25 700
2.641	.002 117	.000 342	1 094 700	17 578	25 700
2.730	.002 117	.000 342	1 094 700	17 578	25 700
2.762	.001 799	.000 340	1 091 000	14 938	25 700
2.840	.000 765	.000 175	563 600	6 350	25 700
2.918	.000 584	.000 146	471 900	4 850	25 700
2.996	.000 765	.000 175	563 600	6 350	25 700
3.074	.001 700	.000 3 40	1 091 000	14 938	25 700
3.105	.002 117	.000 342	1 094 700	17 578	25 700
3.255	.002 117	.000 342	1 094 700	17 578	25 700
3.255	.002 117	.000 342	1 094 700	17 578	1 272
3.280	.000 903	.000 144	467 000	1 366	1 272
3.304	.000 550	.000 088	284 600	3 09	1 272
3.329	.000 448	.000 071	231 400	166	1 272
3.777	.000 448	.000 071	231 400	166	1 272
3.802	.000 550	.000 088	284 600	309	1 272
3.826	.000 903	.000 144	467 000	1 366	1 272
3.851	.002 117	.000 342	1 094 700	17 578	1 272
3.851	.002 117	.000 342	1 094 700	17 578	25 700
3.901	.002 117	.000 342	1 094 700	17 578	25 700
3.901	.002 566	.000 386	1 222 000	32 26 0	25 700
4.051	.002 566	.000 386	1 222 000	32 26 0	25 700
4.051	.002 117	.000 342	1 094 700	17 578	25 700
4.101	.002 117	.000 342	1 094 700	17 578	25 700

TABLE 3.-SIDE BEAM ASSEMBLY PROPERTIES

		1		1	1
Blade	Mass,	Torsional	Flapping	Lead-lag	Torsional
station,	$_{ m slug/in}$	inertia,	stiffness,	stiffness,	stiffness,
in.		$slug-in^2/in$	lb-in ²	lb-in ²	lb-in ²
2.633	0.001 650	0.000 237	465 200	296 400	8 277
2.683	.001 650	.000 237	465 200	296 400	8 277
2.683	.001 905	.000 286	537 000	383 000	8 277
2.833	.001 905	.000 286	537 000	383 000	8 277
2.833	.001 650	.000 237	465 200	296 400	8 277
2.883	.001 650	.000 237	465 2 00	296 400	8 277
2.883	.001 274	.000 171	359 000	191 350	8 277
2.983	.001 274	.000 171	359 000	191 3 50	8 277
3.061	.000 601	.000 104	244 300	90 300	8 277
3.139	.000 497	.000 092	221 400	74 670	8 277
3.217	.000 601	.000 104	244 3 00	90 300	8 277
3.295	.001 274	.000 171	359 000	191 3 50	8 277
3.439	.001 274	.000 171	359 000	191 3 50	8 277
3.517	.000 601	.000 104	244 3 00	90 3 00	8 277
3.595	.000 497	.000 092	221 400	74 670	8 277
3.673	.000 601	.000 104	244 3 00	90 3 00	8 277
3.751	.001 274	.000 171	359 000	191 350	8 277
3.851	.001 274	.000 171	359 000	191 3 50	8 277
3.851	.001 915	.000 236	539 900	221 3 00	8 277
3.901	.001 915	.000 236	539 900	221 3 00	8 277
3.901	.001 661	.000 212	468 100	213 050	8 277
4.051	.001 661	.000 212	468 100	213 050	8 277
4.051	.001 915	.000 236	539 9 00	221 300	8 277
4.101	.001 915	.000 236	539 900	221 300	8 277

TABLE 4.-FLAP FLEXURE PROPERTIES

Blade station, in.	Mass, slug/in	Torsional inertia, slug-in ² /in	Flapping stiffness, lb-in ²	Lead-lag stiffness, lb-in ²	Torsional stiffness, lb-in ²
2.633	0.008 584	0.003 526	2 445 000	9 026 000	591 000
2.683	.008 584	.003 526	2 445 000	9 026 000	591 000
2.683	.008 135	.003 439	2 317 000	8 871 000	591 000
2.833	.008 135	.003 439	2 317 000	8 871 000	591 000
2.833	.008 584	.003 526	2 445 000	9 026 000	591 000
2.883	.008 584	.003 526	2 445 000	9 026 000	591 000
2.883	.001 382	.000 450	10 200	1 452 900	342
2.905	.000 558	.000 181	671	586 600	342
2.927	.000 340	.000 110	151	357 100	342
2.949	.000 276	.000 089	81.6	290 600	342
4.157	.000 276	.000 089	81.6	290 600	342
4.179	.000 34 0	.000 110	151	357 100	342
4.201	.000 558	.000 181	671	586 600	342
4.223	.001 382	.000 450	10 200	1 452 900	342
4.223	.007 515	.002 775	1 889 000	7 139 800	3 548 000
4.243	.007 515	.002 775	1 889 000	7 139 800	3 548 000
4.273	.008 054	.002 870	2 042 000	7 295 000	3 669 000
4.303	.011 406	.003 394	3 399 600	7 641 000	4 339 000
4.423	.011 406	.003 394	3 399 600	7 641 000	4 339 000

TABLE 5.-BLADE AND ROOT SOCKET PROPERTIES

Blade station, in.	$egin{aligned} ext{Mass,} \ ext{slug/in} \end{aligned}$	Torsional inertia, slug-in ² /in	Flapping stiffness, lb-in ²	Lead-lag stiffness, lb-in ²	Torsional stiffness, lb-in ²
in. 4.423 4.484 4.484 4.613 4.613 5.078 5.260 5.410 5.410 5.469 5.469 5.529 5.529	0.006 894 .006 832 .007 174 .007 174 .001 643 .001 584 .005 932 .005 932 .000 755 .000 904 .003 696 .003 665 .004 814	slug-in ² /in 0.001 708 .001 708 .001 708 .001 708 .001 708 .000 077 .000 076 .001 224 .001 224 .000 023 .000 027 .000 457 .000 481 .000 916	lb-in ² 1 770 000 1 770 000 1 770 000 1 770 000 1 24 000 124 000 124 000 124 000 45 900 53 800 53 800 99 100 99 100	lb-in ² 3 660 000 3 660 000 3 660 000 124 000 124 000 124 000 124 000 45 900 53 800 53 800 99 100	1b-in ² 2 180 000 2 180 000 2 180 000 2 180 000 95 900 95 900 95 900 95 900 23 800 28 800 28 800 61 600 61 600
5.659 5.659 5.764 5.764 5.924 7.924 31.92	.004 969 .001 388 .001 460 .001 031 .000 237 .000 235	.000 922 .000 053 .000 052 .000 021 .000 022 .000 027 .000 027	101 000 101 000 102 000 52 600 2 280 2 280 2 280	101 000 101 000 102 000 52 600 61 700 61 700	59 600 59 600 56 800 18 700 1 200 1 200 1 200

	numper numper	Collective pitch, deg	Rotor speed, rpm	Shaft angle, deg	Frequency, Hz	Damping, 1/sec
_	R2239001	6	49.57	99.9	6.201	-0 .153
• H	82242041	0.0	50.98		6.174	-0.154
	83222012	0.0	50.82	-0.01	•	-0.082
11	83222013	0.0	50.82	10.0	6.451	-0.077
	82239003	0 .0	100.66	0 0 0	5.377	Τ,
-	82242044	0 .0	99.73	•	5.387	-0.152
	82260007	9 .0	100.78	0.00	5.377	-e 156
11	83222014	9 .	101.87	6. 6.	5.627	-8.092 0.05
II	83222015	9 .0	100.36	-6.01 -101	5.654	-0.092
-	82239005	0 .0	149.41	9.00	4.689	9.100
.	82242046	9 .0	150.59	9.00	4.588	- 6 .162
ı	82239007	o .	200.04	9.00	3.838	C/I.8
H	82242048	9 .	200.39	9.00	3.822	92.9
–	82260009	o .	199.34	90.0	3.842	991.9
11	83222016	0 .0	200.84	6.	4.059	-6.117
11		9.0	200.84	9. 10.	4.088	411.6
-	82239009	6 .0	250.66	9.00	3.068	- B - 189
н	82242050	0 .0	250.43	9.00	3.070	-6.175
H	82259056	9 .0	275.16	9.00 0	2.709	-0.221
H	82259062	0 .0	275.27	9.60 9.60	2.705	-6.18g
H	82259063	6 .6	274.92	89.69 0.09	2.789	
-	82259064	Ø.	274.80	9.00	2.769) ; s
 4 (82259058	9 (290.27	9 . 9 . 9 .	7.407	27.0
 •	82259068	9.0	290.04	9.6	7.400	9 9
٠,	82228008	9 0	90.607	9.0	054.7	4
٠,	82239011	9.0	300.47	90.0	400.4 644.0	4
→ •	82242008	9 6	300.03	90.0	2.336 677 6	9
٠,	82242852	9 0	366.23	9 6	200.2	9
→ ►	02240001	9 6	70.100	9 6	2.340	179
4 F	R1222011) s	300.00	40.6	2.512	-6.136
:=	83222019	9 6	300.86	9.01		-0.135
; 	82259060	0.0	315.00	90.0	•	-0 .203
	82259072	0.0	315.23	9.00	2.119	-0.176
—	82259073	0.0	316.05	90.0	2.109	•
H	82242010	0.0	350.16	99.0	1.623	-6.185
H	82242054	0 .0	350.39	0.00	1.607	-6.176
-	82246003	0 .0	379.69	9.00	1.193	-0.201
H	82246011	0 .0	380.04	0.00	1.170	171.0
—	82242012	0.0	400.31	09.00	0.912	7 S
-	82242056	0 .	399.38	00.00	410.0	90.0
—	82260013	0.0	399.61	9.00	2 2	6.13
I	83222020	Ø. 6	400.29	9.04 40.0	1.166	44
Ξ'	83222021	9.0	466.99	5 e	- 136	
٠,	82242000		04.00	9.00	144.0	. d

Rotor	Data point number	Collective pitch, deg	Rotor speed, rpm	Shaft angle, deg	Frequency, Hz	Damping. 1/sec
	82260032	6	500.74	-21.00	9 475	9
	82242018	9.0	549.96	0.00		9.151
	82242062	0.0	549.96	90.0	1.123	9.148
	82246005	6 .0	565.66	9 .00	1.326	4.9
	82246009	6 .0	564.84	9 .00	1.314	6.143
	82242020	0.0	600.59	9 .00	1.775	-0.142
	82242064	Ø .	599.06	0.00	1.762	9.147
	82246007	0.0	600.35	0.00	1.756	-6 .150
	82260017	Ø.	600.00	0.00	1.771	-0.151
	83222024	9 .0	599.28	- e- e-	1.524	6.135
	83222025	6	600.21	9 .02	1.532	6 .128
	83222838	9 .0	601.02	6.63	1.545	-6 . 129
	83222831	9.0	600.21	9.04	1.533	-0.128
	82268638	9.0	600.82	-21.00	1.783	9.149
	22024229	s 6	040.88	9.00 0.00	2.406	4.14
	90074770	9.0	648.52	9 (9	2.396	40.147
	47074770	9 6	699.26	9 6	5.051	-8.155
	02247900	9 6	000	9.6	5.040 5.040	
	81000000	9 6	10.80	9.0	20.0	9 6
	8322202		700.00	9 6	2.010	9
	83222032	9	700.46	9.0	2.818	9 9
	83222033	0.0	699.30	9.03	2.802	-6.134
	82260029	9.0	701.25	-21.00	3.061	991.0
	82242026	9.6	750.35	9.00	3.664	-9 .165
	82242070	0 .0	750.35	9 .00	3.668	-6 .160
	83222034	0 .0	750.93	9.04	3.448	9. 141
	83222035	9 .0	750.46	9.0	3.440	9.1
	83222036	9 .0	751.16	40.0	3.446	-0.134
	62222637	9.6	751.02	9.62	5.456	-0.142
	63222040	. 6	750.76	9. 6 C 4	5.44 4.5	9.15
	8322300	9 6	750.55	9 6	1 410	9
	83223001	9.0	750.00	90	3.429	42
	83223039	0.0	749.54	0.02	3.427	-6.142
	83223040	0 .0	749.42	9.00	3.425	b. 143
	83223061	9 .0	749.54	0.03	3.429	
	83223062	9 .	747.91	0.03	3.409	9.14
	83223071	0 .0	748.49	4 . 9	3.417	4.1.6
	83223072	9 .0	749.07	4.0	3.423	-6.141
	83224000	9 .0	750.70	9.00	3.440	-6.143
	83224001	9 .0	749.77	-6.65	3.427	9.145
	83228000	'	749.07	6.6	3.427	6.143
	0222601	9.0	00.04/	9		9
	************	•	140 40			74

tested	Data point number	Collective pitch, deg	Rotor speed, rpm	Shaft angle, deg	Frequency, Hz	Domping. 1/sec
						191 0
—	82269627	9 .0	751.52	-21.00	5.584 1.084	9 9
⊢ ,	82242028	9 e	201.21	9 9 9 9	4.263	92.4
- ,	82243667	. 6	700.00	9 6	4 273	161
<u>-</u> -	82260021	D 6	700.00	. e	4.040	9.145
7 T	0277700 01000018	9 6	73.667	100	4.044	6.143
	82242638	9 6	849.61	8	4.871	
• •	82242033	9	851.02	98.	4.891	J 171
	82243009	9.	850.43	98.99	4.879	-6.174
_	82242035	0.0	900.47	98.99	5.480	-6.173
_	82243011	9 .	966.94	9 .00	5.482	9.172
-	82250021	9 .	900.006	9.00	5.480	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\
_	82260023	0 .0	900.47	9.00	5.486	9.169
Π	83222040	9 .0	960.72	6.63	5.264	
11	83222041	6 .6	990.60	0.63	5.260	
_	82242037	9 .0	949.92	90.00 90.00	80.00 90.00	
—	82243013	9 . 6	949.45	9 . 9 . 9 .	0.00	9
,	82250023	9 .0	958.16	9 6 9 6	0/0.0 0ra	4 5 6
- , .	82242639	9.0	10.000	8.6	6.00 7.73	5
	82243015	D 6	24.000 AA.000	9 6	6.658	-6 . 184
r-	02230022 0235005	9 6	2000		6.643	
-	82263001	9 9	1000.43	0.00	6.646	
· II	83222028	9.9	1666.39	-0.02	6.436	Ψ.
Ξ	83222029	0.0	999.23	-0 . 0 2	6.420	
II	83222042	0 .0	999.81	0.03	6.428	9.169
II	83222043	0 .0	999.23	6.63 5.63	6.422	79.197
I	83222044	9	40.000	9.0	0.420	4
	83222045	S 6	20.000	6 e	6.422	6 .161
	84224110	9 6	1888.39	0.02	6.436	-0 .162
	83223118	9 69	1000.04	0.02	6.430	-9.169
: =	83223119	9.6	999.23	0.03	6.420	-6 .157
Π	83224002	9 .0	1000.62	-0.07	6.436	-8.165
11	83224003	ø. Ø	999.92	-0.07	6.428	20.00
II	83224030	0.0	1000.04	6.6 6.6	6.432	29.162 46.162
ΙI	83224031	o .	998.41	6.61	6.411	9
II	83224969	0.0	999.23	9.93	6.422	9 9
	83224061	9 .0	999.69	6.65 6.65	0.430	9 9
Ξ;	83224092	9 0	999.18	9.60	6.4.6	158
- I	22772007	9.0	000 14		6.424	-e 158
⊒ :	63226663	9.6	+0.000 ++ 000	9	6.422	-6.159
:	63220004 64220004	D 6	988 COO	70.0	6.422	6 .163
: =	10061100	9 6	1999 15	9.87	6.432	-6.163
11	20087720	9,9	200			

rpa	
1098.75	
201.09 250.20	
748.14	
748.96	
748.72	
749.88	
749.30	
747.91	
750.35	
750.00	
749.88	
751.04	
749.19	
749.77	
751.62	
751.28	
750.70	
754 86 754 86	
998.99	
998.99	
998.99	
998.23 001.08	
999.46	
999.81	
999.46	
900.13	
999.85 999.85	
000.73	
666.39	_
999.57	_
69.666	_
50.51	
	_
100.43	
100.20	_
149.65	
150.82	
200.16	
200.16 200.51	
200.16 200.51 249.84	

Damping, 1/sec	-0.190	Τ.		•	- '	6.173	47.9	Ξ,	9	. ~	-6 .129	6.134	-6.136	-6.219	-0.216	-0.247	-6.240	247.0	9.20		-0.303	-6 .337	-6.342	-6.382 9.332	45.4	: -:	╌	٠.	•	9		-0 .185	₩.	Ξ,	9 e	9		Ξ.	•	6.133	•
Frequency, Hz	2.689	2.691	2.473	•	2.479	•	٠	2.111	4 600 4 600	1.615	1.176	998	6.908	0.457	0.467	1.119	1.791	7.764	5.604 5.945	4.289	4.277	5.479	5.467	6.639	6.040 160	6.193		5.361	3.799	3.000 5.000 5.000	3.047	2.682	2.672	•	2.453	2.303	2.100	2.100	1.586	1.588	900 6
Shaft angle, deg	9.00	99.9	9 0.00	•	0.00	0.00	•	9 9 9	9 6		9 6	0.00	9.00	9.00	9.00	9.00	9.00 0.00	9.00	9 G		00.0	9 .00	9.00	9.00		90.0	0.00	9.00	9.00 0.00	9 6	9.00	0.00	9.00		•	9.0	9 6			9.66	•
Rotor speed, rpm	275.16	275.04	289.69	289.92	289.57	300.23	300.23	314.77	510.08	349.92	380.16	399.26	399.61	500.39	500.51	549.61	601.41	500.10	701.25	500.50	799.92	883.88	889.88	1000.08	27.000 50.000	48.75	100.55	166.28	200.39	189.82	250.08	274.92	275.63	290.16	290.39	200.00	306.00	314.77	350.51	350.27	900
Collective pitch, deg	4.0	4.0	6 .4	4 .0	4. 6	4 .0	9 .	4 •	9 ¢	. 4 0 6	9	6.	6.	4.0	4.0	4.0	4 .0	9.	9 4	- -	4	4.0	4.0	4 .0	9 4	9 6	0.0	6.0	Ø.	s	9 69		6.0	•	•	٠	9 G	9 69		•	•
Data point number	82259037	82259043	82259039	82259045	82259046	82243035	82244017	82259041	62223646	82242637	82244021	82243039	82244023	82243843	82244025	82243045	82243047	82244027	82245049	82243052	82244031	82243054	82244033	82243956	82244833	82258048	82258015	82258050	82258017	82238032	82258054	82259001	82259007	82259003	82259009	82238821	82250830	82259011	82258024	82258058	9000000
Rotor	-	—	•••	 :	—		H :	⊶ •	-4 P-	- h-	.		. —	_	H	.	н,	 1	→ 	4	. 14	-	— (ы,	F	- I	. 14	-	-		4	-	-	—	н,	~ ⊦	-4 ⊩-	• •	-	Н	

	Domping. 1/sec	9	9.466	234	-6.293	9.344	-6.358	-0.292	-0.469	-6.418	6 .381	-6.401	-6.465	9. 1 38	-6.437	-8.394	-0.456	-9 .352	-6.367	9.448	-6.465	9.459	9 4 2 4 4	457	437	-6.423	-0.423	-0.427	-6.438	. .	6.463	9.4.6		-0.599	-6.558	-0.494	-0.520	-6.5 44	-6.548	-6.566	-9.566	e.583	-6.579	-0.577	-9·154
	Frequency, Hz	108 0	6.63	•	1.779	1.783	1.777	1.777	3.039	3.055	3.045	3.658	3.689	3.676	3.429	3.434	3.436	3.427	3.454	3.419	3.432	3.432	5.41/ 5.41/	7.432	3.431	3.431	3.438	3.438	3.434	3.425	4.295	4.283	5.475	6.660	6.660	6.412	6.440				•		•	6.422	6.141
a	Shaft angle, deg	9	•		00.00	0.00	0.00	9.00	9.00	90.0	99.	00.0	0.00	90.0	00.0	9.00	0.03	0.03	6.63	9.93	0.03	6.65 5.65	10.07	30.00	20.01 20.01	-19.93	-19.92	-19.99	-19.98	-19.98	9.00 0.00	9 e	9 6	0.00	0.00	0.03	0.03	99.0	4 0.0 4	-19.95	-19.95	o n (-19.96	99. 9
TABLE 6.——CONTINUED	Rotor speed, rpm	400 KK	500.39	500 16	600.35	600.23	600.23	666.66	699.49	700.66	96.669	749.18	751.41	750.35	750.46	750.70	749.65	749.88	751.28	749.65	749.88	749.88	740.65	740.00	749.54	749.42	750.23	750.58	750.23	749.54	801.33	800 . 40. 008	0 - 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	96.666	1000.08	999.81	1000.04	999.23	998.76	998.41	997.83	1000.62	999.81	998.88	50.86
-	Collective pitch, deg	9	9 6	9	9	6.0	0.0	6.0	6.0	6.6	6.6	6.0	6.0	6.9	6.0	6.0	6.0	6.0	6.0	9.	0.		9 4	9	9 6	9	6.9	6.9	6.9	6.9	Ø.0	S	9 G	6.9	6.9	6.9	6.9	6.9	6.9	6.9	6.0	6.0	6.6 6.0	9.0	Ø.
	Data point number	ROOFBORD	82258028	82258062	82258030	82258044	82258045	82258064	82258032	82258043	82258066	82258034	82258042	82258068	83242000	83242901	83242672	83242003	83242004	83242005	83242006	83242007	83242013	4107170	83242015	83242022	83242023	83243000	83243001	83243002	82258036	82258070	02230030 82258073	82258040	82258074	83242008	83242009	83242010	83242011	83242017	83242018	83242019	83242020	83242021	82244037
	Rotor	-	4 1		•	—	-	-	-	-		H		-		I	II	II	I	II	II	:] [7 -	7 1	: -	11	II	Ξ	11	— (-4 b	•		II	II	11	11	II	II	II	II	ï	I

			TABLE 6.—CONCLUDED	G.		
Rotor	Data point number	Collective pitch, deg	Rotor speed, rpm	Shaft angle, deg	Frequency,	Domping, 1/sec
-	80045015	60	49.80	99.69	6.164	-8 .156
- F	8224039	• •	166.26	9.00	5.338	- 6 .183
۰.	82245017	. 60	100.08	00.00	5.350	9.200
•	82244041	0	151.29	00.00	4.549	6 .181
, ,	82244043	60	199.69	9.00	3.789	-0.227
•	82245021	9.60	200.63	9.00	3.781	-0 .222
•	82259019	60.60	275.39	00.0	2.658	-0 .204
	82259025	60.00	275.27	99.00	2.660	-6 . 196
· H	82259021	60.	291.33	0.00	2.422	-6 .188
	82259027	8	290.98	00.00	2.426	-0 .186
	82244045	60	299.30	00.0	2.301	-6 .186
	82245023	60.	300.12	9.00	2.295	-6 .189
	82259023	80	315.47	9.00	2.074	-6 .163
	82259029	80.	315.00	9.00	2.080	-6 .160
-	82244047	8.0	379.69	0.00	1.170	
	82245025	80.00	379.57	9.00	1.176	
-	82245048	8.8	379.92	99.9	1.164	. 138
-	82245027	8	399.73	0.00	898	-6 .135
	82245013	60.	564.73	9.00	1.307	9 .328
-	82245046	8	565.43	99.9	1.334	-0.421
	82244053	8.0	599.06	99.9	1.779	-0.463
-	82244055	8 .0	700.08	9 0.0	3.057	-0 .502
	82245034	8.0	699.73	99.9	3.037	-0.570
-	82244057	8.6	789.57	99.9	4.289	-0.557
-	82245007	8.8	800.39	99.99	4.295	9.66
-	82245036	8.	800.74	99.9	4.291	-0.727
-	82245038	80.80	800.16	99.9	4.291	-9.736
,	82245040	9 .	801.56	99.0	4.307	-0.698
H	82245009	8.0	900.35	9 0.00	5.467	-6.764
	82245042	8.9	900.59	90.0	5.498	-8.655
-	82245011	8 .80	•	9 .99	6.672	598.9
-	82245044	ø.	999.49	99.9	6.639	-6.767

82239001 83222013 83222013 82222013 82239003 82239003 83222014 83222014 83222014 83222014 82239005 82239007 83223007 83222016 83223007 83222016 83223007 832230064 832230064 832230064 832239064 832239064 832239064 832239064 832239064 832239064 832239064 832239064 832239064 832239064 83239064 83239064 83239064 83239064 83239064 83239064 83239064 83239064 83239064 83239064 83239064 83239064 83239064 83239064 83239064 83239064 83239064 83239064 832330011	49.57 58.98 58.82 58.82 198.65 199.73 149.41 159.59	0 0 0 0 0 0 0 0 0		1/800
	56.98 56.82 56.82 166.66 199.73 166.36 149.41	9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	6.201	141
	59.82 59.82 199.73 199.73 199.36 149.41 159.59	6.61	6.174	-6.15 4
	56.82 196.66 99.73 196.78 196.36 149.41 156.59		6.443	-0.082
	198 . 66 99 . 73 190 . 78 190 . 36 159 . 59	. 6.61	6.451	-0.077
	99.73 100.78 101.87 100.36 149.41 150.59	00.00	5.377	-6.157
	166.78 160.36 149.41 156.59	9.60 0.00	5.387	-0.152
	186.36 149.41 156.59	9.6	5.377	-8.158 9.05F
		ē ē	5.654	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
		90.0	600.4	- 16a
		9.00	4.588	-6.162
	to.007	00.00	3.830	6.175
		90.0	3.822	9.166
	199.34	99.	3.842	6.160
	200.84	6.6	4.050	6.117
	200.84	.e. 16.61	4.088	4 - 1 - 4
	250.66	9.00	3.068	. 189
	250.43	90.0	3.070	-0.175
	275.16	9 .00	2.709	-0 .221
	275.27	9.00	2.705	-6 .189
	274.92	9.00	2.709	-0.175
	274.80	00.00	2.709	-0.177
	230.27	9.60 9.60	2.482	6.173
	290.04	9.00	2.486	-6. 168
	209.00	9 6	2.436	2 G
	300.4/ 101.06	90.0	2.554	9 . 100
	20.10C	90.0	2.338	- Pe - 190
	200.43	90.0	2.332	2 .
	2000	9 6	2.310	? 9
	300.05	46	2.512	436
	300.86	-0.01	2.512	-6.135
	315.00	90.0	2.121	-0.203
	315.23	9 0.	2.119	-9 .176
	316.05	•	2.109	-9 .176
•	350.16	0.00	1.623	-6 . 185
	350.39	•	1.607	-9 .176
•	379.69	0.00	1.193	-0 .201
	380.04	0 0 0 0	1.170	-6 .171
	460.31	6.00	0.912	6.179
	399.38	9.0 0.0	0.914	-6.159
	399.61	9.00	0.918	a . 155
83222020 0.0	400.29	40.0	1.166	4.14
9	•	6.6 6.6	1.156	-6.146
82242050	499.45	9.	0.441	6.157

Domping. 1/sec	-6 .169	6 .151	9.148	4.9	6.143	-0.14 2	٣.	٣.	Τ.	٦.	-0.128	-0 .129	-0 .128	-0.149	9.14	-0.147	Τ.	٠.	Ξ.	٠.						. •	. •	-	_	-0 .142	9.140	6 .141	-	_	_	6.143	9 - 7	∓. •	47.9	∓ •	÷	-0.142	-0.143	-6 .142	-0.142	-0.141	
Frequency, Hz	0.475	1.115	1.123	1.326	1.314	1.775	1.762	1.756	1.77.1	1.524	1.532	1.545	1.533	1.783	2.406	2.396	3.631	3.045	3.039	2.818	2.823	2.818	2.803	3.961	3 664	3.668	3.448		•	•	3.444	3.440	3.432	3.429	3.427	3.425	3.429	3.409	3.417	3.423	3.440	3.427	3.427	3.436	3.440	3.434	
Shaft angle, deg	-21.00	90.	90.0	90.0	0.00	9.00	9.00	9.00	9.00	. 9.91	-0 .02	0.03	9.04	-21.00	00.0	00.0	9.00		90.60	5	56.6	9.6	9 6	-2.5 84.	90.6	9 6	9 6	9.0	9.04	0.02	9.05	9.05	9.60	9.00	9.67	9.06	0.03	0.03	9.1	4.14	90.0	-9.95	6.61	9.91	6.67		
Rotor speed,	500.74	549.96	549.96	565.66	564.84	690.59	599.06	600.35	600.00	599.28	600.21	601.02	600.21	600.82	649.80	648.52	699,26	95 559	699.61	786 57	701.15	799.46	90.00	761.25	750 35	750.35	750.037	750.46	751.16	751.62	750.70	750.35	750.60	750.00	749.54	749.42	749.54	747.91		749.07	750.70	749.77	749.07	749.88	750.58	750.12	
Collective pitch, deg	9.	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0						9 6	9 6) G		9 6	9		0.0		0.0		0.0	0.0	0 .0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	S	9.0	
Data point number	82260032	82242018	82242062	82246005	82246009	82242020	82242064	82246007	82260017	83222024	83222025	83222030	83222031	82260030	82242022		82242024	82242068	82260019	83222005	83222027	83222032	8122203	8225000	82242025	82242070	83222634	83222035	83222036	83222037	83222046	83222047	83223000	83223001	83223039	83223040	83223061	83223062	83223071	83223072	83224000	83224001	83228000	83228001	83229000	83229001	
Rotor	П	П	H	H	-	-	-	-	-	11	II	II	II	H	H	_	-	-		11	: -	:=	: -	: -	4 P		11	11	II	11	II	II	Ξ	11	11	11	II	II	I	II	II	11	11	11	11	II	

tested	Data point number	Collective pitch, deg	Rotor speed, rpm	Shaft angle, deg	Frequency, Hz	Domping, 1/sec
	20003000	•				
	82242028	D 6	20.107	90.12-	484	-e .161
•	82243007		800.63		4.203	9 9
-	82260021	0.0	799.80	90.0	4.273	
Ξ	83222038	0.0	799.20	9.62	4.040	
II	83222039	9.0	799.54	0.03	4.044	14.3
H	82242031	0.0	849.61	0.00	4.871	_
H	82242033	9.0	851.02	9.00	4.891	6.171
-	82243009	0.0	850.43	9.00	4.879	6.174
—	82242035	0 .0	900.47	90.00	5.480	6.173
ı	82243011	6 .0	900.94	9.00	5.482	6 .172
-	82250021	0 .0	900.006	00.0	5.480	_
—	82260023	0.0	900.47	9 .00	5.480	
II	83222040	9.0	900.72	0.03	5.264	_
11	83222041	0.0	900.00	0.03	5.260	
H	82242037	9.0	949.92	9.00	6.029	
-	82243013	0.0	949.45	00.00	6.051	
-	82250023	0.0	950.16	0.00	6.070	-6,186
-	82242939	9.0	999.61	0.00	6.639	-6.186
-	82243015	0.0	999.49	9.00	6.637	-6.198
.	82250025	0.0	1000.66	0.00	6.658	-6.184
H	82260025	9 .0	999.84	9.60	6.643	
-	82263001	9 .0	1000.43	00.0	6.646	
II	83222028	6 .0	1000.39	-6.62	6.436	-0 .163
I	83222029	9.9	999.23	-9 . 0 2	6.420	-0 .156
II	83222042	0 .0	999.81	0.03	6.428	-0.160
H	83222043	9 .0	999.23	0.03	6.422	-0 .162
11	83222044	0 .0	999.34	0.03	6.420	
II	83222045	9 .0	1666.62	0.03	6.440	_
11	83223116	0 .0	999.23	0.02	6.422	
II	83223117	0.0	1000.39	0.02	6.436	-0 .162
II	83223118	0 .0	1000.04	0.02	6.430	-0 .160
II	83223119	9 .0	999.23	0.03	6.420	-0.157
II	83224002	0.0	1000.62	-0.0 7	6.436	_
II	83224003	0.0	999.92	-6.67	6.428	-0 .163
II	83224030	0 .0	1000.04	-6.61	6.432	-0 .162
II	83224031	6 .	998.41	-6.61 10.01	6.411	_
II	83224060	9 .	999.23	0.03	6.422	-0 .163
II	83224061	9 .0	993.68	0.03	6.430	-6.161
_	83224092	0 .0	998.18	9.00	6.411	
II	83228002	0 .0	1000.15	9.00	6.436	_
II	83228003	0 .0	999.34	9.00	6.424	-6.158
II	83228004	0.0	999.11	-6.01		-0 .159
II	83229002	0 .0	999.46	0.07		-6.163
II	83229003	9.0	1000.15	0.07		
1) .)	0			

Damping, 1/sec	- 6 .198	2/9.6	-6.677	-6.098	-0.100	Ξ.	╌`	-6 .129	25.6		7/2	4CC 6	9.77.9	9 243	4.24 28.24	57.9	2.6	-9.258	-0.245	-0.242	-0.243	-0.243	-0.246	-0.245	-0.241	-6.243	6.241	-0.248	9.241	457.0	0.7.0	27.9	270	245	272	245	25.0	4 248	27.9	147.0	9.246	6.23	-6.238	-6.239
Frequency, Hz	7.781	6.43/		5.645	5.658	4.088	4.092	2.595	2.59/	9/1.	1.106		332 2 835	7.00 C	770.7	4 443	3.432	3.427	3.438	3.431	3.434	3.442	3.436	3.434	3.431	3.444	3.442	3.440	3.440	404.0	0.440 44.60	3.436 4.48	27.7	3 432	101	3.42/	4.46	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	0.4.5 44.4	0.440	3.423	5.446	3.436	3.429
Shaft angle, deg	0.00	. 6 6 7 6	6.67	0.07	0.07	0.07	0.67	0.07	6.67	•			- 6	9	9 6	9 6	90.0	9 6	6.03	9.03	9.93	-0.05	-6.65	9.04	40.0	9.03	0.03	0.02	9.02	6.67 0	9.63	9.9		9.6	6.6	200	19.92	78.87	10.00	19.90	19.98	78.61-	-20.00	-19.99
Rotor speed, rpm	1098.75	26.4/ 48.06	50.01	100.48	99.78	200.38	200.15	300.51	300.39	466.64	486.64 50.04	00.00	200.000	90.007	740.92	740.42	749.54	749.54	750.23	749.42	749.77	750.12	749.65	749.88	749.54	750.35	750.23	750.23	750.00	749.54	756.23	+8. IC/	740.70		74.647	750.95	750.40	759.00	•	٠	748.96	•	•	749.54
Collective pitch, deg	0 6		. e.	3.0	3.0	3.0	ю. Ф.	9. 9.	9.6	 	9 G	9.6	9 G	9 6	9 6 7 F	9.6	9 G	9 6	9 69	(N)	9.0	3.0	9.6	3.0	3.0	9. 9.	9.0 0.0	ю. 6.	ю. 6.	9 ·	9 (? !	9 G	9 e	9.6) 	9 G	9.0	9.0		5.6 	ю. 9.	ان ن	o.5	g.
Data point number	82250029	83244000 87244001	83244002	83244005	83244006	83244007	83244008	83244009	83244010	62244611	83244012	03244013	83244816	01044010	02244010	81044018	87244021	83244022	83255000	83255001	83255002	83255033	83255834	83256000	83256001	83256032	83256033	83256070	83256071	832560/2	6222666	63238661	02220000	10000000 77087078	0000000	63230636	0707470	03244024	0373360	42722664	83256002	832256003	83258002	83258003
Rotor	н;	! !	:::	II	II	II	II	I:	-				- -	1 -	7 .	: L	-	1 L	::	II	1	=	II	11	II	=	= :	Ξ:	I	≓:	7 :	F	7.	7 -	7 -	7.5	 	7 1	7.1	≓ :	-	-	11	II

Rotor	Data point number	Collective pitch, deg	Rotor speed, rpm	Shaft angle, deg	Frequency, Hz	Damping, 1/sec
	83058030	6	750.58	19.93	3,448	243
: II	83258033	3.0	749.19	-19.94	3.429	-0.244
	83258039	3.0	749.42	-19.98	3.432	-0.244
II	83258040	3.0	749.88	-19.98	3.436	-0.250
11	83244025	3.0	799.78	0.03	4.051	-9 .256
II	83244026	3.0	799.66	0.03	4.047	-0 .256
II	83244027	3.0	899.44	0.03	5.252	-0.270
II	83244028	3.0	899.56	0.03	5.254	-0 .271
=:	83244029	G.0	999.34	9.63	6.428	-0.294
_	83244030	0.0 0.0	999.57	9.93	6.430	-0 .290
I:	83244031	ю. 6	1000.15	0.03	6.436	9.288
=:	85244032	8. G	999.92	9.0 0.0	6.454	-6.288
] :	83244036	o.,	999.46	0.67	6.438	-6 .292
- :	85244057	9 (04.000	9.0	6.428	167.0
= :	83245888	o.,	1666.85	9.63	6.438	-6.293
: :	62245661	9.6	1904.27	9.6	424.0	6.293
: :	9924369	9.6	1001.32	50.00 00.00	0.443	167.9
	03243001	9.6	40.000 1000		0.420 8.457	400.0
:=	81250806 81250804	9 6	1991 29	9.6	8	207.9
•	83250004	9 69	25. 666	90.0	6.428	-6.285
	83250005	9.50	998.53	-6.67	6.416	-0 .292
=	83251000	3.0	1001.55	9.00	6.445	-0.288
=	83251001	3.0	1000.04	9.00	6.428	-0.286
_	83251022	9.0 9.0	999.81	0.07	6.428	-0 .285
	83251023	e. 6	999.11	6.67	6.420	-0.283
<u>.</u>	83251028	ы. ө.е	1000.27	9.93	6.436	-6 . 280
	8221828	9.6	1000	6.63	0.440	907.9
- F-	83252001	9 6	1999.73	80.0	6.436	6 283
	83252054	3.0	1000.00	0.00	6.430	-6 .285
	83252055	3.0	1000.00	0.00	6.416	-0.286
=	83244033	3.0	999.92	-19.92	6.434	-0.294
=	83244034	3.0	998.99	-19.91	6.422	-0 .296
-	83244035	3.0	999.23	-19.91	6.426	-0 .299
=	83249002	9. 9.	1000.50	-19.94	6.434	-0 .284
= :	83249003	6.0 6.0	1666.97	19.94	6.441	-6 .291
Ξ:	83250002	9 ·	1000.50	-20.00	6.434	-0 .282
-	83250003	9 e	40.000	7 1 (0.422	6.28g
= =	6323666	D 6	1000.04	00.00	0.434 436 436	967.0
	81251882	9 G	989.40 008.78	n o	6.420 6.412	28.5
•=	84251001	9 6	9000	0	6.420	-B 286
:=	83251024	9.0	999.11	0	6.418	-0.285
-	200120			1 (1
-			\C.	110.07	F. 424	291

Domping. 1/sec	-6 .291	-6 .285	-9 .288	-6 .512	-9 .556	-9.579	-9 .560	-9 .586	-9 .589	9 .588	-6 .701	-B.690	-6 .678	-0 .723	-6 .723
Frequency, Hz	6.430	6.441	6.418	3.450	3.461	3.452	3.471	3.448	3.450	3.454	6.449	6.451	6.457	6.457	6.440
Shaft angle, deg	-19.93	-20.00	20.00	6.67	0.07	6.07	-19.95	-19.97	-19.96	-19.96	6.61	6.61	-20.00	-20.00	-20.00
Rotor speed, rpm	999.69	1001.32	999.23	750.58	750.70	750.12	751.39	749.65	749.65	750.12	999.46	999.92	999.95	1000.04	998.65
Collective pitch, deg	a.6	a.0	3.0	6.0	6.9	6.0	6.9	6.9	6.9	6.9	6.6	6.0	6.9	9.9	6.9
Data point number	83251031	83252002	83252003	83259022	83259023	83259024	83259021	83259025	83259026	83259027	83259081	83259082	83259083	83259084	83259085
Rotor	11	Π	II	II	II	Π	II	Π	Ξ	II	II	II	II	II	II

TABLE 8.-REGRESSING LEAD-LAG MODE DATA IN FORWARD FLIGHT, CONFIGURATION WITHOUT STRUCTURAL FLAP-LAG COUPLING, 750 RPM

Damping. 1/sec	-0.150	٣.	Τ.	-B. 145	Ť	- 14 5	9.7	-0 .142	-6.139	Τ.	Ξ.	-	-6 .138	-0.137	-6.133	-	_	•		-9.146	9.148	-0.163	_	-0 .173	-	-0.152	_	-0.153	₹.	-9.152	_ '	-6.14/	- •	* * *		- # - # - 9	•	9 9	: *		46.6	•	- •	9 - 7	- e	-
Frequency. Hz	3.431	3.442	3.454	3.429	3.427	3.434	3.444	3.440	3.440	3.446	3.434	3.436	3.444	3.442	3.438	3.452	3.458	3.448	3.461	3.442	3.450	3.456	3.452	3.450	3.450	3.425	3.427	3.434	3.434	3.425	5.458	5.4.5 5.50 5.50 5.50 5.50 5.50 5.50 5.50	0.428	5.4.5 1.4.5	- 60	3.428		3.446	7 4 4 8	3.446	7 446	•	7.7.	•	•	٠.
Shaft angle, deg	-0.07	-0.67	-1.99	1.99	-4.02	4.02	-6.03	-6.03	-8.03	-8.03	-10.07	-10.07	-12.04	-12.04	-12.04	-12.05	-14.04	-14.04	-15.96	-15.96	-15.96	-18.02	-18.02	-19.64	-19.64	69.0-	69. 9	0.00	0.00	6.66 6.66	-2.66	97.7-	***	† . e	9	-2 93 -7 93		-18.92	000	12.00	12.50	1010	10.62	12.00	14.66	Ė
Advance	0.095	0.033	6.693	6.693	0.093	0.003	0.092	0.032	0.093	0.093	0.093	9.036	0.002	6.697	960.0	960.0	960.0	9.038	60.0	869.0	960.0	860.0	0.095	960.0	460.0	0.149	0.150	0.150	6.156	9.159	٠	54.	9.79	- *	: *	. •	•	6 1 40	27.0	971	: "	•	•	٠	. d	-
Rotor speed,	749.54	750.46	751.39	749.42	749.19	749.88	750.70	750.35	750.46	750.93	749.88	750.12	750.70	750.58	750.35	751.39	751.74	750.93	751.97	750.46	751.04	751.39	750.93	750.81	750.81	748.96	749.19	750.00	750.00	750.00	750.12	740.42	74.847	749.54	740 54	759.12	750 75	749.65	750.00	750.46	750 46	750.10	750.02	750.00	750.00	100.00
Collective pitch, deg	0.0	0.0	o . 0	•	•	٠	•	٠	٠	•	•	•	9 .	٠	9.9	0.0	ø.	0.0	0.0	0.0	•	•	0.0	0 .0	•		0 .0	•	ø. 6	•	s 6			e		e	9		•	•	•	•	•	•	9.6	٥.
Data point number	83222048	83222049	83222050	83222051	83222052	83222053	83222054	83222055	83222056	83222057	83222058	83222059	83222060	83222061	83222062	83222063	83222064	83222065	83222066	83222067	83222068	83222069	83222070	83222071	83222072	83222073	83222074	83223002	83223003	83223884	62522675	0707776	1/077700	83222878	0.011100	8322288	00000000	83222883	8322284	83222085	8322286	8400087	81221007 81221005	2002770	87227885	10007700
Rotor	11	H	Ξ:	⊒:	⊒;	:	Ξ:	⊒;	Ξ:	-	Ξ:	II		II		I	II	II	11	11	II	11	11	I	11	11	II	H	Ξ:	 :	- 7	- - -	: :	; <u>-</u>	· -	-	· -		·		: -	:=	: -	1 L	- L	4

Damping, 1/sec	-6.184 -6.194		. e	-6.195	-0.202	-6 .198	•	-0.159	•	9.148	40.79	9 . 48		94.4		٠	182	161	-0.188	-0.193		-0.192	-0.189	-0.201	-0.205	9.281	-6.264	6.0	•	9	-0.151	Τ.	-0.161	┺.	┺.	-0.169	-0.184 ::	▔	-0.196	Τ.	٦.	-0.198
Frequency. Hz	3.448	3.435	5.431 4.436	3.440	3.450	3.432	٠.	3.438	3.438	3.432	404.0	5.440 4.40	0.440	7.44	7.43	1 416	3.442	3.438	3,438	3.442	3.431	3.452	•	3.440	3.444	5.448	3.458	7.4.5	3.432	3 436	3.427	3,427	3.423	3.419	3.419	3.436	3.423	₹.	3.454	₹.	٠.	3.460
Shaft angle, deg	-14.90 -14.90	ω.	15.66	18.00	-18.00	-20.00	-20.00	9.00	0.00	-2.00	-2.66	9.4	99.4	99.9	•	0 0	10.00	-10.00	-16.66	-12.00	-12.00	4	*	9	-16.00	-18.60 00.01	-18.00	9.0	19.61	10:10	66.5-	00.FI	-6.03	-6.03	-8.07	-8.07	-8.07	-8.03	-10.03	-10.03	•	-11.97
Advance	6.156 6.158	0.150		9 .150	0.150	0.150	0.150	0.200	0.200	0.200	9.200	9.500	907.0	907.0	200	90.200	200	9.200	0.200	0.200	0.200	0.200	0.200	0.200	0.200	0.200	9.200	6.249	0.240	0.248	0.248	9.250	0.251	0.250	0.251	0.250	0.253	0.250	0.251	0.251	0.251	0.249
Rotor speed, rpm	759.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	99.96	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	759.88	/20.00	750.00	754 48	750.16	756.10	749.07	749.30	748.84			749.54	748.61	750.93	751.28	750.93	•	751.28
Collective pitch, deg	ø ø	Ø 6		0.0	0.0	0.0	0 .0	6 .6	9.0	9. 0		9 6	9 6	9 9		9		9	0.0	0.0	0.0	0 .0	6	9.0	6. 6		s 6	9 6		9 6			0.0	•	•	٠	•	o .	0 .0	ø. Ø	0 .0	0 .
Data point number	83223008 83223009	83223011	83223012	83223014	83223015	83223016	83223017	83223018	83223819	83223828	6322362	77077750	8407482	#202220 #2022078	83223023	8322382	83223028	83223029	83223030	83223031	83223032	83223033	83223034	83223835	83223836	63223637	83223838	1402770	83223043	83223044	83223045	83223046	83223047	83223048	83223049	83223050	83223051	83223052	83223053	83223054	83223055	83223056
Rotor	II	11	- L-	:=	II	I	I	I:	Ξ:	:	7 .	.	:		:=	-	: -		II	11	=	I	I:	:	Ξ:	7 .	7.		; <u>-</u>	:=	Ξ	II	11	=	=	II	I:	II	I	ΙΪ	II	=

Damping, 1/sec	-6 .199	Τ.	-6 .176	Τ.	-6 .169	-6 .159	-6 .165	-6 .156	-6.153	-0.158	-6 .156	-6.137	-6.147	-6.150	- 8.151	9. 16 4	-6 .169	-6.167	₹.	-6 .166	-6 .173	-6.180	-0.187	-6 .187	-6. 193	-0.165	571.9	9.188	6.138	9 9	5.5	6.173	-6.165	٣.	. 168	-B.158	-0.192	-9 .166	6.170	-6.161	-0 .161	-6.149	-0 .162	-6 .151	-6.153
Frequency, Hz	3.454	3.452	3.442	3.438	3.427	3.427	3.436	3.411	3.438	3.440	3.444	3.440	3.419	3.450	3.452	3.438	3.454	3.444	3.427	3.440	3.425	3.442	3.452	3.432	3.442	3.444	5.446	5.442	5.442	0.400 0.400	3.442	3,434	3.436	3.446	3.440	3.434	3.434	3.442	3.442	3.440	3.444	3.446	3.425	3.450	3.452
Shaft angle, deg	-11.96	-14.07	-14.07	-14.04	0.02	9.01	90.0	-2.02	-2.02	-2.02	-2.02	-3.99	90.7	4.02	-4.02	-6.00	-5.99 -	-5.99	-7.99	-7.99	-7.99	-7.99	-10.03	-10.63	-10.03	0.02	9.62	5 6 5 7		5 6 5 7	66.5	-6.03	-6.03	-6.03	8.80	-8.02	49.8	-6.65 -6.05		-2.02	-2.02	-3.96	-3.99	-3.99	98.E-
Advance	0.252	0.245	0.248	0.247	0.294	0.295	9.236	0.300	0.301	0.296	0.296	0.300	0.297	0.302	0.298	6.238	0.297	0.295	0.299	0.302	0.299	0.299	0.302	6.303	6.298	0.347	0.540	20 C	0.040	9.336	0.347	0.348	0.348	0.350	0.354	0.351	0.348	0.397	0.395	9.400	0.401	9.400	0.402	0.399	0.399
Rotor speed,	751.16	750.58	749.88	749.30	748.96	749.19	749.77	747.68	750.00	750.00	750.46	750.00	748.38	750.81	750.93	749.65	751.04	750.23	748.49	749.54	748.61	749.88	750.35	749.19	749.77	750.23	750.46	750.08	71.00/	749.00	750.12	749.42	749.65	750.23	749.88	749.19	749.19	750.00	750.00	750.00	750.23	750.23	748.61	750.81	750.93
Collective pitch, deg	0.0	9 .0	9 .	9 .0	0.0	0 .0	ø. Ø	0.0	o .	0.0	9 .0	0 .0	0.0	0 .0	0 .0	9.	Ø.	Ø. &	ø. ø	o . o	9 .	ø. Ø	9 .	9.	9.0	6 0 (s		D 6	9 6	9.0	9.0	0.0	9.0	0.0	0.0	9 .0	0.0	0 .0	o .o	9 .0	0 .0	o .o	0 .
Data point number	83223057	83223058	83223059	83223060	83223063	83223064	83223066	83223067	83223068	83223069	83223086	83223070	83223073	83223074	83223075	852258/6	83223077	83223078	83223079	83223080	83223081	83223082	83223083	83223084	83223085	83223087	63223988	85225889	9507770	83223081	83223093	83223094	83223095	83223096	83223097	83223098	83223099	83223100	83223101	83223102	83223103	83223104	83223105	83223106	83223107
Rotor	11	II	I	II	= :	H	I	II	II	I	H	I	I	I	Ξ;	11	Ξ:	= :		H	H	ij	Ξ:	.	- :	7 1	11	1:	::	7 <u> -</u>	H	11	II	II	I	II	II		II	II	II	II	I	II	11

	Domping. 1/sec	-0.158	-0 .162	┰,	9.17	7.5	6.173	ارد. د ازد	الان الان الان	4.635	6 .237	-6.239	-0.237	-0.236	-0.231	-0.236	9.244	25.25	6.245	247	-0.242	-0.239	-0.241	-0.236	-0 .237	6.229	27.9	6 .229	-0.220	-0 .228	-6.229	877.9	223	-0.260	-0.254	-0.249	-0.252	-0.249	-0.245	6.236	245	243	•
	Frequency, Hz	3.460	3.460	3.436	3.446	3.431	3.431	404.0	3.442	3.423	3.450	3.450	3.465	3.438	3.454	3.425	3.432	3.427	5.4.8	5.4.5 7.4.5	3.429	3.421	3.444	3.429	3.427	3.458 4.48	5.440 4.456	3.419	3.421	3.442	3.436	•	•			3.431	•	•	٠	3.446	0.4.5 8.04.5	3.423	
	Shaft angle, deg	-6.93	-6.03	60. 9	-0·10	-1.99	-1.99	-3.99	00.00 90.00	9.60	60 00 00	86.	-4.62	-4.02	-6.00	-6.02	-7.99	-7.99	-7.99	88. / I	. e. e.	-11.97	-11.96	-13.98	-13.98	-16.01	16.61	10.01	-18.01	-18.01	-18.01	18.61	1.00 P.	-0.03	90.0-	-2.03	-2.03	4.02	7.07		•	0 0 0 0 0 0	•
TABLE 8.—CONTINUED	Advance	9.399	9.400	0.447	0.447	0.451	0.451	6.456	6.448 9.449	- 600 - 600 - 600	9.00	566	9.093	0.093	9 .034	9.634	9 . 0 3 †	9.00	6.694	0.00	\$ 00 G	460.6	969.0	9.00	9.036	0.005	6.695	0 00 00 0 00 00 0 00 00	0.00	9.00	0.697	9.09.0	0.00	6.033 144	٠	: -	_	٣.		9.144	0.147	9.144	o+
TABLE 8.~	Rotor speed,	751.51	751.51	749.54	750.35	749.19	749.30	749.19	750.12	748.95	750.00	750.81	752.09	750.00	751.28	748.84	749.54	749.07	748.61	759.96	90.96/ 61.04/	748.72	750.58	749.42	749.19	750.23	751.04	749.18	748.84	750.46	750.12	750.23	759.40	749.65	AT AT	749.77	750.35	750.58	748.96	751.28	748.84	749.54	19.90/
	Collective pitch, deg	6.	0.0	6 .0	0 .0	0.0	Ø. Ø	9 .	Ø. 6	9.6	9 G	9 6	3.0	9.0	3.0	3.0	3.0	ө .	ю. О	٠ ا	9.4	9 69	9.0	3.0	J. 0	ю. 0	9. P	۵. د ت	9 9 9	9.N	0. 0.	9. e	9 G	9.6		9 e		3.0	3.0	3.0	B. I	9.0	D. C
	Data point number	83223108	83223109	83223110	83223111	83223112	83223113	83223114	83223115	83236163	83236188	83236108	83236109	83236110	83236111	83236112	83236113	83236114	83236115	83236116	8113518	83236119	83236120	83236121	83236122	83236123	83236124	85256125	83236127	83236128	83236129	83236130	02730133	83237882	84247864	83237004	83237005	83237006	83237007	83237008	83237009	8323/010	110/0700
	Rotor		=======================================	Ξ	=	11	1	II	I	⊒:	:	: -	::	: 11	11	11	11	-];	1 -	::		I	II	= :	Ξ:	! !	; <u> </u>	I	H	I	7.	7 F	; <u>-</u>		Π	11	I	1	Ξ:		11

Damping, 1/sec	-0.245	-0.238	-6.236	-0.235	-0 .233	-0.233	•		-9 .223	-0.221	4:4	417.0	9.436	•	•	240	-0.240		-0.236	-0.218	-0.227		-6.229 6.229		-0.220	-0.223	-0.216	-0.215	-0.207 0.207		-0.217	-0.237		•	-9.244	•		٠	•	•	٠	-0.224
Frequency, Hz	3.423	3.419	3.427	3.432	3.425	3.432	3.440	3.421	3.413	3.427	874.0	3.4.2	444	4.54 F	3 449	3.431	3.436	3.436	3.431	3.423	3.423	0.428	5.421	3.419	3.427	3.427	3.419	3.421	3.448 4.45	3 419	3.431	3.431	3.436	3.425	3.427	3.423	3.425	3.429	3.436	3.425	3.434	3.438
Shaft angle, deg	-10.07	-10.07	"	N	-13.93	-13.93	-15.97	-15.97	-18.01	18.61	+ 0 0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	C8:81-	10.0	, a	\$ 65 \$ 67	-10.00	-16.00	-12.01	-12.01	-13.97	-13.97	/B.CI-I	13.5.4 0.00	-16.01	-16.01	-16.01	-18.00	8.08	19.93	50.00	-19.95	-8.08	-8.08	-8.08	-8 -8 -9 -9	-10.04		9	-10.04	-12.01	-12.01	-12.01
Advance ratio	0.146	٣.	Τ.	0.145	0.144	-	٣.		9.148	6.147	- +		105 105			. *-	-	Τ.	Τ.	0.195	0.197	40.0	6.196 405	90.198	0.197	0.195	0.196	9.19/			0.198	0.248	0.244	•	0.248	•	•	•	•	٠	•	0.248
Rotor speed,	749.54	749.07	749.77	750.35	749.77	750.23	751.16	749.42	748.84	750.00	740.55	750.13	749 88	749.19	750.58	750.12	750.46	750.58	750.12	749.65	749.42	710.30	750 01	749.42	750.00	750.00	749.54	749.65	/50.81 751 16	749.42	750.35	749.65	750.23	749.30	749.42	749.30	749.42	749.77	750.35	749.54		750.58
Collective pitch, deg	3.0	3.0	G.0	ы. Ө.	ა. ტ.	ы. Ф.	ю. Ф.	0.1 0.0	9.5 9.0	ا چې و	9 6) M) P.) M	9 69	(S)	9.0	3.0	•				ر ق ق				•	ع. ه. د			3.0	3.0	3.0	3.0	3.0	0. 0.		8.0 0.0	_	0.0 0.0	9. e	9
Data point number	83237012	83237013	83237014	83237015	83237016	83237017	83237018	83237019	8323/828	8323/821	220/CZC0 R4047004	81217024		83237826	83237027	83237028	83237029	83237030	83237031	83237032	83237033	0323/034	8525/835	83237037	83237038	83237039	83237040	8323/041	8323/842	83237044	83237045	83237046	83237047	83237048	83237049	83237050	83237051	83237052	83237053	83237054	8323/835	83237056
Rotor	11	I	I	:	II		I	I :	! :	::	11	11		::	:::		II	II	11	Ι:	II:	1:	:		II	II	II:	.	.		11	II	II	11	Ii		1:	:	⊒ ;	Ξ;	1:	I

Domping, 1/sec	-0.220 -0.220 -0.218	-0.213 -0.213		-6.195 -6.210		96.286		•	-0.200 -0.356		-0.227	-0.240	-6.236 9.339	-0.238	-0.224	-0.220 0.220	-0.220	-0.227	•	•	-0.200	•	∵.	•	9.171	-0.185	•	100	15.0	-6.180	-0.184	•		-9.235	-6 .22/
Frequency. Hz	3.417	3.421 4.421 4.20	3.415	3.446 3.425	3.425	3.425	3.4.8 3.4.15	3.419	3.423	3,419	3,432	3.421	3.409	J. 417	3.432	3.425	3.427	3.421	3.417	3.444	3.434	3.44.2	3.450	3.440	3.440	3.440	3.440	404.5	3.432	3.436	3.442	3.438	3.444	3.444	3.442
Shaft angle, deg	-13.97 -13.97 -13.97	-16.07 -16.07	-16.08	-18.02 -18.02	-18.02	18.62	19.95	-19.94	19.95	27.96 7-	-7.96	-8.83	89.69 80.69	16.63	-10.03	-12.04	-12.64	-12.04	-13.97	-13.96	•	40.01		-16.94	-17.98	-17.98	-17.98	∵	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		19.95	-8.08	-8.08		-10.01
Advance	6.251 6.249 6.244	6.248 9.248		0.247		6.251	0.245 0.245	0.241	9 .246	0 . 296 0 . 298	0.293	0.295	9 .295	6.384	6.299		9 ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° °	0.299		•	6 .298	e .361	9.299	0.299	6.300	6.301	0.296	0.297	6.361	650.6	•		•	0.346	0.346
Rotor speed,	749.19 749.54 749.88	749.54	748.96	751.16	749.42	749.65	748.61	748.84	749.07	748.72	749.77	748.84	747.91	748.72	750.00	749.42	749.12	749.19	748.84	750.93	750.12	750.46	758.93	750.23	750.23	750.00	750.12	749.77	740.93	749.63	749.88	759.12	750.58	750.58	750.70
Collective pitch, deg	0 0 0 0	9 O 6	9 69 69	က က စ စ	90	9 6 9 P	0 0 0 0	0°	ю. 6	9 G	3.0	3.0 9.	9.6) N	3.0	0.0 0.0	9 G	9.0	3.0	a.0	ю. 0.0	9 e	9 6	9.0	3.0	J.0	0.0 0.0	9.0 9.0	9 6	9 6	9 6	9.0	3.0	3.0	3.0
Data point number	83237058 83237059 83237060	83237062 83237062	83237064	83237065 83237066	83237067	8323/868	83237070	83237071	83237072	83237076	83237077	83237079	83237080	83237082	83237083	83237084	83237085	83237087	83237088	83237089	83237090	8323/891	83237093	83237094	83237095	83237096	83237097	83237098	880/5750	83237101	83237102	83237103	83237104	83237105	83237106
Rotor		==:	111		:П;	7.	III	II	II	- I -	I	II	Ξ:	11	II	Ι:	11		II	II	II:] <u>:</u>	- F	II	II	11	I	.	11		:	II	11	II	I

Rotor	Data point number	Collective pitch, deg	Rotor speed, rpm	Advance	Shaft angle, deg	Frequency, Hz	Damping, 1/sec
_	83237107	9.0	750.12	0.350	-10.00	3,436	727
,	83237108		4	M	6	•	•
_	83237109	9	750.58	0.348	-12.04	•	95.4
	83237110	9.6	750.23	0.353	,,,		101.6
_	83237111	9	749.65	9.344	: 5	429	. e
	83237112	6 m	759.78	•	! 7	•	1.6
		9 6	751.16		• •	•	9 4
	· -	9.0	750.93	• •	*	•	4 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
-	_	9.0	749.42	0.351	4		166
_	-	9.0	750.81	•	9		-6.179
_	83237117	3.0	750.00	•	6	3.442	-e.155
_	83237118		750.12	•	-16.04	٦.	-0.175
_	83237119	3.0	750.23		-18.01	•	-0.186
 .	83237120	3.0	750.93	0.349	-18.01	•	-e.17e
_	83237121	3.0	751.04	0.349	-18.01	٦.	-6.195
	83237122	J.0	751.39	0.349	-18.01	3.461	-0.188
_	83243003	6.0	749.65	960.0	-11.99	•	-0.421
— ,	83243004	9. ₉	750.81	0.095	CA.	3.444	-0 .432
	83243005		749.65	0.093	Ξ.	•	-0.432
<u>.</u>	83243006	0 .0	750.35	0.095		•	-0.429
	83243007	Ø.	750.23	0.093	K)	•	-0.427
.	83243008	9 .9	750.81	0.095	W)	٠	-0.430
	83243009	9.	749.54	0.095		3.427	-0.422
	83243010	ල ·	749.88	•	-17.97	•	-0.432
	83243011	o.	750.58	0.093	-20.00	•	-0.422
	83243012	Ø.	750.23	0.004	-20.00	3.436	-0 .454
	83243013	9.9	750.12	0.145	in	۳.	-6.435
	83243014	Ø. Ø	750.46	Ξ.	-15.97	•	-0.445
	83243015	ø.ø	749.42	▔	-18.01	3.427	-0.440
	83243016	ø. ø	750.46	9.148	-18.02	•	-0.427
	83243017	ø.ø	751.39	0.145	-20.00	•	-0.429
	83243025	6.9	748.72	0.146	-20.00	•	-0.429
	83243026	6.9	748.84	0.148	-20.00	•	-0.430
	83243018	6.9	749.65	•	-16.01	•	-0.435
	83243019	6.6	750.00	0.196	-16.01	3.434	-0.431
_	83243020	6.9	750.00	0.197	-16.01	•	434
	83243021	6.6	750.23	0.197	-18.05	3.432	-6.436
	83243022	6.0	749.19	0.195	-18.05	•	-0.429
_	83243023	9	30 072	4			
			۰	. J 200	-20.00	3,417	420

TABLE 9. -- REGRESSING LEAD-LAG MODE DATA IN FORWARD FLIGHT, CONFIGURATION WITHOUT STRUCTURAL FLAP-LAG COUPLING, 1000 RPM

Damping, 1/sec	-0.164	-8.163	26.6	- 161 - 161			٠.	-0.162	-0.160	-0.161	-0.162	- 9 .160	-6.158	-6.157	2 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	-6.157	9.13	ا ا ا	80 F	- Par)	9 9	9 9	9	9 - 69	167	9.16	-6.168	٦.	٣.	┪.	Ξ,	Ξ,	9.104	401.9	92.98	9/1.9	∵`	•	9 6	997.9	9 - 6	286	7.70
Frequency, Hz	6.428		6.426	6.422 6.422	6.405		6.438		6.432	6.432	•	6.422	•	6.430	٦.	6.430	6.424	6.411	6.428	6.441	404.0	6.436 A46	0.4.0	6.422	6.428	6.420	6.414	6.4.3	6.443	6.432	6.418	6.428	6.420	6.438	6.430	6.438	6.443	6.447	6.426	6.428	6.418	4.4.0	0.432	4.4.0
Shaft angle, deg	0.02	0.02		/B. I	70.4	46	16.4		-8.63	-10.00	-19.00	-11.97	-11.97	4	-14.00	-16.04		-17.98	-17.98	-19.64	40.61-	9 6	99.0	9.0	9 6	10.2	10.2- 80 F.	86.5	96. 66.	-5.96	-5.96	-7.99	-7.99	-10.00	-10.00	-12.04	-12.04	2	-13.96	-13.96	-16.01	<u>.</u>	~ I	16./1-
Advance	9.044	0.042	0.043	9.044	6.04	9.0	944	0.045	0.044	9.044	9.044	9.044	0.043	0.043	0.043	0.043	0.043	0.043	0.043	0.043	0.043	6.697	8.035	6.095	6.695	6.030	60.00	700.0	20.0	6.097	860.0	660.0	660.0	660.0	0.097	0.097	0.097	0.097	6.097	0.097	0.097	0.097	969.0	6 .696
Rotor speed,	69.666	1000.62	999.34	999.23	08.788 09.700	99. Vee	1000	999.92	1000	1000.15	999.81	999.34	999.34	1666.64	999.92	999.92	999.46	998.41	999.81	1000.85	1000.15	1000.04	11.000	999.57	999.34	26.666	888.00 000 000	90.000	1001	1969.27	998.99	1000.04	999.34	1000.85	1000.27	1000.97	1001.43	1001.55	999.46	69.666	998.88	998.53	1000.04	998.53
Collective pitch, deg	9	9.9	0.0	o o			9 6						9.0	0 .0	0 .	0 .0	9 .	9 .	0 .0	0 .0	9 .	6 .6	9.0	9 .6	9 .0	9 (s 6	9.6	9 6	9 9	0.	9.0	9 .0	0.0	•	0.0	•	٠	0.0	0.0	0.0	0 .0	0.0	0. 0.
Data point number	83223120	83223121	83223122	83223123	63223124	63223123 83223123	0212220	83223127	83223129	83223130	83223131	83223132	83223133	83223134	83223135	83223136	83223137	83223138	83223139	83223140	83223141	83224004	83224005	83224006	83224029	83224007	83224008	82224688	81224010	83224012	83224013	83224014	83224015	83224016	83224017	83224018	83224019	83224020	83224021	83224022	83224023	83224024	83224025	83224026
Rotor	11	II	II	Ξ:		7.	7 -] [1 F	:=		II	Ξ	11	===	11	II	11	11	11	II	I	I	I	II	= ;	Ξ:	-	; :	::	I	II	=======================================	Ξ	II	11	II	II	II	II	11	II	II	II

83224027 83224028 82263003 82263005 82263017 83224033	pitch, deg	Rotor speed,	Advance	Shaft angle, deg	Frequency, Hz	Domping. 1/sec
83224028 82263003 82263005 82263017 83224032	0.0	23. 52	969.0	-19.64	6.426	-0.204
82263005 82263005 82263017 83224032	0.0	999.11	0.095	-19.65	6.429	-0.204
82263005 82263017 83224032 83224033	0 .0	1666.68	0.149	0.00	6.639	-6.194
82263017 83224032 83224033	9 .0	1001.13	0.142	0.00	6.639	-6 .179
83224833	6 .6	999.38	0.149	0.00	6.639	•
63224633	9.0	998.30	0.148	9.00 0.00	6.412	-6.176
04570070		1888.84	6.148	99.69 00.69	6.434	הַ י
63224636	s e	1666.13	9.146	9.62	6.434	<u> </u>
80947700	9 6	70.000	- •	- œ-	6.428	•
82263884		1000.01	9 4 4 6	99.7	0.032 6.653	- •
8226360	9 9	1000.000	- •	2.66	6.632	
0100770	9.6	1000.00	. •	98.7-	90.0	•
65224654	s 6	1999.27	9.140	-2.62	•	-6.169
63224633		1000	90.10	-2.62	6.4.0	60.00
82263007		1666.68	9.148	99.	6.639	•
8226368	9 (988.80	9.148	99.	6.639	-6 .172
82263019	S	1998.88	9.149	-4.00	•	•
83224836	s 6	40.000	9.136	-4.62	•	- P. 165
63224637	9.0	70.000) - C	79.4	6.428	Ξ,
8225508		98.80	9 4	9 9	6.639	9.1/2
82263626	9 6	10001	9 1 4	99.9	90.0 914.0	9 9
83224038	9 6	1000.97	9,159	96.	6.443	162
83224039	0.0	1000.39	-	55 56 56 56 56 56 56 56 56 56 56 56 56 5	6.438	-6.176
83224040	0.0	998.41	0.148	-5.99	6.414	. –
83224041	0.0	999.92	0.148	-6.00		-0.162
82263010	0.0	1000.43	0.149	-8.00	6.639	-6.177
82263022	0.0	999.84	0.147	8.00	6.639	-0.175
83224042	6 .0	999.46	9.148	-7.99	6.424	-6.173
83224043	0 .0	999.46	6. 148 8	-7.99	6.428	-6.178
82263011	ø.	999.84	0.149	-10.00	6.639	-6 . 198
82265825	•	00.000	84.	-16.66	•	-0.130
63224644	•	1001.03	9.140	16.65	•	9.183
01017700	9.6	07.000	• • • • • • • • • • • • • • • • • • •	16.63	0.420	9.10
21000000	5 6	00.000	n 0	12.66	6.638	/97.9-
6220264 63224646	•	1000.31	0 4	12.66	•	797.9
03224646	9 · ·	1000	- 1	19.71	٠	•
83224047	•	1000.27		-12.68	5.438	•
03224040	٠	1900 13	- `	00.71-	0.450	•
62263013		1000.78	6.140 6.140	99.4	6.658 6.658	
62263623	٠	1000.00	. •	14.00	•	217.9
03224043	•	1999.13	7	14.00	0.430	/97.a
83224838	•	- 00 000 00 000 00 000	0 · 1 • 0	99.4.	6.432	•
4105250	9.0	97.555 550	. 	٠	9.0°0	•
97793079	9 (e	00.00	0.14/	99.91-	6.652	9.219

	Damping, 1/sec	-0.202	-0.205	9.216	20.212	200	-0.207	-0.201	-0.209	-9.206	100					╌`	-6.186	9 7 8	-6.167		-0.185	-0.178	-6.164 6.164	9 - 67	-6.198	-0.185	-0.166	-0.182 9.171			-6.205	-0.206 -0.206	•		•		•	•	-6.211	-0.212
	Frequency, Hz	6.440	6.639	6.648 843	6.432	6.424	6.639	6.658	6.447	6.438	6.628	0.040	6.664	6.428	6.434	6.668	6.650	6.638	6.428	6.660	6.656	6.646	6.451	6.422 6.653	6.643	6.646	6.422	6.432	٠	6.639	6.656	6.662	0.040	6.443	6 432		•	٠	•	6.424
	Shaft angle, deg	-16.03	-18.00	-18.00	13.66	90.71	-26.66	-20.00	-19.64	-19.64	9 6 9 6	9 6		9.62	0.02	-2.00	-2.99	-2.00	98.7-	86. 7 7	98.7	-4.00	-3.95	DD 9	90.9	-6.00	-5.99	-5.99 8.99	יים היים היים היים	8 . 8 . 8 .	-8.00	89.69 8.69	9 .00	86. 7-1	66.7	86.7- 99.7-	-10.00	-10.00	-10.00	-10.03
9CONTINUED	Advance	6.148	0.148	0.148	6.148	74.0	. 6 1. 40 0 84	6.148	0.147	Ξ,	0.202	90.00	97.90	0 0	0.197	0.200	6.199	6 .198	9.201	0.201	0.201	0.200	0.199	6.199	9.20	0.199	0.201	6 . 199	6.201 9.408	6 .201	0.199	0.200	0.200	9.201		90.00	0.202	0.199	•	6 .199 6 .201
TABLE 9	Rotor speed, rpm	1000.62	989.84	999.84	999.81	57.666	999 999 88	1000.43	1001.20	1000.39	1000.55	999.84	2/.1991	990.10	999.92	1001.25	1000.55	1001.13	988.88	1000.40	1000.90	1000.20	1001.43	998.86	000 40	1000.08	998.99	999.92	998.76	999.02	1666.78	1001.25	98.86	999.11	900 60	80.08 75.000	1001.13	96.666	939.56	998.88 998.88
	Collective pitch, deg	0.0	0 .0	0.0	9 .0	S 6		9 6	0.	0 .0	0 (0	9.0	s 6	9 6	9.0	0.0	9 .0	© (s	9 6	9 9	0.0	0.0	6		9	6.6	9 .0	S. G	9 0	0.0	0 .0	9.	6	e e		9	0.0	0.0	0 0 0 0
	Data point number	83224052	82263015	82263027	83224053	83224854	82224855	82263028	83224056	83224057	82263029	82264001	82264002	83224063	83224064	82263030	82264003	82264004	83224065	82263031	82264005	82264007	83224067	83224068	82263832	82264009	83224069	83224070	83224071	82263033	82264010	82264011	82264012	83224073	032240/4	83224075	82263034	82264013	82264014	83224 <i>0</i> 77 83224 <i>0</i> 78
	Rotor	11	-	-	Ξ:	⊒:	≓ ⊢	• •	II	11	н,	щ,					H	-	F	 	• ⊷		II		F-	• •	II	II	- :	- I			⊣ ;	I.	7 1	<u> </u>	•			

Damping, 1/sec	-0.196	-6 .199	-0 .213	-0 .208	-0.206	-0.200	-0.202	-0 .211	-0.209	-0 .195	-9 .200		-6 . 199	- 6 . 199	- 6 .195	-0.201	. 188	-8.194	-0.205	-0.192	-0.201	-0.179	-0 .189	٠.		٠.	-0 .182	∹	٠.	٦.		٠.	٣.	٠.				-6.177	-0 .187		-6.177	Τ.	-0 .172		-0.190	-0.160
Frequency.	6.428	6.674	6.648	•	999.9	6.426	6.418	6.432	6.426	6.652	6.652	6.656	6.652	6.422	6.412	6.440	6.438	6.648	6.650	6.652	6.656	6.432	6.436	6.432	6.438	999.9	6.682	6.658	6.670	6.662	6.658	6.672	6.668	6.650	-	6.432	6.445	6.434	6.650	6.646	6.445	6.426	6.445	6.669	6.641	
Shaft angle, deg	-10.03	-12.00	-12.00	-12.00	-12.00	-12.02	-12.02	-12.02	-12.02	-14.00	-14.00	-14.60	-14.00	-14.00	-14.00	-14.00	-14.00	-16.00	-16.00	-16.00	-16.00	-16.01	-16.01	-16.01	-16.01	-18.00	-18.00	-18.00	-18.60	-20.00	-20.00	-20.00	-20.00	0 .00	9.00	0.02	0.02	0.02	-2.00	-2.00	-2.06	-2.06	-2.06	-4.00	-4.00	-3.99
Advance ratio	0.199	•	0.198	•	٠	0.197	•	0.201	0.200	0.202	0.199	0.199	6.	0.199	٠.	0.198		0.202		0.200	0.199		0.197	0.199	0.200	0.200	6.197	0.199	6.200	0.202	٠	٠	0.197	0.251	•	•	•	0.249	0.250	0.251	0.248	•	•	0.250	0.250	
Rotor speed,	999.11	1001.60	1000.20	1000.20	1001.60	999.34	998.53	999.57	999.11	1000.08	1000.43	1000.78	1000.55	998.99	998.07	1000.27	1000.15	999.49	96.666	1000.08	1000.43	999.46	999.81	999.57	999.92	1000.31	1001.84	1000.08	1001.13	999.61	999.73	1000.66	1000.43	1000.08	999.61	999.92	1000.97	1000.04	98.86	999.84	1000.97	999.23	1000.97	1001.02	989.26	999.92
Collective pitch, deg	0.0	0.0	0 .0	0 .0	0 .0	9 .0	0.0	0.0	0.0	0.0	9 .0	0.0	0 .0	9 .0	0.0	0.0	0.0	Ø.0	0.0	0.0	0.0	0.0	0.0	0 .0			0.0	•	0.0	0 .0	•	•	9.0	9 .0	9 .0	0.0	•	0.0	0.0	0.0	0.0	0.0	9.0	0.0	9	9.0
Data point number	83224079	82263035	82264015	82264016	82264017	83224080	83224081	83224082	83224083	82263036	82264018	82264019	82264020	83224084	83224085	83224086	83224087	82263037	82264021	82264022	82264023	83224088	83224089	83224090	83224091	82263038	82264024	82264025	82264026	82263039	82264027	82264028	82264029	82264030	82264031	83224094	83224095	83224096	82264032	82264033	83224097	83224098	83224099	82264034	82264035	83224100
Rotor	11	1	-	-	-	11	11	II	11	-	н	H	-	11	=	=	11	-	-	-		II	11	II	Π	-	-	-	-	-	-	-	-	-			II		H	Н	II	II	II	_	-	ï

Data point number	Collective pitch, deg	Rotor speed, rpm	Advance ratio	Shaft angle, deg	Frequency, Hz	Damping, 1/sec
81224870	G	999 11	90,199	-10.03	6.428	-0.196
82263835	9	1001.60	0.203	-12.00	.67	-6.199
82264015	9.0	1000.20	0.198	-12.00	6.648	-0.213
82264016	0.0		0.200	-12.00	6.648	-0 .208
82264017	0.0	1001.60	0.199	-12.00	6.666	-0.206
83224080	0.0	999.34	0.197	-12.02	6.426	-0.200
83224081	0.0	998.53	0.201	-12.02	6.418	-0.202
83224082	0.0	999.57	0.201	-12.02	6.432	-0.211
83224083	9.0	999.11	0.200	-12.02	6.426	-0.203
82263036	0.0	1000.08	0.202	-14.00	6.652	-0 .195
82264018	0.0	1000.43	0.199	-14.00	6.652	-9 . 200
82264019	9	1999.78	0.199	-14.00	6.656	-0.196
82264020	9 9	1000.55	0.198	-14.00	6.652	-B. 199
81224084	9 6	66.866	0.199	-14.00	6.422	-0·199
0.22.2400.4 0.42.2400.4	9 6	200	197	-	6.412	-e. 195
0077770	9 6	10.000	801	٠4	6.440	192.61
007774000	9.6	1000.1	9 6	90.41	A 4.38	9
65224667	9.0	900.13	0.00	٧ ٢		40.
82265057		n +	0.207 0.204) Ľ	9.0	20.20
82264821		00.000	90.200) Œ	6.652	192
2704077	D 6	1000.00	20.00	œ	6.656	-6.201
67040770	9.0	000 46	. 6	9	6.432	-0.179
03224000	9 6	999.40	200) W	6.436	-6.189
807776	9	55.000	601	(0	6.432	-6.199
027774030	9.6	0000	. 6) C	6.438	-6.187
0222403	9.0	20.000 11.000	200.0	18.00	6.666	180
62263636	9.0	10.000	0.700	3 0	6.583 6.883	4 183
82264624	9.0	1000	9 6	3 α	6.62	40.0
82264825	9	1001	0000	3 Q		4
82264026	S (1661.13	007.0	90.00	0.07 6.05	9
82265859	9.0	0.00	707.0	90.00		473
82264027	9 (000. 000.	907.0	99.00	6.030 8.73	10.1
82264628		1000.00	00.0	90.04	2.0.0 8.0 8	9. 4
82264629	9.0	1000	7 - 0	90.07		9
82264030	s (1666.68	0.73	9	6.03	9 9
82264031	9.0	10.000	907.0	99.9	٠	9.100
83224094	ø.	999.92	9.529 9.510	9.67	0.432	9
83224095	® .	1666.97	6.248	9.95	•	10.
83224096	9.0	1000.04	0.249	0.02	6.434	7/1.6
82264032	0.0	96.666	•	-2.00	6.650	-0.187
82264033	0.0	999.84	•	-2.00	6.646	-6 . 180
83224097	0.0	1000.97	•	-2.06	6.445	-0.177
83224098	8	999.23	•	-2.06	6.426	-0.166
83224099	0.0	1000.97	•	-2.06	6.445	-0.172
82264034	9	1001.02	•	-4.00	6.660	-0 .189
82264035	9	92 666		-4.00	6 641	961.90
					•	

Damping, 1/sec	-0.165 9.145	- 1	Ξ.	-0.192	-0.196	-0.183	-0.185	-0 .182	-0.200	-0.198	-0.207	-0 .200	-0.202	-0.201	-0.195	-6 .195	− 0.195	-6 .182	-6.18 4	• •	•	-0.224	٠	•	• • •	٠. ٠	-e-183	-6.18/	25.9	9 0	9 4	9 6		-6.181	-6.184	-e. 195	-6.182	-0.176	-6.184	-0.184	-6.175	-B. 177	-0.166	-0.172	
Frequency, Hz	6.428	8.434 434	6.648	6.648	6.664	6.436	6.424	6.428	8.666	6.672	6.436	6.428	6.422	6.639	6.639	6.639	6.639	6.641	6.662	6.639	6.639	6.639	6.672	6.639	6.639	6.639	6.639	6.432	6.424	0.470	0.430 A 4 4 4	A 445	6.441	6.434	6.424	6.432	6.432	6.445	6.639	6.639	6.436	6.434	6.441	6.434	
Shaft angle, deg	13.99 90.1-	6 6 F	-6.00	98.99	-6.00	-5.92	-5.92	-5.92	8.89	8.00	8.00	8.00	-7.99	-16.66	-10.00	-12.00	-12.00	-14.00	-14.00	-16.00	-16.00	-18.00	-18.00	-20.00	-20.00	9.00	9.00	6.62	9.0	99.9	0 6	9	8) e	6.6	6.6	-0.04	40.0	-2.00	-2.60	-2.62	-2.62	-2.62	-2.02	
Advance ratio	0.250	0.23 0.25	0.250	9.259	0.250	0.250	0.249	0.251	0.250	0.249	0.251	0.248	0.248	0.250	0.254	0.252	0.252	0.252	0.252	0.250	0.250	0.252	0.253	0.250	6.259	9.301	9.301	0.297	6.299	87.0	787.0 800. 8	0.730	0.297	0.298	0.302	9.301	6.298	0.300	0.300	0.301	0.301	0.299	0.299	0.300	
Rotor speed, rpm	999.34	1000 DA	999.73	999.73	1000.90	1000.04	999.11	999.34	1666.98	1661.48	1000.04	999.34	998.65	1000.55	999.84	1000.90	999.84	998.32	98.86	1000.90	998.55	1000.20	999.38	1000 . 66	1666.96	999.73	40.000	18.888	30 C C C C C C C C C C C C C C C C C C C	988.	1000.57	1000.02	1000.73	69 666	998.76	99.46	1666.15	1001.20	96.666	1000.20	1000.04	999.81	1000.62		
Collective pitch, deg	0.6	9 6	0.00	0.0	9 .0	ø. Ø	ø. Ø	9 .0	9 .	ø. Ø	9 .	0 .0	0 .0	0 .0	0 .0	9 .0	9 .	9 .	ø. Ø	0.0	9 .0	0.0	0.0	©	9.0	9.0	9 G	s 6		9 9		9	9 9	0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Data point number	83224101	83224103	82264036	82264037	82264038		83224105	83224106	82264039	82264040	83224107	83224108	83224109	82264041	82264042	82264043	82264044	82264045	82264046	82264047	82264048	82264049	82264050	82264051	82264652	62264033	40040770	02724110	82004110	87224114	83228065	83228006	83228007	83228008	83228009	83228010	83229004	83229005	82264055	82264056	83224114	83224115	83224116	83224117	
Rotor	II		-	-			II	II	-	-	II	I	I.	⊢ 4 1			-	-		н,	-	н.	→•	⊶ ,	→ •	F-	٦ <u>:</u>	7.	:				ij						-		II		II	11	

Domping, 1/sec	478	9 4	7.	٠.	-6.187	a 185	. 163	6.171	9.170	-6 .160	-0 .204	-0.201	- 6 .185	-0.196	-9.199	- 6 .199	- 6 .193	-0 .196	-0 .202	-6 .203	-0 .207	-0 .202	-6.197	-6 .185	-6 .191	- 6 . 189	-6.193	-0.244	-0.242	-6 .308	− 9.277	-0.274	-6 .293	-0.293	-0.326	.348	-6 .215	. 181 181	-0.212	-6 .194	-0.195	-6.197	-6 .183	-0.194	-B.189	-0 .188
Frequency, Hz	8 414	4.5	A 4.30	6.445	6.639	6.639	6,445	6.440	6.434	6.434	6.639	6.639	6.424	6.428	6.430	6.422	6.440	6.639	6.639	6.449	6.445	6.457	6.451	6.639	6.639	6.639	6.639	6.639	6.639	6.684	6.639	6.639	6.639	6.639	6.639	6.639	6.639	6.639	6.639	6.639	6.424	6.428	6.426	6.418	6.639	6.635
Shaft angle, deg	-2 83	-2.52	-2.62	-2.02	8.7	8.	14.01	1.01	1.9	1.01	99.9-	98.99	-5.96	-5.96	-5.96	-5.96	-5.96	98.89	-8.90	-7.99	-7.99	-7.99	-7.99	-10.00	-16.66	-12.00	-12.00	-14.00	-14.00	-16.00	-16.90	-16.00	-18.99	-18.90	-20.00	-20.00	0 0.00	9.60	00.00	00.00	-6.61	6.61	-0.02	-6.62	-2.00	-2.00
Advance	300	300	0.299	0.301	9.300	0.302	0.300	0.299	0.297	0.297	0.299	0.298	0.298	0.300	0.298	0.300	0.297	0.299	0.299	0.300	0.297	0.299	0.300	0.299	0.299	6.300	6.23	0.300	0.299	0.301	6 .299	0.297	•	0.295	•	9.301	0.350	0.348	0.350	0.353	0.346	0.350	0.350	0.349	0.351	0.352
Rotor speed,	997 95	35.000	999.23	1999.59	999.84	986.38	1666.56	999.92	989.46	939.46	1000.08	1666.26	998.53	998.88	998.99	998.41	1000.04	1000.08	1000.43	1000.73	1000.73	1001.43	1000.85	1001.13	1000.43	1001.37	1001.84	98.86	999.38	999.84	1000.43	1000.20	1001.13	1991.69	999.84	98.86	1000.08	1000.43	1661.48	1666.68	999.46	69.666	999.57	998.88	999.84	998.32
Collective pitch, deg	G		9 6	0.0	0.0	0.0	0.0	9.9	0.0	0.0	0.0	6 .	6 .0	0 .0	0 .0	0.0	0.0	0.0	6 .0	0.0	6 .6	0.0	0.0	0.0	0.0	9 .0	9 .	0 .0	ø. Ø	9 .	6 .6		•	0.0	.	9 .0	ø. Ø	0.0	0.0	0.0	0.0		0.0		9.0	0.0
Data point number	81008011	81228011	83228013	83228014	82264057	82264058	83228015	83228016	83228017	83228018	82264059	82264060	83228019	83228020	83228021	83228022	83228023	82264061	82264062	83228024	83228025	83228026	83228027	82264063	82264064	82264065	82264066	82264067	82264068	82264069	82264070	82264071	82264072	82264073	82264074	82264075	82264076	82264077	82264078	82264079	83229006	83229007	83229008	83229009	82264080	82264081
Rotor	11	-	:-	H	-		II	11	11	11	н	-	II	11	Π	II	II	-		11	II	Π	11	н	-	-	-			—	-	—	-	.	_	I	-	-	г	П	11	II	II	II	 4	-

Damping. 1/sec	-0.187	-6 . 183	-6.180		- 6 .185	٣.	-6.183	-6.175	-0.184	-0.186	-0.203	-0.202	-0.193	-6.192	-0.203	-0 .211	-0 .200	-0.200 -	-0.225	0 .237	9.218	-6.220	-0.325	-6.327	6.375	-0.347	16.398 1.398	9.413	-6.363	-6.383	654.99 654.99	9 . 4	+ n+ n	9.45	0.00	957.9	77.9		-6.19&	•	-0.202	-6.208	-0.223	9.206	-0.187	-6.194
Frequency, Hz	6.424	6.422	6.434	6.434	6.637	6.639	6.424	6.430	6.422	6.455	6.639	6.639	6.416	6.424	6.428	6.422	6.639	6.639	6.639	6.639	6.639	6.639	6.639	6.639	6.639	6.686	6.695	6.691	6.689	6.701	6.695	6.71	6.721	0.740	0.040	D . 0	6.632	6.428	6.424	6.441	6.451	6.637	6.643	6.418	6.412	6.428
Shaft angle, deg	-1.99	-1.99	-1.99	-1.99	90.7	90.7	4.02	4.03	4.03	4.03	99.9	90.9°	-5.98	-5.98	-5.98	-5.98	-8.00	98.89 F	-10.00	-10.00	-10.00	-10.00	-12.00	-12.00	-14.00	-14.00	-16.00	-16.00	-16.00	-16.00	-18.66	-18.00	-26.66	99.92-	9.00	9.00	90.0	99.9	0.00	00.00	6 0.00	-2.00	-2.00	-1.99	-1.99	-1.99
Advance	0.350	0.351	0.350	0.349	0.351	0.349	0.352	0.349	0.348	0.347	0.349	0.351	0.349	0.351	6.349	0.351	0.351	0.350	6.351	0.352	6.349	9.348	0.349	0.350	0.320	0.349	0.351	0.350	9.350	6.350	0.350	6.356	9.548	6.348 5.68	904.0	86.0	9.400	6.397	0.396	0.397	0.398	9.491	0.403	0.401	0.400	0.400
Rotor speed,	999.23	999.23	1000.27	1666.64	998.67	1000.31	999.34	69.666	999.11	1001.90	1000.43	999.84	998.65	69.666	69.666	998.99	1000.43	1000.20	1000.55	1000.08	1000.90	1001.25	1000.08	999.84	999.49	1000.66	1000.55	1000.43	1000.20	1000.90	900.000	1000.20	1666.43	1662.38	1666.28	77.000	1000.55	999.11	999.46	1000.85	1001.55	999.02	999.49	998.65	998.18	989.46
Collective pitch, deg	0.0	0.0	0 .0	0 .0	9 .0	.	0 .0	0 .0	0 .0	9 .	9.0	0 .0	0 .0	9 .	9 .	9 .	0 .0	9.0	0 .0	9 .	0 .0	0	0.0	0.0	6	0.0	0.0	0 .0	0 .0	6 .0	9.0	9.0	9.0	S	9.0	9.0	9.0	9.	0	0 .0	9 .	0.0	0.0	0 .0	0.0	9 .0
Data point number	83229010	83229011	83229012	83229013	82264082	82264083	83229014	83229015	83229016	83229017	82264084	82264085	83229018	83229019	83229020	83229021	82264086	82264087	82264088	82264089	82265001	82265002	82265003	82265004	82265005	82265006	82265007	82265008	82265009	82265010	82265011	82265012	62265013	\$2265614 \$2066914	0.002220	01000770	7186779	83229022	83229023	83229024	83229025	82265018	82265019	83229026	83229027	83229028
Rotor	11	I	=	11	-	-	II	I	11	11	-	-	=		I		-	-	 :	-	-	- 4 :	-	 4 (1	.	-	 .	 .	⊢ ,	⊸ •	→ ►	→•	- -	→ .	→ ト	→ ;		H :	I	I	-			II	

Domping. 1/sec	-0.207	-0.208	-6.198	9 9	4 5 5 5	. e	-0.213	-0.214	-0.218	-6 .219	•	-0.318	-6 .392	-0.374	-6 .358	-0.462	4.47	-6.471	-6.237	-0.236	-6.221	-0.243	9.216	/17.9-	+17.9	207.0	4.22/	7 9 9	9.201	-0.205	-0.201		-6 .195	-9 .191	-0.199	-0.200	-0.208	-9.261	-0.272	417	- 9.4 63	٠	٠	-0.477
Frequency, Hz	6.436	6.670	6.654	0.4.0 8.4.8	8 4 4 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	6.440	6.643	6.648	6.641	6.645	6.643	6.650	6.682	6.688	6.701	6.688	6.717	6.705	6.658	6.646	6.438	6.430	404.0	400.0	0.00	0.00.0	0.632 6.413	201.0 87.4	6.426	6.666	6.654	6.428	6.430	6.441	6.434	6.658	6.656	6.674	6.658	6.678	6.689	6.699	6.699	6.695
Shaft angle, deg	-1.99	96.7	99.7	8 S	, T	60	90.9-	-6.90	-8.00	8.00	-10.00	-10.00	-12.00	-12.00	-14.00	-14.00	-14.00	-16.00	0.00	•	0.61	00.00	9 (-2.ee	2.00	2.66	-2.00 -1.07	٠	60.	90.+	90.7	10.4	4 . 6	14.04	+ 0. + -	-6.00	90.99	-8.00	98.99	-10.00	-10.00	-12.00	-12.00	-14.00
Advance	0.398	6.399	6 - 4 - 6 - 6 - 6 - 6 - 6 - 6 - 6 - 6 - 6 - 6	0.+02 401	. e	9.396	6.401	9.400	9.402	6.401	0.402	9.403	6 .462	0.402	9.401	6.399	9 . 4 00	0.396	6.456	0.451	6.449	9.448	6.447	6.4.0 6.4.0	04.40	4.40	6.43	0 45.	6.49	0.452	0.450	0.451	0.453	0.448	0.449	9.450	0.449	0.453	0.451	0.447	0.449	0.450	0.450	0.451
Rotor speed,	1000.04	1001.72	1888.43	1999.13	1000.01	1000.27	800	1666.68	999.02	999.38	998.55	998.91	1000.66	1000.90	1666.31	999.26	1001.37	999.73	1000.43	999.49	999.57	999.69	888.68	1999.98	19.88	000	7	70.00	000	1000.56	999.61	899.57	999.57	1000.39	999.92	1000.55	1000.20	1000.78	999.49	1000.08	1000.55	1000.43	1000.43	998.44
Collective pitch, deg	0.0	0.0	9.0	9 6	9 6		9 6		0.0	0.0	0 .0	6 .6	6 .0	6 .6	0 .0	6 .6	0 .0	6 .0	6 .0	0.0	0 .0	9	9.0	9 .0	9.0		9 6	D 6)	9	9.9	6 .6	0.0	0 .0	6 .0	6 .0	6 .	ø. ø	0 .0	0.0	0.0	0 .0	0.0	0.0
Data point number	83229029	82265920	82265921	83229838	0777001	83229833	8226502	82265023	82265024	82265925	82265026	82265027	82265028	82265029	82265030	82265031	82265032	82265034	82265035	82265036	83229035	83229036	83229037	82265037	82265038	82265839	82265040	020778020	81229839 81229848	82265041	82265042	83229042	83229043	83229044	83229045	82265043	82265044	82265045	82265046	82265047	82265048	82265049	82265050	82265051
Rotor tested	11	H	۰:		7 -		-	• •	—	—	-	-	-	-	-	H	-	-	-		II		I '	⊷ •	⊶•	>	<u>-</u> -		<u>.</u>	-		II	II	II	II	—	-	-	-	-	-		_	-

Rotor	Data point number	Collective pitch, deg	Rotor speed, rpm	Advance	Shaft angle, deg	Frequency, Hz	Domping, 1/sec
	RODESASO	9	9000	977		ACT A	0
•	82265053		1000.70	400	90. 4 4	0.72 888 888	96.5
	82265054	9 6	1990.75	9 6		9.00	-8 246
	82265055	6	0000		- S	6.654	21.4
_	82265056	0.0	1666.26	9.591	-2.60	6.662	-0.244
_	_	0.0	41.666	9.595	4.00	6.648	-0.210
-	82265058	0.0	999.14	0.503	8	6.648	-6.199
_	82265059	9.0	96.666	9.500	-6.00	6.654	-0.235
-	82265969	0.0	1600.31	0.503	-6.99	6.658	-0.249
_	82265061	0.0	1000.66	0.503	8 9.	6.676	-6.394
—	82265062	.	98.86	0.501	8.80	6.664	-0.406
	82265963	0 .0	999.61	9.500	-10.00	8.678	-0 .528
—	82265964	0 .0	999.38	9.500	-10.00	6.676	-6 .581
	82265965	6 .6	1000.08	9.588	-12.00	6.697	-6.720
— 1	82265966	0 .0	1000.90	6.438	-12.00	6.717	-0.566
	82265967	6 .	1001.48	0.549	9 .00	6.680	-0.241
	82265968	6	1001.37	0.550	0 .00	6.674	-0.246
٦.	82265969	6	999.61	0.552	-2.88	6.652	-0.220
	87765978	.	999.84	9.550	-2.00	6.658	-0.234
	1/00770		40.000	6.55 100	- 	6.046	-6.194 0.04
	82265071	9 6	40.00	9.00	8 8	40.0	907.00
	82265974) e	999.04 67	6.557 5.577	9 9	6. 63 6. 63 63 6. 63 6.	45.55
	82265075	6	1001.37	55.5 155.		889	444
	82265076	9.0	1666.43	55.0	90.8	6.674	9.464
	82265977	0.0	1000.43	0.553	-10.00	6.699	-0.620
	82265978	0.0	1666.78	0.553	-10.00	6.689	-6.620
	83236010	3.0	1000.04	0.642	0.03	6.426	6 .300
	83236011	3.0	999.81	0.042	0.03	6.424	-0 .299
	83229063	a.e	1000.73	0.043	-2.03	6.441	-6.300
	83229064	G.0	1666.39	9.044	-2.03	6.438	-0.305
	83229065	9	999.23	6 .043	4.03	6.424	-0.305
	83229066	B. 1	999.11	0.043	-4.03	6.422	-6.302
	83229067	B. 0	999.34	0.044	-6.06	6.424	-0.306
	83223068	B. 1	000	0.045	90.9-	6.424	-6 .302
	83229069	B 1	1000.39	0.044	-8-63 	6.436	6.303
	832280/8	ю. Э.	1000.85	6.045	- B- 03	•	-6.306
	83228071	B. 1	999.46	6.045	-16.62	6.426	-0.295
	83229072	9. 9.	999.46	0.044	-10.02	6.426	-0.296
	83236012	ю. Ю.	1000.62	0.044	66.6-	6.432	-6.291
	02720013	9 (?)	1666.15	0.042	-16.62	6.426	-6.292 0.292
	6796778	9 (88.88	9.044	-12.64	6.418	-6.292 0.292
٠.	4/0677C0	\$ (1666.58	0.043	-12.66	•	-6.292 0.292
	6786776	9 (20.000	6.643	98.11-	6.4.8	967.9
	2/57///						•

ency, Damping, z 1/sec	700 0	•		420		42.7 42.4 43.4 43.4		-		- 19	+14	+14	+34	428	+12	•	426 -0.297		430 -0.288		_	424 -0.293	426 —0.296		434 -0.297		•		•	426 -0.292		•			9	P '	•	9		9	9	.426 —0.290	•	.436 —0.296	•	9
Shaft Frequency angle, deg Hz	90		10.01	10.01	10.01	18.64		8.79	6/.	66.	-19.99 6.	_		6.06		6.01	-1.98 6.	-1.98	14.04	4.04	-5.97 6.	-5.97 6.		-7.97	-10.04	-10.03 6.	-10.03 6.	-10.03 6.	-11.97 6.	-11.97 6.	-13.99	-13.94	_15.98	15.98	-17.99	-17.98	-19.80 6.	-19.81 6.	-20.00	-20.00 6.	-19.99 6.	-4.02 6.	-4.03	-6.00	-6.00	K. C.
Advance ratio		6.643	749.0	0.040	0.040	6.645	110.0	6.643	6.643	0.043	0.042	0.041	0.003	6.697	0.095	0.094	0.097	9.69.6	6.698	0.097	6.097	0.097	680.0	6.699	6.638	8.696	9.036	6.697	0.097	9.100	6.693	6.697	6.695	89.69	6.697	6.695	6.695	9.096	86.0	6.697	9.096	0.148	0.148	0.145	0.148	177
Rotor speed,		70.888	28.868	999.23	62.888	999.23	5000	1666.15	1888.15	999.57	999.23	999.23	999.81	999.23	998.53	1666.64	999.11	999.81	69.666	1666.39	999.11	999.11	999.34	999.81	1000.04	999.92	1666.27	999.69	999.57	999.46	1666.15	998.88	998.67	999.68	999.23	998.76	1000.15	999.46	999.92	999.69	1000.15	999.57	1666.97	1888.39	0000	
Collective pitch, deg	•	9.0	9 (s :	9.0	B. 6	9.0	6.	d.0	3.0	g.0	3.0	a.e	a.b	a.0	3.0	9,5	9	0	9 60	9	6	9 9	3.0	() () () () () () () () () ()	9.0	9.0	3.0	Ø.6	3.0	0 .0	9.0	3.0	9.E	3.0	9.°C	9 .0	a.6	J. 0	9.0	.0.	9.7) (S)) (S) e) i
Data point number		83229078	83229079	83229686	83229081	83229082	53229683	83229084	83229085	83236014	83236015	83236016	83229086	83229087	83236017	83236018	83229088	83229889	8322990	83229091	83229092	83229093	83229094	83229895	8322988	83229097	83236019	83236020	83229098	83229099	83229100	83229101	83229102	83229103	83229104	83229105	83229106	83229107	83236021	83236022	83236023	83236024	84236925	840460	81216020 R1216027	02520021
Rotor	;	Ξ		II	=======================================	I	I	II	11	11	1 -4	II	II	=	_) p=-	ı	1 -	, p	:=	:=	:=	:=		:=	:=	:=	I	Ξ	11	II	11	11	II	Π	II	II	II	H						→ F	

Domping, 1/sec	-0.293	-6.294	-6.286	-0.284	-9.285	-0.284	-0 .282	-6 .283	-0.271	-6.278	4/7.9	807.0	207.9	787	282	980	- P. 281	-0.274	-0.274	-9.267	-0.261	-0.253	-8 .255	4. 23.8 4. 23.8	25.62	-9.293	-0.287	-0.282	-0.269	-0.269	-6.238 9.238	9.20g	256	-0.222	-0.225	-0.213	-0.225	-0.225	-0.277	-0.271	-9.236	-9.268
Frequency.	6.430	6.436	6.441	6.429	6.422	6.426	6.434	6.432	6.432	6.424	+ C+ . 0	0.420	6.420	6.428	6.414	6.429	6.434	6.438	6.443	6.432	6.428	6.432	6.426	6.424	6.40g	6.436	6.428	6.422	6.424	6.424	6.422	6.424	6.4.30	6.426	6.426	6.432	6.428	6.428	6.420	6.426	6.426	6.420
Shaft angle, deg	-10.00	-10.00	-12.01	-11.97	-14.00	-14.00	-16.04	-16.04	-17.97	-17.97	00.00	/8.8/- Pa a-	9 9	14.67	10.01	12.00	-12.00	-13.93	-13.93	-15.97	-15.97	-17.98	-17.98	# 70 OF	46.81 46.81	46.	-10.01	-10.00	-12.05	-12.04	40.01	14.04	٠ ٦		-15.97	-18.05	-18.05	-18.04	96.6-	96.6-	-12.05	-12.05
Advance ratio	0.147	0.147	0.147	0.148	9.146	9.146	0.149	0.147	9.146	0.147	9 .	96.	40.00	80.0	9 6	200	9.195	98.198	0.199	0.197	0.197	0.198	0.199	401.04	9.193	9.249	0.248	0.248	0.250	0.250	6.256	9.236 9.248	9.246	0.247	0.248	0.248	0.249	0.249	0.301	0.301	0.296	0.297
Rotor speed, rpm	1666.64	1000.50	1001.32	999.34	69.666	1000.04	1000.85	1000.62	1666.73	1666.64	1001	77.000	000	76.666	10. WG	FC 066	1666.39	1000.85	1001.32	1000.50	1000.27	1999.62	999.92	80.88	000 000 000 000 000 000 000 000 000 00	1000.04	69.666	999.23	999.57	999.57	94.500	45.000	1000	999.46	989.46	18.666	999.57	999.81	998.88	999.57	999.46	999.46
Collective pitch, deg	3.0	3.0	0.0 0.0	6. 6.	g.8	o. 1	6. 6.	ю. 6	9.0	ა . გ. დ	9.6	9 6) M	9 6	9 6	6	3.0	3.0	3.0	3.0	a. 0	6.0 6.0	ю. В е	5 G	D 60	9 9	a.6	3.0	G.0	9. n	9 e	9 G	9 6	9	9.0	3.0	a.0	3.0	G.0	ю. 0.	9.°	0.0 0.0
Data point number	83236030	83236031	83236032	83236033	83236034	83236035	83235836	83236037	63236636	82222828	84246841	83236043			83236046	83236047	83236048	83236049	83236050	83236051	83236052	83235853	83235854	81216855	83236057	83236058	83236059	83236060	83236061	2000220	81236863	83236865	83236066	83236067	83236068	83236069	83236070	83236071	83236074	83236075	83236076	83236077
Rotor	II	= :	Ξ:	:	⊒;	=:	7:		7 1	11	: -	:=				II	II	II	II	I	Ι:	:		7.1	::	II	II	II	I:		; <u>.</u>		II	II	11	II	II	I	Ι:	Ξ:	:	7:

Hz 1/sec
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tor Data point Collective Rotor speed, Advance sted number pitch, deg rpm ratio at a statement step number pitch, deg rpm ratio at a statement step number pitch, deg rpm ratio at a statement step number pitch, deg rpm ratio at a statement step number pitch, deg rpm ratio at a statement step number pitch, deg rpm ratio at a statement step number pitch, deg rpm ratio at a statement step number pitch, deg rpm ratio at a statement step number pitch number pitch, deg rpm ratio at a statement step number pitch number p				TABLE 9	TABLE 9.—CONCLUDED			
6.0 999.46 6.0 999.57 6.0 999.57 6.0 999.57 6.0 1000.043 6.0 1000.044 6.0 997 1000.15 6.0 1000.15 6.0 999 11 0 0998 6.0 999.11 6.0 999.11 6.0 999.11 6.0 999.11 6.0 999.11 6.0 999.11 6.0 999.11 6.0 999.11 6.0 999.11 6.0 999.11 6.0 999.11 6.0 999.11 6.0 998.11 6.0 999.11 6.0 999.11 6.0 999.11 6.0 999.11 6.0 999.11	- 8	Data point number	Collective pitch, deg	Rotor speed,	Advance ratio	Shaft angle, deg	Frequency, Hz	Damping, 1/sec
6.0 999.57 6.0 999.34 6.0 1000.04 6.0 1000.04 6.0 1000.04 6.0 1000.15 6.0 1000.15 6.0 1000.15 6.0 1000.15 6.0 148 6.0 1000.50 6.149		83242046	ø.	999.46	0.047	-19.93	6.432	-0.592
6.0 1999.34 0.042 6.0 1000.04 0.097 6.0 1000.04 0.097 6.0 1000.15 0.097 6.0 1000.15 0.098 6.0 1000.15 0.098 6.0 1000.15 0.098 6.0 1000.04 0.098 6.0 1000.04 0.148 6.0 1000.50 0.149		83242047	6.0	999.57	0.043	-19.93	6.438	-6.578
6.0 1000.04 0.097 6.0 1000.15 0.097 6.0 1000.15 0.097 6.0 1000.15 0.098 6.0 999.11 0.098 6.0 999.92 0.098 6.0 1000.04 0.098 6.0 1000.05 0.098 6.0 1000.50 0.148		83242048	6.0	999.34	0.042	-19.93	6.430	-9.566
6.0 1000.15 0.097 6.0 1000.15 0.097 6.0 1000.15 0.098 6.0 999.11 0.098 6.0 999.31 0.098 6.0 1000.85 0.148 6.0 1000.50 0.148		83242049	6.0	1000.04	6.097	-15.98	6.441	-0.561
6.0 1000.04 0.096 6.0 1000.15 0.097 6.0 1000.15 0.098 6.0 939.11 0.098 6.0 939.81 0.098 6.0 1000.85 0.098 6.0 1000.85 0.148 6.0 1000.50 0.148		83242050	6.0	1000.15	6.097	-15.98	6.443	-0.550
6.0 1000.15 0.097 6.0 1000.15 0.098 6.0 999.11 0.098 6.0 999.11 0.098 6.0 1000.85 0.098 6.0 1000.04 0.148 6.0 1000.50 0.149		83242051	6.9	1000.04	960.0	-18.02	6.440	-6.548
6.0 1000.15 0.098 6.0 999.11 0.098 6.0 999.81 0.098 6.0 1000.85 0.098 6.0 1000.04 0.148 6.0 1000.50 0.147		83242052	6.0	1000.15	6.697	-18.02	6.441	-0.552
6.0 999.11 0.098 6.0 999.81 0.096 6.0 1000.85 0.098 6.0 1000.04 0.148 6.0 1000.50 0.147 6.0 1000.50 0.147		83242053	6.0	1000.15	86.0	-19.97	6.443	-0.547
6.0 999.81 0.096 6.0 1000.85 0.098 6.0 1000.04 0.148 6.0 1000.27 0.147 6.0 1000.50 0.149		83242054	6.0	999.11	0.038	-19.96	6.430	-0.577
6.0 1000.92 0.098 6.0 1000.85 0.148 6.0 1000.27 0.148 6.0 1000.50 0.147 6.0 1000.50 0.149		83242055	6.0	999.81	969.0	-19.97	6.438	-0.555
6.0 1000.85 0.148 6.0 1000.04 0.148 6.0 1000.27 0.147 6.0 1000.50 0.149		83242056	8.0	999.92	860.0	-19.97	6.441	-9.566
6.0 1000.04 0.148 6.0 1000.27 0.147 6.0 1000.50 0.149		83242057	6.0	1000.85	0.148	-18.00	6.451	-6.573
6.0 1000.27 0.147 6.0 1000.50 0.149 8.0 0.08 6.1		83242058	6.0	1000.04	9.148	-18.00	6.440	-0.543
6.0 1600.50 0.149 6.0 008.51 0.140		83242059	6.0	1000.27	0.147	-17.99	6.447	-0.558
K 0 000 KT 0 140		83242060	6.6	1000.50	0.149	-19.95	6.440	-0.558
841.0 CC.088		83242061	6.9	998.53	0.149	-19.98	6.418	-0.569

TABLE 10. -- REGRESSING LEAD-LAG MODE DATA IN FORWARD FLIGHT, CONFIGURATION WITH STRUCTURAL FLAP-LAG COUPLING, 750 RPM

Damping. 1/sec	-6.150	-6.150	-0.147	-6.145	4 . •	-0.145	‡ •	-0.142	-6 .139	-6.138	-0.137	-9.1 38	-6 .138			a 136	-0.140	19.141	-0.148	9.148	148	-6.1 63	-0 .162	-6. 173	-6.170	6.152	9.138	-a.153	4.138	-6.152	9 ;	9	77	141	14.14	Τ.	. 138	-0.149	-0.146	-0.172	-0.166	-0 .169	-0.176	-6.171	-0 .190	
Frequency, Hz	3,431	3.442	3.454	3.429	3.427	3.434	J. 444	3.440	3.440	3.448	3.434	3.436	J. 444	3.442	3.438	3.452	3,458	3,448	3.461	3.442	3.450	3.456	3,452	3.450	3.450	3.425	5.427	3.434	404.0 404.4	3.425	0.400	5.4.5 4.50	A 441	3.431	3.429	3.436	3.440	3.432	3.436	3.446	3.446	3.440	3.434	3.434	3.446	
Shaft angle, deg	29.67	-6.67	-1.99	-1.99	-4.02	4.02	-6.03	-6.03	-B.63	6.03	-10.07	-10.07	-12.04	'n	N.	-12.05	-14.04	-14.04	w.	-15.96	-15.96	-18.02	-18.02	-19.64	-19.64	8 .	50.0	90.0	9 . 9 . 9 .	9 6 9 6	9 0.7-	20.7-	16	6.6	-6.02	-7.93	-7.92	-10.00	-10.00	-12.01	-12.01	-12.01	-12.00	-12.00	-14.00	
Advance	898	0.093	0.693	6.693	0.003	6.693	0.082	0.082	0.093	6.693	0.093	960.0	6.095	6.097	9.098	989.9	960.0	6.698	60.00	6.698	9.696	869.	0.095	960.0	9 .034	0.140	9.158	0.150	9.120	9.138	9	0 - 0	. e	0.149	9.149	0.149	9,146	6.149	0.150	0.149	0.146	0.148	0.150	9.150	0.150	
Rotor speed, rpm	749.54	750.46	751.39	749.42	749.19	749.88	750.70	750,35	750.46	750.93	749.88	750.12	750.70	750.58	750.35	751.39	751.74	750.93	751.97	750.46	751.04	751.39	750.93	750,81	750.81	748.96	749.19	750.00	750.00	750.00	750.12	740.42	740 54	749.65	749.54	750.12	750.35	749.65	750.00	750.46	750.46	750.12	750.00	750.00	750.00	
Collective pitch, deg	6	9	0.0	6.6	0.0	0 .0	0 .0	6 .6	0 .0	6 .0	6 .6	o. o	.	.	ø.	•	•.6	0.0	.	9.0	6.6	.	9 .0	9 .	9 .	6 .	0 .0	0 .0	9 . 9	6 . 6	9 (P . 6	9.0	9.6	9 6	9	9	0.0	9	9.6	9	9	9	9	0.0	
Data point number	810000E	83222049	83222050	83222051	83222052	83222053	83222054	83222055	83222056	83222057	83222058	83222059	83222060	83222061	83222062	83222063	83222064	83222065	83222066	83222067	83222968	83222069	83222070	83222071	83222072	83222073	83222074	83223002	83223003	83223004	852226/5	83222876	077770	83222070	83222080	83222081	83222082	83222083	83222084	83222085	83222086	83222087	83223005	83223006	83223007	
Rotor	E	:=	:=	II	Ξ	II	11	11	11	11	11	II	II	II	II	Ξ	11	II	11	II	11	II	11	II	=======================================	II		II	I	I	:	- :	F	- h-	-	:=	: =	II	<u> </u>		-	: -		:=	H	

Domping. 1/sec	-6.184	491.0	-6.201	-0.196	-0.198	-0.195	-0.202	-0.198	-0.198	-0 .159	-0 .160	-6.148	6.154	-9·148	4.14	-0.149	9.140	-0 .160	-0 .164	-0.182	6 .191	-9.188	-0.193	-0.198	-0 .192	-0.189	-0.201	-0.205	-0.201	-0.204	-9.159	-0.160	-6 .155	-6 .161	-0.151	-9 .151	9.161	-0.159	-9 .181	-0.169	-0.184	-6.179	-6.196	-0.184	196	-6.198
Frequency, Hz	3.448	3.448	3.435	3.431	3.436	3.440	3.450	3.432	3.432	3.438	3.438	3.432	3.434	3.440	3.440	3.444	3.433	3.431	3.436	3.442	3.438	3.438	3.442	3.431	3.452	3.413	3.440	3.444	3.448	3.450	3.417	3.452	3.440	3.436	3.427	3.427	3.423	3.419	3.419	3.436	3.423	3.454	3.454	3.454	3.448	3.460
Shaft angle, deg	-14.00	-14.00	-16.00	-16.00	-16.00	-18.00	-18.00	-20.00	-20.00	99.00	9.00	-2.00	-2.00	14 .00	8.7	98.99	-6.80	8.80	8.90	-16.00	-10.00	-10.00	-12.00	-12.00	-14.00	-14.00	-16.00	-16.00	-18.00	-18.00	99.0	19.01	-2.04	-2.04	-3.99	-3.99	-6.03	-6.03	-8.07	-8.07	-8.07	-8.03	-10.03	-10.03	-10.03	
Advance rat io	0.150	6.150	0.150	9.159	0.150	0.150	0.150	0.150	0.150	0.200	0.200	9.200	0.200	0.200	0.200	0.200	0.200	0.200	9.200	6.200	0.200	0.200	9.200	0.200	0.200	9.200	0.200	0.200	0.200	0.200	0.249	0.248	0.245	0.248	0.248	0.250	0.251	0.250	0.251	0.250	0.253	0.250	0.251	0.251	9.251	0.249
Rotor speed,	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	748.61	751.16	750.46	750.12	749.07	749.30	748.84	748.38	748.38	749.54	748.61	750.93	751.28	750.93	750.81	751.28
Collective pitch, deg	9.	0.0	0 .0	0.0	0 .0	0.0	0.0	0.0	ø. ø	0 .0	0.0	0 .0	0 .0	0 .0	0.0	0.0	0.0	9 .9	0.0	0.0	9.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	9.9	0 .0	0.0	0.0	9.0	0.0	0.0	0.0	0.0	9.0	0.0	0.0			8) 0
Data point number	83223008	83223009	83223011	83223012	83223013	83223014	83223015	83223016	83223017	83223018	83223019	83223020	83223021	83223022	83223023	83223024	83223025	83223026	83223027	83223028	83223029	83223030	83223031	83223032	83223033	83223034	83223035	83223036	83223037	83223038	83223041	83223042	83223043	83223044	83223045	83223046	83223047	83223048	83223049	83223050	83223051	83223052	83223053	83223054	83223055	83223056
Rotor	II	II	H	II:	-	:	I			I	II	—	II	II	II	II	I	II	11	11	II	Ξ	Ξ	I	I	II	II	.	II	II	II	II	II	I	II	II	II	11	II	I	II	:	II	II	II	

	Domping. 1/sec	9		176	-0.167				-0.156	٠.	-8.158	٠.	٠.	Ξ,	٦,	12.9	49.164	- Pa - 169	49. P	2 - S	9 - 6	9.5	-6.187	-6.187	-0.193	-0.165	-0.173	9 6	85. 1. 85.	-0.154	-0.152	-6.173	9 - 9	9/ 9	25.00	193	-0.166	-6.170	161	-6 .161	-0.149	-0 .162	-6.151	-d. 155
	Frequency, Hz	1 454	452 452	3 442	3.438	3.427	3.427	3.436	3.411	3.438	3.440	N. ++	3.449	3.419	5.438	3.452	3.438	3.454	****	3.427	5.440 4.25	3.42	3.452	3.432	3.442	3.44	3.446	5.442	3.438	3.438	3.442	3.434	3.4.5	0 · + · ·	4.34 A.34	¥ 4 4 4	3.442	3.442	3.440	3.444	3.446	3.425	3.450	3.452
,	Shaft angle, deg	90 11	76.41-	-14 97	-14.04	6.62	6.91	90.0	-2.02	-2.02	-2.02	-2.02	-3.99	8. †	4.62	7.62	Θ . φ	86.69 66.69	56. 17.		50°./-	88. /-	-16.63	-10.03	-10.03	9.02	9 .95	<u>.</u>	1 1	96.4	-3.99	-6.03	9. 9 2. 6	6.00	9 6	20.0	9 9	6	-2.02	-2.02	-3.96	-3.99	66.5-	-3.99
TABLE 10.—CONTINUED	Advance	25.0	9.222	97.6	0.247		6.295	0.296	0.300		0.296	0.296	9.300	0.297	6.302	0.298	6.299	6.297	6.295	0.299	202	867.0 600 6	6.302	0.303	0.298	0.347	0.346	9.540	9.040	9.351	9.347	0.348	9.348	9.22.0	0.554 454	27. e	26.397	395	0.400	9.401	9.400	0.402	0.399	0.399
TABLE 10.	Rotor speed, rpm	751 16	75.0	749 88	749.30	748.96	749.19	749.77	747.68	750.00	750.00	750.46	750.00	748.38	750.81	750.93	749.65	751.04	750.23	748.49	40.04	740.88	759.35	749.19	749.77	750.23	750.46	750.58	71.0C/	749.77	750.12	749.42	749.65	758.23	749.88	740 10	750.00	750.00	750.00	750.23	750.23	748.61	750.81	
	Collective pitch, deg	6	9 6) s			9 6	9.9	0.0	0.0	9.0	9 .	6 .6	9 .	9.	9 .	9 .	6 .6	6 . 6	9 . (9 .6	P 6	9 6	9 6	0.0	0 .0	9 .9	9 . 6	9 G	9 6	0.0	6 .	9 .0	9 (e	s e	9.0	9 6	9 6		9.9	9.	0.0	9 .0	0 .
	Data point number	100000	02223007	0.00.77.00	81221858	83223063	83223864	83223066	83223067	83223068	83223069	83223086	83223070	83223073	83223074	83223075	83223076	83223077	83223078	83223079	83223080	63223061	81221881	83223884	83223085	83223087	83223088	83223089	83223090	83223892	83223093	83223094	83223095	83223096	83223097	0207770	81221100	8422400	83223102	83223103	83223104	83223105	83223106	83223107
	Rotor	;	 		<u> </u>	: -	: =	:=	: II	Ξ	11	11	11	11	11	11	11	II		I	Ι:] <u> </u>	-	=	11	II	II	Ξ:	; <u>-</u>	H	11	= :	=:	F	7.	71	4 F-	-		II	11	II	11

Damping, 1/sec	•		7 6	2/1	9	9 4		4	-0.250	-6.252	-0.253	-0.262	-0.254	-0.245	-0.257	-0.261	-0.263	-0.253	-0.252	-0.255	-0.257	-0.256	-0.254	-0.255	-0.256	-0 .251	-0.249	-0.249	-0.248	-0.244	-0.249	-0.243	-9.245	-0.241	-0.243	-0.245	-0.257	-9.258	-0.257	-0.256	-0.254	-0.258	-0 .252	-0.251	-0.245	-0.249	
Frequency, Hz	•	3.456	0.400			7 7 7	3 434	3 442	3.440	3.444	3.444	3.436	3.450	3.436	3.458	3.450	3.436	3.444	3.434	3.440	3.431	3.431	3.440	3.434	3.434	3.440	3.442	3.448	3.438	3.438	3.446	3.442	3.423	3.429	3.444	3.434	3.454	3.454	3.446	3.444	3.448	3.438	3.448	3.452	3.450	3.444	
Shaft angle, deg	•	9.6	6.6	70.0	9-1-1		00.	000	6 e	10.01	-2.03	-2.02	-2.02	-3.99	-3.98	-3.98	-3.98	-6.06	90.9-	-7.99	-7.99	-10.00	-10.00	-11.96	-11.96	-13.99	•	-15.93	-15.93	-18.04	-18.04	-18.04	-18.04	-19.96	-19.96	-19.96	-3.96	-3.96	-6.04	-6.04	-8.07	-8.07	-10.04	-10.07	-12.02	-12.01	
Advance ratio		2007 2007	9.400	0.44/	0.44/ 454	6.45 451	6.456	0 440	260.0	0.093	0.095	0.095	9.034	6.634	0.005	969.0	0.095	0.005	0.095	0.005	0.095	960.0	6.697	9.002	6.094	0.034	6.034	6.095	6.095	0.005	0.005	0.095	0.095	0.095	0.005	6.694	0.149	9.151	0.150	0.150	0.150	0.150	0.150	0.149	6.149	0.152	
Rotor speed, rpm	,	10.107	10.107	759.34	749.19	740 19	749.19	750 12	749.77	750.12	750.23	749.65	750.58	749.54	751.16	750.58	749.54	750.12	749.42	750.00	749.19	749.19	750.00	749.42	749.42	750.00	750.12	750.58	749.77	749.88	750.46	750.12	748.72	749.19	750.35	749.65	750.35	750.35	749.88	749.65	750.12	749.30	750.12	750.35	750.46	749.88	
Collective pitch, deg	•	P 6	9 6	9 6	9 6	• •	9 6	9	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	J.0	J. 0	3.0	۵. ف	3.0	3.0	3.0	G. 0	6. 6.	9 .0	0.0 0.0	9.0	3.0	0.0	0.N	3.0	3.0	3.0	3.0	G.0	3.0	3.0	3.0	
Data point number	80110018	83223186	8422414	83223111	83223112	83223113	83223114	83223115	83255005	83255006	83255007	83255008	83255009	83255010	83255011	83255012	83255013	83255014	83255015	83255016	83255017	83255018	83255019	83255020	83255021	83255022	83255023	83255024	83255025	83255026	83255027	83255028	83255829	83255030	83255031	83255032	83255035	83255036	83255037	83255038	83255039	83255040	83255041	83255042	83255043	83255044	
Rotor	:	: -	: =	:=	I	I	II	II	11	II	II	11	II	I	, II	II	II	11	II	II	II	11	I	= :	II	Ξ:	⊒ :	I	-	=:	⊒:	⊒:	7 ;	-	-			II	I	II	11	II	II	11	II	II	

Domping. 1/sec	244	244	-0.241	-0.242	-6.240	-0.241	-0 .239	-0 .232	-0 .239	-6.233	-0.264	-8 .256	-9 .256	- 9 .256	29.762	- 6 .233	6.249	9.247	-6.248	6.244	44.4	9.5	-0.240	-6.235	-6.237	-0.239	-0 .250	-6.238	977.0	6.236	22.9			-0 .221	-0.223	•		٠	٠	•	-0.249	6.233	٠	-0.242
Frequency, Hz	3 420	3.442	3.431	3.429	3.438	3.450	3.444	3.431	404.6	3.440	3.438	3.432	3.440	5.427	5.425	5.42/	5.440	3.446	5.4.6 5.4.6	5.444 4.40	20.5	3.434	3,434	3.434	3.427	3.436	3.434	3.442	0.446	404.0	3.425	3.421	3.429	3.423	3.442	3.436	3.438	3.432	3.446	3.434	3.429	0.444	5.432	A 425
Shaft angle, deg	-14.04		-16.68	-16.08	-18.05	-18.05	-19.97	-19.97	-19.98	-19.98	-6.02	-6.62	-6.62	29.62	-6.62	7 6 9 6 9 7	99.91-	-10.06	99.99	-11.93		- 4	-14.06	-14.06	-14.06	-15.93	-15.93	-15.93	10.61 10.61	17.9/	• [-17.97	-19.99	-19.98	-20.00	-20.00	-6.02	-6.03	-6.03	-6.03	-7.99	-7.99	-7.99	20 CT
Advance	6, 152	0.151	0.150	6.151	6.151	9.156	0.151	6.151	0.152	6.150	6.197	8.198	9.786	e.261	907.9			781.0	9.1.0		• • • • • • • • • • • • • • • • • • •	9.1.90	6.198	9.196	6.198	6.198	0.197	6 .198	/6. · 6	6.193	. e	6.198	0.201	0.202	0.201	0.200	0.249	0.248	0.249	0.253	0.243	6.248	0.248	۵ ۲۲۷
Rotor speed,	748.72	749.77	749.07	748.96	749.88	756.93	750.58	749.42	749.65	750.23	749.77	0. 04 / n	749.88	746.80	740.72	740.90	736.30	750.58	750.36	758.40	748 84	750.00	750.00	750.00	749.30	750.35	750.23	750.81	750.10	21.00/	74.9.70	749.07	•	748.84	750.23	749.88	749.54	749.07	750.12	749.30	748.72	750.68	749.19	77.8 77
Collective pitch, deg	6	(S)	0.D	a.0	3.0	3.0	3.0	3.0	3.0	ю. •	B. 1	D. 7	9 G	9 G	D 6	D 6	9.0	D (D (D 6) K) e	6.6	9.6	3.0	3.0	3.0	9.0	9. c	٠ ه و) M	9.0	3.0	3.0	3.0	J. 0	3.0	J. 0	0.0 0.	o.0	6 .0	8. e	B.:	5
Data point number	83255045	83255046	83255047	83255048	83255049	83255850	83255051	83255052	83255053	83255054	83256004	83256005	8323686	/999CZCR	8223088	62220668	83236818	83236811	21000200	85256013	81256814	83256016	83256017	83256018	83256019	83256020	83256021	83256022	6200020	83236824	83256025	83256027	83256028	83256029	83256030	83256031	83256034	83256035	83256036	83256037	83256038	83256839	83256040	81256041
Rotor	=	=	П	Π	11	II	11	II	II	-	11	Ξ:	- :	-	-	- :		1;	7;	 		4	I		II	II	II	Π:] :	11	:=	H	II		11	11	II				II	- :];	_

Damping, 1/sec	-0.243	-0.245	-0.234	-0.226	-6.240	9.240	-6 .231	-0 .223	-0.236	-0.224	6 .213	-0.213	-0.220	-0 .206	-6 .211	-0 .192	-0.202	-0.206	-0.204	-9 .216	-6 .268	-0.245	-0 .251	-0 .251	-0.245	-0.247	9.248	-0.250	-0.233	-0.236	-6 .239	-6 .239	9.246	6.232	247.0	9.730	9.7.9	077.9	757.	9.779	-6.198	-6.204	-0.203	-9.207	-6.204	-0.210
Frequency, Hz	3.427	3.432	3.421	3.421	3.450	3.438	3.446	3.438	3.434	3.421	3.436	3.436	3.438	3.442	3.450	3.434	3.44	3.438	3.446	3.442	3.442	3.434	3.436	3. 1 ‡	3.429	3.432	3.436	3.452	3.438	3.432	3.438	3.442	5.428	5.4.5	\$ 05.00 \$ 00.00	404.0 44.4	- C+	3.432	0.446	5.432	404.5	3.454	3.444	3.446	3.434	3.458
Shaft angle, deg	-10.03	-10.03	-12.04	-12.04	-12.04	-12.04	-14.04	-14.04	-14.04	-14.04	-16.94	-16.04	-16.04	-17.98	-17.98	-17.98	-17.98	-19.97	-19.98	-19.98	-19.98	-8.02	-8.9 4	-8.03	-7.99	8 9.	-7.99	-7.99	-10.01	-10.01	-16.01	-16.01	-10.65 -	-16.65	-16.60			-12.00	30 I-		-13.96	-13.96	-13.96	-13.96	-16.11	-16.11
Advance ratio	0.245	0.247	9.244	0.250	0.251	0.251	0.249	0.243	0.242	0.248	0.248	0.259	0.253	0.252	0.250	0.252	0.246	0.250	0.248	0.248	0.249	0.296	0.298	9.300	0.299	0.297	0.300	6.300	0.302	6.301 -	0.300	0.299	6.298	6.298	0.230	9.738	9.300	9.381 9.381	667.0	9.300	0.298	٠	0.299	0.295	0.300	0.299
Rotor speed, rpm	748.96	749.30	748.72	748.72	750.93	750.12	750.70	750.23	749.77	748.72	749.65	749.42	749.77	749.65	750.35	749.07	749.88	749.42	750.12	749.77	749.77	749.30	749.54	750.23	748.96	749.19	749.88	751.16	749.88	749.65	750.00	750.12	749.42	758.35	/26.66	10.107	749.00	750.00	/56.55	750.12	751.16	751.16	750.23	750.35	749.42	751.16
Collective pitch, deg	6	9.B	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	a.6	a.0	3.0	3.0	0.0 0.0	3.0	G.0	J.0	3.0	3.0	3.0	3.0	a.e	a.6	3.0	3.0	3.0	a.6	3.0	9. 9.	6 .0	9. 9.	o.,	٠ د د	9.0	9 (9.°	٠ ٠	9.0	ы. Ө.	a.0	9.B	J.0	G.6	G. 0
Data point number	83256042	83256043	83256044	83256045	83256046	83256047	83256048	83256049	83256050	83256051	83256052	83256053	83256054		83256056	83256057	83256058	83256059	83256060	83256061	83256062	83256063	83256064	83256065	83256073	83256074	83258004	83258005	83256066	83256067	83256068	83256069	83258006	83258007	6323666	82228689	03230010	83238011	83238012	83258013	83258014	83258015	83258016	83258017	83258018	83258019
Rotor	II	11	II	II	11	II	11	II	II	II	II	II	!	II	II	=	II	II	II	II	II	11	11	II	II	II	11	11	II	11	II	I	:		⊒:	7 1		-	- ;	≓ :	1:	I	II	II	II	I

Damping, 1/sec	-0.187	-0.205	-6 .198	-0.207	-0.191	-6 -188	-0.189	-0.191	-6.189	6 .171	-0.240	-9 .256	-0 .252	9.540	-0 .221	-0 .228	-0.234	-0.212	-0 .22 0	-0.207	-0.233	-0 .182	-0 .196	-0.194	-0.203	- 6 .186	-a. 165	-0.176	-0.187	-6.176	-9.181	-6.177	45.	‡ ! • •	9	2	4.1/4	- 588 - 588 - 588	-6.578	-0 .572	-6.581	-6.577	-6 .581	6 .581	-0.564	-0.574
Frequency, Hz	3.442	3.446	3.444	3.434	3.444	7. T	3.450	3.454	3.446	3.450	3.440	3.444	3.442	3.434	3.436	3.432	3.427	3.438	3.450	3.423	3.429	3.440	3.434	3.427	3.440	3.425	3.427	3.442	3.444	3.467	3.458	3.440	3.440	3.436	2.401	0.440	5.456	3.456	3.448	3.454	3.460	3.456	3.448	3.444	3.446	3.450
Shaft angle, deg	-16.11	-16.11	-17.98	-17.97	-17.98	-17.97	-20.00	-20.00	-20.00	-20.00	98. 89.	8.00	8 8.89	98.89 P	8 9. 8 9	8 .89	88. 89.	-10.00	-10.03	-10.02	-10.03	-12.04	-12.04	-12.04	-12.04	-14.01	-14.00	-14.00	-14.00	-16.01	-16.01	-16.01	16.61	18.66	20. /r-	88.71-	-17.99	-12.06	-12.07	-12.07	-14.00	-14.00	-16.04	-16.04	-17.97	-17.97
Advance ratio	9.300	0.303	0.295	0.298	0.296	6 .298	6.299	0.300	6.301	6.301	0.348	6.351	0.348	0.347	0.351	9.351	9.348	9.349	0.353	6.352	0.353	6.349	0.348	0.351	0.348	0.352	9.348	6.351	0.352	0.349	0.350	0.349	6.356	6.348	9.54/	6.548	6.345	9.634	0.093	0.091	0.093	6.091	0.093	0.093	960.0	6.694
Rotor speed, rpm	750.12	750.35	750.23	749.19	750.00	750.00	750.12	750.35	749.54	749.77	749.88	749.88	750.00	749.54	749.77	749.30	748.84	750.00	750.81	748.72	749.30	749.77	749.65	748.72	750.00	748.49	748.49	749.65	759.66	751.39	750.46	749.65	749.30	750.12	750.45	749.50	750.12	749.77	749.54	749.77	750.23	750.12	749.19	749.07	749.19	749.54
Collective pitch, deg	G. 6	3.0	3.0	3.0	o.0	a. 0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	0.0 0.0	3.0	a.6	9.0	a.6	3.0	3,0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	9. 9.	B. 0	8 .0	g.9	9 .9	9 .9	9 .9	6.6	6.0	6.0	9.9	6.0	9.
Data point number	83258020	83258021	83258022	83258023	83258024	83258025	83258026	83258027	83258028	83258029	83258034	83258035	83258036	83258041	83258042	83258043	83258044	83258045	83258046	83258047	83258048	83258049	83258050	83258051	83258052	83258053	83258054	83258055	83258056	83258057	83258058	83258059	83258060	83258061	83258062	83258063	83258064	83259028	83259029	83259030	83259031	83259032	83259033	83259034	83259035	83259036
Rotor	11	H	II	II	II	11	11	11	H	II	II	11	11	Π	Ξ	11	Π		=======================================	: =	: =	I	II	II	II	11	- 11	Н	11	==	11	11	11	I	II	!!	11	II	11	11	11	=	II	II	Π	II

		-0.578													
	Frequency	3.465	3.456	3.454	3.460	3.460	3.442	3.446	3.429	3.461	3.450	3.438	3.440	3.450	3.438
	Shaft angle, deg	-19.98	-19.98	-16.05	-16.05	-18.01	-18.01	-20.00	-20.00	-15.97	-15.97	-18.01	-18.01	-20.00	-20.00
TABLE 10.—CONCLUDED	Advance	6.693	0.094	0.148	9.148	6.148	0.149	9.144	0.143	0.195	9.196	0.197	9.196	0.195	0.196
TABLE 10.	Rotor speed, rpm	756.70	750.23	749.77	750.23	750.35	749.19	749.30	748.26	750.58	749.65	748.96	749.19	750.23	749.19
	Collective pitch, deg	6.9	0.0	6.6	6.9	6.9	6.6	6.9	6.9	6.9	6.6	9.9	6.9	9.9	6.9
	Data point number	83259037	83259038	83259039	83259040	83259041	83259042	83259043	83259044	83259045	83259046	83259047	83259048	83259049	83259050
	tor	II													

TABLE 11. - REGRESSING LEAD-LAG MODE DATA IN FORWARD FLIGHT, CONFIGURATION WITH STRUCTURAL FLAP-LAG COUPLING, 1800 RPM

Frequency, Damping, Hz 1/sec	6.428 -0.164	7	7	6.422 6.489	7	99	9	6.432 — 6.162	9	t32 —0.1	- .	₹,	F. 9	- •	- • •	6.434	9	- -	-	_	6	9	77	- -	412	9	. e	•	-	- 1	- -		Ģ	i e	ę ٻ	.447	ဝှ ်	φ, φ	0	•
Shaft angle, deg	6.62	-1 07	(6:1-)) - 	70.1	10. 9	4	, e	. 8. 59.			<u>.</u>	-11.97	•		10.01	17:04	• 1	-19.64	-19.64	9.00	00.00	9.0	- F	12.6	86	-3.98	-5.98	-5.96	1.98	86. /- 86. /-	-10.00	-10.00	-12.04	•	-12.02	<u>.</u>	2;	٠	60 07
Advance ratio	9.944 943	0.042 7.040	9.6	9 945	446	944	9.64	0.045	9.044	9.944	9.044	9.044	9.843	6.640 5.40	•	0.04 0.45 0.45	•			0.043	•	•						6.697	0.097		700 G	689.0	0.097	6.097	0.097	6.097	0.097	0.097	/60.0	100
Rotor speed, rpm	999.69	20.000	+0.000 +c.000	C7. E86	00.700	1000.39	1000.62	999.92	1000.15	1000.15	999.81	999.34	40.000	1000.04	20.000	999.92 000 AA	998.43	999.81	1000.85	1000.15	1000.04	999.11	70.888	40.000	20. 800 65. 855	88.866	999.23	1001.32	1999.27	86.86	4F. 000	1000.85	1000.27		•	1001.55	999.46	999.68	880.00	F-1 000
Collective pitch, deg	6	9	9	9 6	9	9 6		9 9	9.0	0 .0	0 .0	.	9 (9.0	D 6	9 6	9 9	0.0	0 .0	9 .0		9.0			9	9.0	0.0	0 .0	9 6		9	9.9	0.0	9.9	0.0	9 .0	ø. 6	9.	
Data point number	83223120	8107719	1017078	81027123	8107108	83223126	83223127	83223128	83223129	83223130	83223131	83223132	83223133	83223134	62223133	62223136 847774477	81221138	83223139	83223140	83223141	83224004	83224005	83224006	62244029	83224007 83224008	83224009	83224010	83224011	83224012	83224013	83224014 83224015	83224016	83224017	83224018	83224019	83224020	83224021	83224022	63224623	10010010
Rotor		- F	- F		::	; <u>.</u>	: <u>-</u>	:::	11	II	II	I.	Ξ:	=:	:	11			II	11	II	Ξ:		::		11	II	II	H	11		I	I	II	II	II	I:	Ξ:	77	

Rotor	Data point number	Collective pitch, deg	Rotor speed, rpm	Advance	Shaft angle, deg	Frequency, Hz	Domping, 1/sec
	83224027	6	000 57	900	10 64	A 426	400 0
	83224028	9 6	11.666	0.00	19.65	•	186.6
	82263003	9	1000	0.149	9	6.639	461
-	82263005	0.0	1001.13	0.142	90.0	6.639	-6.179
-	82263017	0.0	999.38	6.149	99.9	6.639	-6.175
II	83224032	0.0	998.30	9.148	00.00	6.412	-6.170
11	83224033	0.0	1000.04	0.148	99.0	6.434	-0.174
I	83224058	0 .0	1000.15	9.146	0.02	6.434	-0.163
Ξ'	83224059	0.0	999.57	0.152	0.01	6.428	-6.170
— ,	82263004	0 .0	1666.31	0.149	-2.00	6.652	-0. 180
⊶•	82263006	0 .0	1000.08	9.146	-2.60	6.652	-0.176
→ ;	82263018	9 .0	1000.08	0.148	-2.00	6.639	6.174
⊒:	83224034	0 .0	1000.27	0.146	-2.02	6.436	-0 .169
Ξ'	83224035	6 .6	1000.39	0.150	-2.02	6.438	9.169
.	82263007	0 .0	1000.08	9.148	8 . †	6.639	-0.176
- - ,	82263008	0 .0	96.666	9.148	8. †	6.639	-0.172
		0 .0	1000.08	0.149	8:	6.639	-0.173
-		9 .0	999.34	0.150	4.02	6.424	-0.165
Ι.	83224037	0 .0	999.57	9.147	-4.02	6.428	-0.166
-	82263009	0 .0	96.666	0.148	90 .9	6.639	-0.176
	82263020	0.0	999.61	0.148	90.9	6.639	-0.168
⊶ ;	82263021	0 .0	1666.31	0.148	-6.90 	6.639	6.172
: :	83224038	9 .0	1000.97	0.150		6.443	-0.162
:	85224039	9 .0	1666.39	6.148	9.00 0.00	6.438	-9.176
-	85224646	9 .0	998.41	9.148	-5.99	6.414	9.169
-	83224041	9 .0	999.92	9.148	90.99	6.432	-0.162
→ ►	82263616	9 .0	1666.43	0.149	98. 190.	6.639	-6.177
-	62265822	9.0	989.84	9.147	8 8 8 8	6.639	6.175
::	03224042	9.0	84.886	24. 24.	56./- 1	6.424	و. ا د د د
	82264043	9 6	9.00		55./- 66.64	6.428	9 00
-	8226301	9.0	+ 0 · 0 · 0	7 T	99.9	9.00.0	9 6
·:	83224044	S	00.000 00.000		10.01	6.633	9 9
II	83224045	6	EC 000	4	-10.03	6.426	187
H	82263012	9.9	999.38	0.149	-12.00	6.639	-0.207
-	82263024	0.0	1000.31	9.148	-12.00	6.639	-0 .202
II	83224046	9. 0	1000.15	0.150	-12.07	6.438	-0.205
II	83224047	9 .0	1666.27	0.149	-12.08	6.438	-0.193
II	83224048	6 .0	1666.15	6.156	-12.08	6.436	-0.200
—	82263013		1666.78	0.148	-14.00	6.639	-0.212
-	82263025		1000.08	0.147	-14.00	6.654	-0 .212
Ξ:	83224049		1000.15	0.149	-14.00	6.436	-0.207
ij	83224050	9 .0	999.81	0.149	-14.00	6.432	-0.208
→ •	82263014	0.0	999.26	0.147	-16.00	6.639	-0.212
-4 :	82263026	0.0	96.86	0.147	•	6.652	-0.210
II	83224051		1001.66	0.149	-16.92	6.453	-0.202

Domping, 1/sec	-0.202	-9.205	-0.210	-0.212	-9.207	-9.208	-0.207	-9 .291	-6 .203	-0.206	9	-6.186 186	-6.179	-6.169	9.178	-6 .172	-6 .179	-6.180	-9·186	-6 .169	-0.167	9.177	2	8/1.9	40.10	70. 07	9	-6.185	-0.166	-0.182	6.171	-0.170	a 195	-6.205	-0.286	٠	186	•		-6.194	-0.206	-6.211	12.9	٠	-0 .212
Frequency, Hz	6.440	6.639	6.648	6.432	6.424	•	6.639	6.658	6.447	6.438	6.658	6.643	6.664	6.412	6.428	6.434	6.668	6.650	6.658	6.424	6.428	6.660	6.656	6.646	6.451	0.422	6.632	6.646	6.422	6.432	6.420	6.432	6.639	6.656	6.662	6.648	6.428	6.443	6.432	6.432	6.666	6.646	6.641	6.424	6.424
Shaft angle, deg	-16.03	-18.00	-18.99	-18.00	-17.99	-17.99	-20.00	-20.00	-19.64	-19.64	9	00.00 0	6 .66	0.02	0.02	0.02	-2.00	-2.00	-2.00	-2.06	-2.06	96. †	4.00	90.	08.5- 08.1-	7 G	9 6	98	-5.99	-5.99	-5.99	-5.99	89. 99.	8 . 66 6	89.00 0.00	98. p	-7.99	-7.99	-7.99	-7.99	-10.00	-10.00	•	-10.03	-10.03
Advance	0.148	0.148	0.148	9.148	0.147	0.148	0.148	0.148	9.147	0.147	9.202	0.199	0.200	0.199	0.199	0.197	0.200	9 .199	6 .198	0.201	0.198	9.201	0.201	0.200	9.199	90.0	9.70 0	907.6	0.201	0.199	9.201	9 .198	0.201	6.199	6.286	9.200	٠	•	•	0.196	0.202	٦.	0.198	0.199	0.201
Rotor speed,	1000.62	999.84	999.84	999.81	999.23	998.88	1000.08	1000.43	1001.20	1666.39	1000.55	999.84	1001.72	998.18	999.57	999.92	1001.25	1000.55	1001.13	998.98	999.46	1000.78	1000.90	1666.26	1001.43	30.000 30.000 30.000	98.88	2000 -	66.866	989.82	998.76	999.57	999.02	1000.78	1001.25	989.86	999.11	1000.62	69.666	999.34	1001.13	98.86	999.26	998.88	998.88
Collective pitch, deg	6 .	0.0	9.0	9 .0	0 .	0 .0	9 .0	0 .0	9.6	9 .	0 .0	9 .	9 .0	9 .0	9 .	9 .0	9 .0	0.0	0.0	9.0	9 .0	9 .9	9.	6 .6	9 .	9 · 6	D 6	9 6		9.	9 .0	0 .0	6 .6	. 0	.	o .	.	0 .0	0.0	9 .0	0 .0	0 .0	0 .0	9 .0	9.0
Data point number	83224052	82263015	82263027	83224053	83224054	83224055	82263016	82263028	83224056	83224057	82263029	82264001	82264002	83224062	83224063	83224064	82263030	82264003	82264004	83224065	83224066	82263031	82264905	82264007	83224067	83224068	82263832	07704000	83224069	83224070	83224071	83224072	82263033	82264010	82264011	82264012	83224073	83224074	83224075	83224076	82263034	82264013	82264014	83224077	83224078
Rotor	11		-	11	II	II	-	-	11	11	-	-	-	II	II	II	-	H	-	11	11	-	-	-	II	I.	 •		-	: :	II	11	-	,	H	-	II	11	II	II	H	—	H	I	Π

8.2224407 0.00 100	numbe r	Collective pitch, deg	Rotor speed,	Advance	Shaft angle, deg	requency. Hz	Jomping.
1989 1989	83224079	9 .	999.11	6.199	6	6.428	-6, 196
0.0 0.0	82263035	9.0	1001.60	0.203	-12.00	6.674	-6.199
9.6 (6.48) 9.9 (1.40) (82264015	0 .0	1000.20	6.198	-12.00	6.648	-0.213
8.6 999.34	82264016	0 .	1000.20	0.200	•	6.648	-9.208
8.6 998.534	82264017	9	1001.60	0.199	٠	6.666	-0 .206
8.6 998.53 998.53 99.201 12.22 22 6.418 99.6 999.57 999.57 9.202 112.02 2 6.418 999.57 999.57 9.202 112.02 2 6.418 99.6 999.57 9.202 114.000 6.6 6.422 999.57 9.202 114.000 6.6 6.522 99.6 99.0 99.0 99.0 99.0 99.0 99.0 99.0	83224086		999.34	6.197	•	•	-0 .5 00
9.0 999.57	83224081		998.53	0.201	٠	٠	-0 .202
9.0 999.11	83224082		999.57	0.201	•	6.432	6 .211
1000 08 1000 08 0.202 14.00 0.652 0.0 1000 135 0.193 1-14.00 0.652 0.0 1000 135 0.193 1-14.00 0.652 0.0 1000 127 0.193 1-14.00 0.652 0.0 1000 127 0.193 1-14.00 0.652 0.0 1000 127 0.193 1-14.00 0.642 0.412 0.0 1000 127 0.193 1-14.00 0.642 0.412 0.0 1000 127 0.193 1-14.00 0.642 0.412 0.0 1000 127 0.193 1-14.00 0.642 0.412 0.0 1000 127 0.193 1-14.00 0.642 0.412 0.0 1000 127 0.193 1-16.00 0.642 0.0 1000 127 0.193 1-16.00 0.642 0.0 1000 127 0.193 1-16.00 0.642 0.0 1000 127 0.193 1-16.00 0.642 0.0 1000 127 0.193 1-16.00 0.642 0.0 1000 127 0.193 1-16.00 0.642 0.0 1000 127 0.193 1-16.00 0.642 0.0 1000 127 0.193 1-16.00 0.642 0.0 1000 127 0.193 1-16.00 0.642 0.0 1000 127 0.193 1-16.00 0.642 0.0 1000 127 0.193 1-16.00 0.642 0.0 1000 127 0.193 1-16.00 0.642 0.0 1000 127 0.193 1-16.00 0.642 0.0 1000 127 0.193 1-16.00 0.0 1000 127 0.243 0.244 0.02 0.042 0.042 0.042 1000 127 0.244 0.256 0.042 0.042 0.042 1000 127 0.244 0.256 0.042 0.042 0.042 1000 127 0.244 0.256 0.042 0.042 0.042 1000 127 0.244 0.256 0.042 0.042 0.042 1000 127 0.244 0.256 0.042 0.042 0.042 1000 127 0.244 0.256 0.042 0.042 0.042 1000 127 0.244 0.256 0.042 0.042 0.042 1000 127 0.244 0.256 0.042 0.042 0.042 1000 127 0.244 0.256 0.042 0.042 0.042 1000 127 0.244 0.256 0.042 0.042 0.042 1000 127 0.244 0.256 0.042 0.042 0.042 1000 127 0.244 0.256 0.042 0.042 0.042 1000 127 0.244 0.256 0.042 0.042 0.042 1000 127 0.244 0.256 0.042 0.042 0.042 1000 127 0.244 0.244 0.042 0.042 0.042 1000 127 0.244 0.244 0.042 0.042 0.042 1000 127 0.244	83224083	0 .0	999.11	9.200	-12.02	6.426	-0.203
0.0 10000 43 0.199 -14.00 6.652 -0.0 0.0 10000 78 0.199 -14.00 6.652 -0.0 0.0 10000 78 0.199 -14.00 6.422 -0.0 0.0 10000 15 0.199 -14.00 6.422 -0.0 0.0 10000 15 0.199 -14.00 6.422 -0.0 0.0 10000 15 0.199 -14.00 6.422 -0.0 0.0 10000 15 0.199 -14.00 6.422 -0.0 0.0 10000 15 0.199 -14.00 6.436 -0.0 0.0 10000 15 0.199 -16.00 6.436 -0.0 0.0 10000 15 0.199 -16.00 6.436 -0.0 0.0 1000 15 0.199 -16.00 6.436 -0.0 0.0 1000 15 0.199 -16.00 6.436 -0.0 0.0 1000 15 0.199 -16.00 6.436 -0.0	82263036		1000.08	0.202	-14.00	6.652	-e. 195
1000 78	82264018		1000.43	0.199	-14.00	6.652	-0.200
0.0 1980.55 0.198 -14.00 6.652 -0.98 0.0 1988.99 0.197 -14.00 6.442 -0.99 0.0 1988.97 0.198 -14.00 6.442 -0.90 0.0 1980.15 0.198 -14.00 6.442 -0.90 0.0 1980.15 0.199 -14.00 6.443 -0.90 0.0 1980.16 0.200 -16.00 6.448 -0.90 0.0 1980.16 0.200 -16.00 6.656 -0.90 0.0 1980.17 -16.00 6.656 -0.90 0.0 1990.17 -16.00 6.435 -0.90 0.0 1990.18 0.199 -16.00 6.435 -0.90 0.0 1990.18 0.199 -16.00 6.435 -0.90 0.0 1990.18 0.199 -16.00 6.435 -0.90 0.0 1990.18 0.199 -16.00 6.435 -0.90 0.0	82264019	٠.	1000.78	0.199	-14.00	6.656	-0.196
998.99 91	82264020		1000.55	9.198	-14.00	6.652	
0.0 998.07 0.197 -14.00 6.412 -0.198 -14.00 6.412 -0.198 -14.00 6.412 -0.198 -14.00 6.412 -0.198 -14.00 6.412 -0.198 -14.00 6.412 -0.198 -14.00 6.412 -0.198 -14.00 6.412 -0.198 -14.00 6.412 -0.198 -14.00 6.412 -0.198 -14.00 6.412 -0.198 -16.00 6.628 -0.198 -16.00 6.628 -0.198 -16.00 6.628 -0.198 -	83224084	9.	66,866	961.0	-14.00	6.422	651.6
0.0 10000.27 0.198 -14.00 6.446 -0.438 -0.99 -0.99.49 0.200 -14.00 6.446 -0.438 -0.99 -0.99.49 0.200 -16.00 6.438 -0.99 -0.99.49 -0.200 -16.00 6.438 -0.99	83224085	9	20000	0.197	-14.00		19.
0.0 1000.15 0.193 -14.00 6.438 -0.202 -14.00 6.438 -0.202 -14.00 6.438 -0.202 -16.00 6.438 -0.202 -0.202 -16.00 6.438 -0.202 -0.202 -0.203	83224086	9	1999.27	801	-14 99		2 4
939.43 90.0 939.43 90.0 939.43 90.0 939.96 90.0 939.96 90.0 939.96 90.0 939.97 90.0 939.97 90.0 939.97 90.0 939.97 90.0 939.97 90.0 939.73 90.0 939.7	83224087	9 6	10001	90.0	-14 99	•	9
0.0 999.95 0.200 -16.90 6.552 -0.00 0.0 1999.95 0.199 -16.90 6.552 -0.00 0.0 999.81 0.199 -16.91 6.436 -0.00 0.0 999.87 0.199 -16.91 6.436 -0.00 0.0 999.57 0.199 -16.91 6.435 -0.00 0.0 1999.57 0.199 -16.91 6.435 -0.00 0.0 1999.57 0.200 -18.90 6.656 -0.00 0.0 1999.57 0.200 -18.90 6.658 -0.00 0.0 1990.61 0.200 -18.90 6.658 -0.00 0.0 1990.73 0.200 -20.90 6.658 -0.00 0.0 1990.64 0.200 -20.90 6.658 -0.00 0.0 1990.64 0.200 -20.90 6.658 -0.00 0.0 1990.64 0.200 0.200 6.659 -0.00 <	82263037	•	000	. d	20.41	6.43	9 9
999.95 9	82264031	9.6	n 4 c	707.0	99.91	0.040	9 6
6.6 10000.43 6.129 -16.00 6.556 -9.50 6.6 999.46 6.199 -16.01 6.436 -9.50 6.6 999.81 6.199 -16.01 6.436 -9.50 6.6 999.92 7 6.199 -16.01 6.436 -9.50 6.6 999.92 9 -199 -199 -16.01 6.436 -9.50 6.6 999.57 6.200 -18.00 6.432 -9.50 6.6 1000.03 6.200 -18.00 6.658 -9.50 6.6 1000.03 6.200 -18.00 6.658 -9.50 6.6 1000.03 6.200 -18.00 6.658 -9.50 6.6 1000.03 6.200 -18.00 6.658 -9.50 6.6 1000.03 6.200 -20.00 6.658 -9.50 6.6 1000.03 6.200 -20.00 6.658 -9.50 6.6 1000.03 6.200 6.2	82264021	9.0	000.000	997.9	•	6.65 <i>6</i>	-6.263
9.99	B2264021		1000	907.0	•	6.652	26.192
999.81 909.92 909.93	83224023	D 6	900.43	D 0	•	0.000	197.9
999.57	8122488	9.0	0 t	0.00	٠	0.432	•
999.37 999.38 999.37 999.38 999.38 999.38 999.38 999.39 999.30	8122400	9 6	- 0.00 - 0.00 - 0.00	76.18	•	0.450	٠
6.6 1993.37 18.00 19.00 <td< td=""><td>81224001</td><td>9.0</td><td>\0.000 000</td><td>600</td><td>٠</td><td>204.0</td><td>٠</td></td<>	81224001	9.0	\0.000 000	600	٠	204.0	٠
6.6 1000.08 10	160+77C0		78.888	997.9	•	0.4.0	•
6.6 1990 -18.00 0.082 -18.00 0.082 -18.00 0.082 -18.00 0.082 -18.00 0.082 -18.00 0.082 -18.00 0.082 -20.00 0.082 -20.00 0.082 -20.00 0.082 -20.00 0.082 -20.00 0.082 -0.092 -0.092 -0.092 -0.092 -0.092 -0.092 -0.092 -0.092 0.0	02202020	9.0	1001	997.9	10.00	0.000 0.000	•
6.6 1999.00	47040770	.	1991.84	9.197	13.66	0.082	٠
6.66 -18.86 6.67 -6.69	07740770	3 9 (1666.68	96.0	-18.66	6.658	٠
9.99 51 9.20 -20 96 6.662 -9 -6	82204026	9. 9.	1661.13	0.286	-18.66	6.670	•
9.99.73 0.296 -20.00 6.658 -0. 0.0 1000.43 0.197 -20.00 6.672 -0. 0.0 1000.43 0.251 0.00 6.658 -0. 0.0 1000.97 0.250 0.00 6.452 -0. 0.0 999.92 0.250 0.00 6.452 -0. 0.0 1000.97 0.249 0.02 6.445 -0. 0.0 1000.97 0.249 0.02 6.445 -0. 0.0 1000.97 0.249 0.02 6.445 -0. 0.0 1000.97 0.249 0.02 6.445 -0. 0.0 1000.97 0.248 -2.06 6.445 -0. 0.0 1000.97 0.248 -2.06 6.445 -0. 0.0 1000.97 0.248 -2.06 6.445 -0. 0.0 1000.97 0.249 -2.06 6.445 -0. 0.0 1000.97 0.250 -4.00 6.661 -0. 0.0 0.0	6585838	9 .0	999.01	0.202	-20.66	6.662	
0.0 1000.66 0.199 -20.00 6.672 -0.0 0.0 1000.08 0.251 -0.00 6.658 -0.0 0.0 939.02 0.250 0.00 6.658 -0.0 0.0 939.02 0.249 0.02 6.432 -0.0 0.0 1000.04 0.249 0.02 6.435 -0.0 0.0 1000.04 0.249 0.02 6.435 -0.0 0.0 1000.04 0.249 0.02 6.435 -0.0 0.0 1000.04 0.249 0.29 6.445 -0.0 0.0 1000.09 0.250 -2.06 6.56 -0.0 0.0 1000.09 0.248 -2.06 6.445 -0.0 0.0 1000.09 0.249 -2.06 6.445 -0.0 0.0 1000.00 0.250 -4.00 6.660 -0.0 0.0 0.0 0.250 -4.00 6.61 -0.0 0.0	82264027	9.9	999.73	6.286	-20.00	6.658	-6 .172
0.0 1000.43 0.197 -20.00 6.668 -0. 0.0 1000.08 0.250 0.00 6.645 -0. 0.0 999.92 0.250 0.00 6.445 -0. 0.0 1000.04 0.249 0.02 6.445 -0. 0.0 1000.04 0.249 0.02 6.445 -0. 0.0 999.23 0.249 0.02 6.445 -0. 0.0 1000.97 0.249 -2.00 6.445 -0. 0.0 1000.97 0.249 -2.00 6.445 -0. 0.0 1000.97 0.249 -2.00 6.445 -0. 0.0 1000.97 0.249 -2.00 6.445 -0. 0.0 1000.97 0.249 -2.00 6.445 -0. 0.0 1001.02 0.250 -4.00 6.660 -0. 0.0 999.26 0.250 -4.00 6.660 -0. 0.0 999.26 0.250 -4.00 6.660 -0.	82264028	0 .0	1000.66	6.199	-20.00	6.672	-0.195
6.6 1000.08 0.251 0.00 6.650 -0.00 6.0 999.61 0.250 0.00 6.645 -0.00 6.0 1000.97 0.249 0.02 6.445 -0.00 6.0 1000.99 0.249 0.02 6.445 -0.00 6.0 1000.99 0.249 0.249 0.00 6.445 -0.00 6.0 999.28 0.250 -2.00 6.45 -0.00 6.0 1000.97 0.248 -2.00 6.445 -0.00 6.0 1000.97 0.248 -2.00 6.445 -0.00 6.0 1000.97 0.249 -2.00 6.445 -0.00 6.0 1000.97 0.249 -2.00 6.445 -0.00 6.0 1000.20 -4.00 6.669 -0.00 -0.00 6.0 1000.20 -4.00 6.669 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00	82264029	6 .6	1000.43	6.197	-20.00	6.668	-6.197
0.0 999.61 0.250 0.00 6.645 -0 0.0 999.92 0.250 0.02 6.432 -0 0.0 1000.97 0.249 0.02 6.445 -0 0.0 1000.99 0.249 0.02 6.445 -0 0.0 1000.97 0.250 -2.00 6.650 -0 0.0 1000.97 0.249 -2.00 6.455 -0 0.0 1000.97 0.249 -2.06 6.455 -0 0.0 1001.02 0.249 -2.06 6.455 -0 0.0 1001.02 0.249 -2.06 6.455 -0 0.0 1001.02 0.250 -4.00 6.669 -0 0.0 0.250 -4.00 6.669 -0 0.0 0.250 -4.00 6.661 -0	82264030	0 .0	1000.08	0.251	99.9	6.650	•
0.0 999.92 0.250 0.002 0.445 0.445 0.445 0.002 0.445 0.002 0.445 0.003	82264031	0 .0	999.61	0.250	9 0.0	•	٠
0.0 1000.97 0.249 0.029 6.445 0.249 0.249 0.02 6.434 0.0 0.0 1000.04 0.249 0.02 6.434 0.0<	83224094	0 .0	999.92	0.250	0.02	•	
0.0 1990.04 0.249 0.02 6.434 -0.0 0.0 999.96 0.250 -2.00 6.650 -0.0 0.0 999.84 0.251 -2.00 6.646 -0.0 0.0 1000.97 0.248 -2.06 6.445 -0.0 0.0 1000.97 0.249 -2.06 6.426 -0.0 0.0 1001.02 0.250 -4.00 6.660 -0.0 0.0 999.26 0.250 -4.00 6.660 -0.0	83224095	0.0	1666.97		0.02	6.445	
6.6 999.96 6.256 -2.00 6.656 -0.0 6.0 999.84 6.251 -2.00 6.646 -0.0 6.0 1000.97 0.248 -2.06 6.445 -0.0 6.0 1000.97 0.249 -2.06 6.426 -0.0 6.0 1001.02 0.250 -4.00 6.660 -0.0 6.0 999.26 0.250 -4.00 6.660 -0.0	83224096	8	1000.04		0.02		_
0.0 999.84 0.251 -2.06 6.646 -0. 0.0 1000.97 0.248 -2.06 6.445 -0. 0.0 999.23 0.249 -2.06 6.426 -0. 0.0 1000.97 0.249 -2.06 6.445 -0. 0.0 1001.02 0.250 -4.00 6.660 -0. 0.0 999.26 0.250 -4.00 6.660 -0.	82264032	9.0	96.666		-2.00		
0.0 1000.97 0.248 -2.06 6.445 -0.0 0.0 999.23 0.249 -2.06 6.426 -0.0 0.0 1000.97 0.249 -2.06 6.445 -0.0 0.0 1001.02 0.250 -4.00 6.660 -0.0 0.0 999.26 0.250 -4.00 6.641 -0.0	82264033	6	48.000		-2.86	•	
0.0 999.23 0.249 -2.06 6.426 -0.06 0.0 1000.97 0.249 -2.06 6.445 -0.0 0.0 1001.02 0.250 -4.00 6.660 -0.0 0.0 999.26 0.250 -4.00 6.641 -0.0	83224097	9	1000		-2.96		
6.6 1980.97 9.249 -2.96 6.445 -6.1 6.6 1981.82 6.259 -4.99 6.669 -6.1 6.6 999.26 6.259 -4.99 6.641 -6.1	83224098	9	EC 000	•	-2.96	•	
6.6 1961.62 0.256 —4.96 6.669 —6.1 6.6 999.26 0.256 —4.96 6.641 —6.1	8 122400		1000	i c	20.7	•	. •
6.6 999.26 0.250 -4.06 6.641 -6.1	8227778	9.0	76.000	•	90.7-	•	- •
6.25 6.25 6.54 6.04 6.04 6.04 6.04 6.04 6.04 6.04 6.0	92264934	9.0	79.1991	•	90.4	9.00.0	- '
	82264635	9 .	999.26	0.250	8. †	6.641	٠.

Domping, 1/sec	-0.165	-0.171	-9 .164	-6.199	-6 .192	-0.196	-0.183	-0.185	-0.182	-0.200	-0 .198	-0.207	-0 .200	-0 .202	-9 .201	-0.195	-6.195	-0.195	-6 .182	-6.184	-0.200	-0.197	-0.224	-0.231	-0 .229	-0.216	-0.182	-0.183	-0.187	-0.173	-0.18¢	-e 180	a . 163	-0 .202	٠	. 181 181	-6.18 4	-6.195	-0 .182	-0.176	6 .184	. 18 4	-0.175	-6.177	9 166	-0.172
Frequency, Hz	6.428	6.430	6.434	6.648	6.648	6.664	6.436	6.424	6.428	6.866	6.672	6.436	6.428	6.422	6.639	6.639	6.639	6.639	6.641	6.662	6.639	6.639	6.639	6.672	6.639	6.639	6.639	6.639	6.432	6.424	6.426	6.430	6.443	6.445	6.441	6.434	6.424	6.432	6.432	6.445	6.639	6.639	6.436	6.434	6.441	6.434
Shaft angle, deg	-3.99	-3.99	66.51	-6.90	-6.00	-6.00	-5.92	-5.92	-5.92	8.99	-8.99	-8.60	-8.00	-7.99	-10.00	-10.00	-12.00	-12.00	-14.00	-14.00	-16.00	-16.00	-18.00	-18.00	-20.00	-20.00	9.00	9 .	0.02	90.0	90.0	90.0	6 .88	9 . 9	00.00	9	6.9	-6.01 10.01	40.04	6.04	-2.00	-2.00	-2.62	-2.62	-2 60	-2.02
Advance	0.250	0.251	0.251	0.250	0.250	0.250	0.250	0.249	0.251	0.250	0.249	0.251	0.248	0.248	0.250	0.254	0.252	0.252	0.252	0.252	0.250	0.250	0.252	0.253	0.250	0.250	6.301	6.301	0.297	0.298	9 .299	6.297	9 .298	0.297	0.302	0.298	0.302	0.301	0.298	9.300	9.388	9.301	9.391	299	000	0.300
Rotor speed,	999.34	999.57	1000.04	999.73	999.73	1000.90	1000.04	999.11	999.34	1000.90	1001.48	1666.64	999.34	998.65	1000.55	999.84	1000.90	999.84	998.32	96.66	1666.96	998.55	1000.20	999.38	1000.66	1000.90	999.73	999.14	999.81	888.88	999.46	999.34	1000.62	1000.73	1000.27	899.68	998.76	999.46	1606.15	1001.20	96.666	1666.26	1000.04	0 0 0	1888 52	999.92
Collective pitch, deg	6 .	0.0	0.0	0.0	0.0	0.0	0 .0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.00	9	9	6	9	9.0	9	9.	0.0	9 .0	0.0	9.6	0 .0	0 .0	9 . 0	9 .0	9 .0		9 . 0	9 . 0	0 .0	0.0	9 .0	9.0	9.9	9	9 6	9 6		90
Data point number	83224101	83224102	83224103	82264036	82264037	82264038	83224104	83224105	83224106	82264039	82264040	83224107	83224108	83224109	82264041	82264042	82264043	82264044	82264045	82264046	82264047	82264048	82264049	82264050	82264051	82264052	82264053	82264054	83224110	83224111	83224112	83224113	83228005	83228006	83228007	83228008	83228009	83228010	83229004	83229005	82264055	82264056	83224114	83224115	84224118	83224117
Rotor	11	II	II	, -	-	_	II	I	II	-	-	::	11	II	H			ı þ=-		1 b) p -	1 1			-	-	-	-	II	Ι	II	II	II	II	I	Ξ	II	11	11	<u>-</u>	11	[:::

1	Rotor	Data point number	Collective pitch, deg	Rotor speed, rpm	Advance	Shaft angle, deg	Frequency, Hz	Domping, 1/sec
83228811	-	R1008011	6	007	902	- S	¥17 8	4 1 2 3 3
82228811 0.0 999 23 6.299 7.29 -2.42 6.43 -9.40 6.43 -9.40 6.443 -9.40 6.443 -9.40 6.443 -9.40 6.443 -9.40 6.443 -9.40 6.443 -9.40 6.613 -9.40 6.443 -9.40 6.613 -9.40 6.443 -9.40 6.613 -9.40 6.613 -9.40 6.613 -9.40 6.613 -9.40 6.613 -9.40 6.613 -9.40 6.613 -9.40 6.613 -9.40 6.613 -9.40 6.613 -9.40 6.613 -9.40 6.613 -9.40 6.613 -9.40 6.613 -9.40 6.613 -9.40	II	83228012	9 9	45. 999 45. 989	9.302	-2.02	6.430	9
822228914 0.0 0	11	83228013	0.0	999.23	0.299	-2.02	6.430	-0.177
82264657 0.0 999-84 0.00 999-84 0.00 999-94 0.00	11	83228014	0.0	1000.50	9.301	-2.62	6.445	
822564656 0.0 999.38 0.302 -4.00 6.539 -4.00 6.445 -4.00 6.444 -4.00 6.444 -4.00 6.445 -4.00 6.445 -4.00 6.446 -4.00 6.446 -4.00 6.446 -4.00 6.446 -4.00 6.446 -4.00 6.446 -4.00 6.446 -4.00 6.446 -4.00 6.446 -4.00 6.446 -4.00 6.446	-	82264057	0.0	999.84	9.300	-4.00	6.639	٠.
83228615 0.0 1006.59 -4.01 6.445 -6.44 83228617 0.0 999.46 0.299 -4.01 6.445 -4.01 6.445 -4.01 6.444 -4.01 6.444 -4.01 6.445 -4.01 -6.01 -6.01 6.01 6.02 -6.02	-	82264058	0.0	999.38	0.302	8.7	6.639	٠.
83228916 0.0 999.92 0.299 -4.01 6.444 -4.01 6.444 -4.01 6.444 -4.01 6.444 -4.01 6.444 -4.01 6.444 -4.01 6.444 -4.01 6.444 -4.01 6.444 -4.01 6.444 -4.01 6.444 -4.01 6.444 -4.01 6.444 -4.01 6.444 -4.01 6.444 -4.01 6.444 -4.01 6.444 -4.01 6.444 -4.01 6.444 -4.01 6.449 -6.539 -4.01 6.449 6.539 -6.539 -6.596 6.539 -6.596 6.449 6.539 -6.596 6.449 6.539 -6.596 6.449 6.539 -6.596 6.449 6.539 -6.596 6.449 6.539 -6.596 6.449 6.539 -6.596 6.449 6.539 -6.596 6.449 6.539 -6.596 6.449 6.539 -6.596 6.449 6.539 -6.596 6.449 6.449 6.539 -6.596 6.449 6.539	II	83228015	0.0	1000.50	0.300	14.01	6.445	-0.163
83228917 0.0 999,46 0.297 -4,81 6,44 -6,24 -6,44 -6,24 -6,44 -6,44 -6,44 -6,44 -6,24 -6,44 -6,44 -6,24 -6,44 -6,44 -6,24 -6,44 -6,24 -6,44 -6,24 -6,44 -6,24 -6,44 -6,24 -6,44 -6,24 -6,44 -6,24 <t< td=""><td>II</td><td>83228016</td><td>0.0</td><td>999.92</td><td>0.299</td><td>14.01</td><td>6.440</td><td>-6.171</td></t<>	II	83228016	0.0	999.92	0.299	14.01	6.440	-6.171
8.2228918 0.0 1999.46 0.297 -4.01 6.434 -9.8 8.2228918 0.0 1999.46 0.298 -6.90 6.539 -6.90 6.539 -6.90 6.539 -6.90 6.539 -6.90 6.539 -6.90 6.539 -6.90 6.539 -6.90 6.539 -6.90 6.539 -6.90 6.539 -6.90 6.539 -6.90 6.539 -6.90 6.424 -6.90 6.424 -6.90 6.424 -6.90 6.424 -6.90 6.428	11	83228017	9.9	999.46	0.297	-4.01	6.434	6.179
822264659 0.0 1000.0 0.0 <t< td=""><td>I</td><td>83228018</td><td>0.0</td><td>999.46</td><td>0.297</td><td>-4.01</td><td>6.434</td><td></td></t<>	I	83228018	0.0	999.46	0.297	-4.01	6.434	
83228466 0.0 0.28 -5.96 6.53 -6.99 6.424 -6.99 6.424 -6.99 6.424 -6.99 6.424 -6.99 6.424 -6.99 6.424 -6.99 6.424 -6.99 6.424 -6.99 6.424 -6.99 6.428 -6.99 6.429 -6.99	-	82264059	0.0	1000.08	0.239	-6.00	6.639	-0.204
83228819 0.0 998.53 0.288 -5.96 6.424 -6.98 6.428 -6.96 6.428 -6.96 6.428 -6.96 6.428 -6.96 6.428 -6.96 6.428 -6.96 6.428 -6.96 6.428 -6.96 6.428 -6.96 6.429 -6.96 6.429 -6.96 6.429 -6.96 6.429 -6.96 6.429 -6.96 6.429 -6.96 6.429 -6.96 6.429 -6.96 6.429 -6.96 6.429 -6.96 6.439 -6.96 6.439 -6.96 6.439 -6.96 6.439 -6.96 6.439 -6.96 6.439 -6.96 6.439 -6.96 6.439 -6.96 6.439 -7.99 6.439 -6.96 6.439 -7.99 6.439 -6.96 6.449 6.239 -7.99 6.445 -6.96 6.445 -6.96 6.445 -6.96 6.445 -6.96 6.445 -6.96 6.445 -6.96 6.445 -6.96 6.449 -6.96 <	—	82264060	0.0	1666.26	0.298	99.9-	6.639	-0.201
83228629 0.0 998.98 0.286 -5.96 6.428 -6.96 6.428 -6.96 6.428 -6.96 6.428 -6.96 6.428 -6.96 6.428 -6.96 6.428 -6.96 6.428 -6.96 6.428 -6.96 6.428 -6.96 6.449 -6.96 6.449 -6.96 6.449 -6.96 6.449 -6.96 6.449 -6.96 6.449 -6.96 6.449 -6.96 6.449 -6.96 6.449 -6.96 6.449 -6.96 6.449 -6.96 6.449 -6.96 6.449 -6.39 -7.99 6.445 -6.449 <td>II</td> <td>83228019</td> <td>0.0</td> <td>998.53</td> <td>0.298</td> <td>-5.96</td> <td>6.424</td> <td>-9.185</td>	II	83228019	0.0	998.53	0.298	-5.96	6.424	-9 .185
83228021 0.0 998.99 0.288 -5.96 6.436 -6.539 -6.436 -6.539 -6.446 -6.539	I	83228020	0.0	998.88	0.300	-5.96	6.428	-0.196
B.2228922 0.0 1998.41 0.399 -5.96 6.422 -6.29	Ξ.	83228021	0.0	998.99	0.298	-5.96	6.430	-0.190
B.2254022 0.0 10000.04 0.297 -5.96 6.444 -6.39 -6.44 -6.39 -6.44 -6.39 -6.44 -6.39 -6.49 6.445 -6.39 -6.49 6.449 -6.39 -6.49 6.449 -6.39 -6.49 6.539 -6.39 -6.49 6.539 -6.49 6.539 -6.49 6.539 -6.49 6.539 -6.49 6.539 -6.44 -6.39 -6.45 -6.45 -6.45 -6.45 -6.45 -6.45 -6.45 -6.45 -6.45 -6.45 -6.45 -6.45 -6.45	II	83228022	0.0	998.41	9.366	-5.96	6.422	٠.
82264661 9.0 1000-03 0.299 -8.00 6.639 -0.639 -0.639 -0.639 -0.639 -0.639 -0.639 -0.639 -0.639 -0.639 -0.639 -0.639 -0.639 -0.639 -0.639 -0.639 -0.639 -0.639 -0.639 -0.645 <td>I</td> <td>83228023</td> <td>0.0</td> <td>1000.04</td> <td>0.297</td> <td>-5.96</td> <td>6.440</td> <td>-0.193</td>	I	83228023	0.0	1000.04	0.297	-5.96	6.440	-0.193
83228462 0.0 1000 43 0.299 -8.00 6.53 -9.00 83228624 0.0 1000 73 0.299 -7.99 6.449 -0.00 83228625 0.0 1000 73 0.297 -7.99 6.449 -0.00 83228625 0.0 1000 73 0.299 -7.99 6.451 -0.00 83228625 0.0 1000 1.13 0.299 -7.99 6.451 -0.00 82264064 0.0 1000 1.37 0.299 -10.00 6.539 -0.445 -0.00 82264065 0.0 1000 1.37 0.299 -10.00 6.539 -0.639 <td>-</td> <td>82264061</td> <td>0.0</td> <td>1000.08</td> <td>6.288</td> <td>8.00</td> <td>6.639</td> <td>-9. 196</td>	-	82264061	0.0	1000.08	6.288	8.00	6.639	-9 . 196
83228824 0.0 1000.73 0.390 -7.99 6.445 -0 83228825 0.0 1000.73 0.297 -7.99 6.445 -0 83228825 0.0 1000.43 0.299 -7.99 6.457 -0 83228025 0.0 1000.43 0.299 -7.99 6.457 -0 82284065 0.0 1000.13 0.299 -10.00 6.457 -0 82284065 0.0 1000.134 0.299 -10.00 6.539 -0 82284066 0.0 1001.14 0.300 -12.00 6.639 -0 82284066 0.0 1001.14 0.300 -14.00 6.639 -0 82284070 0.0 1000.14 0.300 -14.00 6.639 -0 82284071 0.0 1000.14 0.300 -14.00 6.639 -0 82284071 0.0 1000.43 0.299 -14.00 6.639 -0 822844071 0.0	-	82264062	0.0	1000.43	6.23	-8.00	6.639	-0.202
83228925 0.0 1000.73 0.297 -7.59 6.445 -0 83228926 0.0 1001.43 0.297 -7.59 6.457 -0 83228927 0.0 1001.13 0.299 -7.99 6.457 -0 832264965 0.0 1001.37 0.299 -10.00 6.53 -0 82264965 0.0 1001.37 0.299 -12.00 6.53 -0 82264965 0.0 1001.37 0.299 -12.00 6.53 -0 82264965 0.0 1001.34 0.299 -14.00 6.53 -0 82264967 0.0 1001.34 0.299 -14.00 6.639 -0 8226497 0.0 1000.20 399.36 0.299 -14.00 6.639 -0 8226407 0.0 1000.20 399.36 0.299 -16.00 6.639 -0 8226407 0.0 1000.20 0.0 1000.20 0.299 -16.00 6.639 <td>11</td> <td>83228024</td> <td>9</td> <td>1000.73</td> <td>9.399</td> <td>-7.99</td> <td>6.449</td> <td>-0.203</td>	11	83228024	9	1000.73	9.399	-7.99	6.449	-0.203
83228826 0.0 1001.43 0.299 -7.99 6.457 -0.258627 0.0 1001.13 0.299 -7.99 6.457 -0.299 -7.99 6.457 -0.299 -10.00 6.457 -0.299 -10.00 6.639 -0.299 -10.00 6.639 -0.299 -10.00 6.639 -0.299 -10.00 6.639 -0.299 -10.00 6.639 -0.299 -10.00 6.639 -0.299 -12.00 6.639 -0.299 -12.00 6.639 -0.299 -12.00 6.639 -0.299 -12.00 6.639 -0.299 -12.00 6.639 -0.299 -14.00 6.639 -0.299 -14.00 6.639 -0.299 -14.00 6.639 -0.299 -14.00 6.639 -0.299 -14.00 6.639 -0.299 -14.00 6.639 -0.299 -14.00 6.639 -0.299 -14.00 6.639 -0.299 -14.00 6.639 -0.299 -14.00 6.639 -0.299 -14.00 6.639 -0.299 -14.00		83228025	0.0	1000.73	0.297	-7.99	6.445	-0.207
83228027 0.0 1000.85 0.360 -7.99 6.451 -0 82264064 0.0 1001.37 0.299 -10.00 6.639 -0 82264065 0.0 1001.37 0.299 -12.00 6.639 -0 82264065 0.0 1001.37 0.299 -12.00 6.639 -0 82264066 0.0 1001.37 0.299 -12.00 6.639 -0 82264066 0.0 1001.34 0.299 -14.00 6.639 -0 82264076 0.0 1000.43 0.299 -14.00 6.639 -0 82264071 0.0 1000.43 0.299 -14.00 6.639 -0 82264072 0.0 1000.43 0.299 -16.00 6.639 -0 82264073 0.0 1001.13 0.299 -18.00 6.639 -0 82264074 0.0 1001.13 0.299 -18.00 6.639 -0 82264075 0.0 <td></td> <td>83228026</td> <td>0.0</td> <td>1001.43</td> <td>6.288</td> <td>-7.99</td> <td>6.457</td> <td>-0.202</td>		83228026	0.0	1001.43	6.288	-7.99	6.457	-0.202
1 82264063 0.0 1000.43 0.299 -10.00 6.539 -0 1 82264064 0.0 1000.43 0.299 -12.00 6.639 -0 1 82264065 0.0 1001.84 0.299 -12.00 6.639 -0 1 82264065 0.0 1001.84 0.299 -14.00 6.639 -0 1 82264067 0.0 1001.84 0.299 -14.00 6.639 -0 1 8226407 0.0 1000.43 0.299 -14.00 6.639 -0 1 8226407 0.0 1000.43 0.299 -14.00 6.639 -0 1 8226407 0.0 1000.43 0.299 -16.00 6.639 -0 1 8226407 0.0 1000.43 0.299 -16.00 6.639 -0 6.639 -0 6.639 -0 6.639 -0 6.639 -0 6.639 -0 6.639 -0	II	83228027	0.0	1000.85	9.300	-7.99	6.451	-0.197
I 82264064 0.0 1000 43 0.299 -10.00 6.539 -0 I 82264065 0.0 1001 37 0.300 -12.00 6.539 -0 I 82264065 0.0 1001 37 0.300 -14.00 6.639 -0 I 82264065 0.0 1000 33 0.299 -14.00 6.639 -0 I 8226407 0.0 1000 43 0.299 -14.00 6.639 -0 I 8226407 0.0 1000 43 0.299 -16.00 6.639 -0 I 8226407 0.0 1000 13 0.299 -16.00 6.639 -0 I 8226407 0.0 1000 13 0.299 -16.00 6.639 -0 I 8226407 0.0 1000 13 0.299 -16.00 6.639 -0 I 8226407 0.0 0.0 0.299 -16.00 6.639 -0 I 8226407	I	82264063	0.0	1001.13	0.299	-10.00	6.639	-0.185
I 82264065 0.0 1001.37 0.300 -12.00 6.639 -0 I 82264066 0.0 1001.84 0.299 -12.00 6.639 -0 I 82264068 0.0 999.36 0.299 -14.00 6.639 -0 I 82264068 0.0 1000.43 0.299 -14.00 6.639 -0 I 82264071 0.0 1000.43 0.299 -14.00 6.639 -0 I 82264071 0.0 1000.43 0.297 -16.00 6.639 -0 I 82264077 0.0 1000.13 0.295 -18.00 6.639 -0 I 82264074 0.0 1000.13 0.295 -18.00 6.639 -0 I 82264075 0.0 1000.13 0.295 -18.00 6.639 -0 I 82264076 0.0 1000.08 0.348 0.299 -18.00 6.639 -0 I	-	82264064	0.0	1000.43	6.299	-10.00	6.639	-6 .191
I 82264666 9.0 1001.84 0.299 -12.00 6.639 -0 I 82264067 0.0 999.96 0.309 -14.00 6.639 -0 I 82264068 0.0 999.84 0.299 -16.00 6.639 -0 I 82264070 0.0 1000.43 0.299 -16.00 6.639 -0 I 82264071 0.0 1000.43 0.299 -16.00 6.639 -0 I 82264071 0.0 1001.13 0.299 -18.00 6.639 -0 I 82264074 0.0 1001.67 0.299 -18.00 6.639 -0 I 82264074 0.0 1001.69 0.299 -18.00 6.639 -0 I 82264076 0.0 1000.08 0.361 0.00 6.639 -0 I 82264077 0.0 1000.08 0.346 0.00 6.639 -0 I 82264078 </td <td>H</td> <td>82264065</td> <td>0.0</td> <td>1001.37</td> <td>0.300</td> <td>-12.00</td> <td>6.639</td> <td>-0.189</td>	H	82264065	0.0	1001.37	0.300	-12.00	6.639	-0.189
I 82264067 0.0 999.96 0.360 -14.00 6.539 -0 I 82264068 0.0 0.0 1999.38 0.299 -14.00 6.639 -0 I 8226407 0.0 1000.43 0.299 -16.00 6.639 -0 I 8226407 0.0 1001.13 0.295 -18.00 6.639 -0 I 8226407 0.0 1001.13 0.295 -18.00 6.639 -0 I 8226407 0.0 1001.13 0.295 -18.00 6.639 -0 I 8226407 0.0 1001.14 0.295 -20.00 6.639 -0 I 8226407 0.0 1000.08 0.361 -20.00 6.639 -0 I 8226407 0.0 1000.08 0.361 0.36 6.639 -0 I 8226407 0.0 1000.08 0.36 0.36 0.639 -0 I <	_	82264066	0.0	1001.84	0.239	-12.00	6.639	-9 .193
I 82264068 0.0 999.38 0.299 -14.00 6.639 -0 I 82264070 0.0 1000.43 0.299 -16.00 6.639 -0 I 82264071 0.0 1000.20 0.299 -16.00 6.639 -0 I 82264072 0.0 1001.13 0.299 -18.00 6.639 -0 I 82264074 0.0 1001.60 0.299 -18.00 6.639 -0 I 82264074 0.0 1001.60 0.299 -20.00 6.639 -0 I 82264074 0.0 1000.08 0.250 0.00 6.639 -0 I 82264076 0.0 1000.43 0.348 0.348 0.00 6.639 -0 I 82264078 0.0 1000.43 0.348 0.360 6.639 -0 I 82254079 0.0 1000.43 0.348 0.36 0.00 6.639 -0 <tr< td=""><td>-</td><td>82264067</td><td>0.0</td><td>98.86</td><td>9.300</td><td>-14.00</td><td>6.639</td><td>9.244</td></tr<>	-	82264067	0.0	98.86	9.300	-14.00	6.639	9.244
I 82264069 0.0 999.84 0.301 -16.00 6.684 -0 I 82264070 0.0 1000.43 0.299 -16.00 6.639 -0 I 82264072 0.0 1000.13 0.299 -16.00 6.639 -0 I 82264073 0.0 1000.13 0.299 -18.00 6.639 -0 I 82264074 0.0 999.84 0.299 -20.00 6.639 -0 I 82264075 0.0 1000.03 0.301 -20.00 6.639 -0 I 82264076 0.0 1000.03 0.348 0.301 -20.00 6.639 -0 I 82264077 0.0 1000.03 0.348 0.00 6.639 -0 I 82264076 0.0 1000.043 0.348 0.00 6.639 -0 I 82264077 0.0 1000.044 0.350 0.00 6.639 -0 I	-	82264068	0.0	999.38	0.299	-14.00	6.639	-0.242
I 82264070 0.0 1000.43 0.299 -16.00 6.639 -0 I 82264071 0.0 1000.13 0.297 -16.00 6.639 -0 I 82264072 0.0 1001.13 0.295 -18.00 6.639 -0 I 82264074 0.0 0.0 1001.60 0.295 -18.00 6.639 -0 I 82264074 0.0 0.0 0.295 -20.00 6.639 -0 I 82264075 0.0 0.0 0.360 6.639 -0 6.639 -0 I 82264075 0.0 0.0 0.348 0.36 6.639 -0 6.639 -0 6.639 -0 6.639 -0 6.639 -0 6.639 -0 6.639 -0 6.639 -0 6.639 -0 6.639 -0 6.639 -0 6.639 -0 6.639 -0 6.639 -0 6.639 -0 6.639	-	82264069	0.0	999.84	0.301	-16.00	6.684	-0.308
I 82264071 0.0 1000.20 0.297 -16.00 6.639 -0 I 82264072 0.0 1001.13 0.295 -18.00 6.639 -0 I 82264074 0.0 1001.60 0.295 -18.00 6.639 -0 I 82264074 0.0 999.84 0.295 -18.00 6.639 -0 I 82264076 0.0 1000.03 0.361 -20.00 6.639 -0 I 82264076 0.0 1000.43 0.348 0.00 6.639 -0 I 82264078 0.0 1000.43 0.348 0.00 6.639 -0 I 82264078 0.0 1000.43 0.350 0.00 6.639 -0 I 82264078 0.0 1000.43 0.350 0.00 6.639 -0 I 83229006 0.0 1000.43 0.350 0.00 6.426 -0 I 83229008	-	82264070	0.0	1000.43	6.298	-16.00	6.639	-0 .277
I 82264072 0.0 1001.13 0.299 -18.00 6.639 -0 I 82264073 0.0 1001.60 0.295 -18.00 6.639 -0 I 82264074 0.0 0.0 0.295 -20.00 6.639 -0 I 82264075 0.0 1000.03 0.350 0.00 6.639 -0 I 82264076 0.0 1000.43 0.350 0.00 6.639 -0 I 82264077 0.0 1000.43 0.350 0.00 6.639 -0 I 82264078 0.0 1001.48 0.350 0.00 6.639 -0 I 82264079 0.0 1001.48 0.353 0.00 6.639 -0 I 82264079 0.0 1000.08 0.350 0.00 6.639 -0 I 83229006 0.0 0.0 0.350 0.00 6.424 -0 I 8226408 0	-	82264071	0.0	1000.20	0.297	-16.00	6.639	-0.274
I 82264073 0.0 1001.60 0.295 -18.00 6.639 -0 I 82264074 0.0 999.84 0.299 -20.00 6.639 -0 I 82264075 0.0 1000.08 0.361 -20.00 6.639 -0 I 82264076 0.0 1000.08 0.350 0.00 6.639 -0 I 82264078 0.0 1000.08 0.350 0.00 6.639 -0 I 82264078 0.0 1000.08 0.350 0.00 6.639 -0 I 82264078 0.0 1000.08 0.350 0.00 6.639 -0 I 822264078 0.0 1000.08 0.356 0.00 6.424 -0 I 83229006 0.0 999.46 0.356 -0.01 6.424 -0 I 83229008 0.0 999.57 0.350 -0.01 6.426 -0 I 832264080	-	82264072	0.0	1001.13	0.299	-18.00	6.639	-0.293
I 82264074 0.0 999.84 0.299 -20.00 6.639 -0 I 82264075 0.0 0.0 0.301 -20.00 6.639 -0 I 82264076 0.0 1000.08 0.348 0.00 6.639 -0 I 82264078 0.0 1000.43 0.348 0.00 6.639 -0 I 82264078 0.0 1000.08 0.350 0.00 6.639 -0 I 82264078 0.0 1000.08 0.350 0.00 6.639 -0 I 83229066 0.0 1000.08 0.346 -0.01 6.424 -0 I 83229087 0.0 939.46 0.356 -0.01 6.424 -0 I 83229088 0.0 939.57 0.350 -0.01 6.426 -0 I 83229099 0.0 939.84 0.349 -0.02 6.426 -0 I 82264080 <t< td=""><td>-</td><td>82264073</td><td>0.0</td><td>1001.60</td><td>0.295</td><td>-18.00</td><td>6.639</td><td>-0.293</td></t<>	-	82264073	0.0	1001.60	0.295	-18.00	6.639	-0.293
I 82264075 0.0 999.96 0.301 -20.00 6.639 -0 I 82264076 0.0 1000.08 0.348 0.00 6.639 -0 I 82264077 0.0 1000.43 0.348 0.00 6.639 -0 I 82264078 0.0 1001.48 0.350 0.00 6.639 -0 I 82264079 0.0 1001.48 0.350 0.00 6.639 -0 I 83229006 0.0 999.46 0.356 -0.00 6.639 -0 I 83229006 0.0 999.46 0.346 -0.01 6.424 -0 I 83229008 0.0 999.57 0.350 -0.01 6.428 -0 I 83229008 0.0 999.88 0.350 -0.01 6.426 -0 I 83220008 0.0 999.84 0.350 -0.01 6.426 -0 I 82264080 <	-	82264074	0 .0	999.84	0.299	-20.00	6.639	-0.326
I 82264076 0.0 1000.08 0.350 0.00 6.639 -0 I 82264077 0.0 1000.43 0.348 0.00 6.639 -0 I 82264078 0.0 1001.48 0.350 0.00 6.639 -0 I 82264078 0.0 1001.48 0.350 0.00 6.639 -0 I 83229006 0.0 999.46 0.346 -0.01 6.424 -0 I 83229008 0.0 999.69 0.350 -0.01 6.428 -0 I 83229008 0.0 999.57 0.350 -0.01 6.428 -0 I 83229008 0.0 999.88 0.350 -0.01 6.426 -0 I 83229009 0.0 999.84 0.350 -0.02 6.426 -0 I 832264080 0.0 999.84 0.351 -2.00 6.635 -0 I 899.37 <td< td=""><td>-</td><td>82264075</td><td>0.0</td><td>96.666</td><td>9.301</td><td>-20.00</td><td>6.639</td><td>-0.348</td></td<>	-	82264075	0.0	96.666	9.301	-20.00	6.639	-0.348
I 82264077 0.0 1000.43 0.348 0.00 6.639 0.0 I 82264078 0.0 1001.48 0.350 0.00 6.639 0.0 I 82264079 0.0 1000.08 0.353 0.00 6.639 0.0 I 83229006 0.0 999.46 0.346 0.0 6.424 0.0 I 83229007 0.0 999.69 0.350 0.0 6.426 0.0 I 83229008 0.0 999.89 0.350 0.0 6.426 0.0 I 83229009 0.0 999.84 0.350 0.0 6.426 0.0 I 832264080 0.0 999.84 0.354 0.200 6.639 0.0 I 82264080 0.0 998.32 0.351 -2.00 6.635 0.0 I 82264081 0.0 998.32 0.351 -2.00 6.635 0.0	-	82264076	0.0	1000.08	9.350	0.00	6.639	-0.215
I 82264078 0.0 1001.48 0.350 0.00 6.639 -0 I 82264079 0.0 1000.08 0.353 0.00 6.639 -0 I 8322906 0.0 999.46 0.346 -0.01 6.424 -0 I 8322908 0.0 999.57 0.350 -0.01 6.428 -0 I 8322908 0.0 999.57 0.350 -0.01 6.426 -0 I 8322408 0.0 999.57 0.350 -0.02 6.426 -0 I 8322408 0.0 998.84 0.354 -0.02 6.426 -0 I 8226408 0.0 998.84 0.351 -2.00 6.639 -0 I 8226408 0.0 998.32 0.351 -2.00 6.635 -0	-	82264077	0.0	1000.43	9.348	0.00	6.639	-0.181
I 82264079 0.0 10000.08 0.353 0.00 6.639 -0 I 8322906 0.0 999.46 0.346 -0.01 6.424 -0 I 83229007 0.0 999.59 0.350 -0.01 6.428 -0 I 83229008 0.0 999.57 0.350 -0.01 6.426 -0 I 83224009 0.0 998.84 0.351 -2.00 6.639 -0 I 82264080 0.0 998.32 0.351 -2.00 6.635 -0 I 82264081 0.0 998.32 0.351 -2.00 6.635 -0	-	82264078	0.0	1001.48	0.350	0.00	6.639	-0.212
I 83229006 0.0 999.46 0.346 -0.01 6.424 -0 I 83229007 0.0 999.69 0.350 -0.01 6.428 -0 I 83229008 0.0 999.57 0.350 -0.02 6.426 -0 I 83229009 0.0 998.88 0.349 -0.02 6.418 -0 I 82264080 0.0 999.84 0.351 -2.00 6.639 -0 I 82264081 0.0 998.32 0.352 -2.00 6.635 -0	-	82264079	0.0	1000.08	0.353	9 .00	6.639	-0.194
I 83229007 0.0 999.69 0.350 -0.01 6.428 -0 I 83229008 0.0 999.57 0.350 -0.02 6.426 -0 I 83229009 0.0 998.88 0.349 -0.02 6.418 -0 I 82264080 0.0 999.84 0.351 -2.00 6.639 -0 I 82264081 0.0 998.32 0.352 -2.00 6.635 -0	II	83229006	0.0	999.46	9.346	-6.61	6.424	-0.195
I 83229008 0.0 999.57 0.350 -0.02 6.426 -0 I 83229009 0.0 998.88 0.349 -0.02 6.418 -0 I 82264080 0.0 999.84 0.351 -2.00 6.639 -0 I 82264081 0.0 998.32 0.352 -2.00 6.635 -0	II	83229007	0.0	69.666	0.350	6.61	6.428	
I 83229009 0.0 998.88 0.349 -0.02 6.418 -0 I 82264080 0.0 999.84 0.351 -2.00 6.639 -0 I 82264081 0.0 998.32 0.352 -2.00 6.635 -0	11	83229008	0.0	999.57	0.350	-6.62	6.426	-0 .183
82264089	II	83229009	0.0	998.88	0.349	-0.02	6.418	-6.194
82264081 0.0 998.32 0.352 -2.00 6.635 -0	-	82264080	9.0	999.84	9.351	-2.00	6.639	-0.189
	-	82264081	9,0	998,32	0.352	-2.00	6.635	-9 .188

Damping, 1/sec	Τ.	┰.	-0.180	-9.184	٠.	-0.190	- 6 . 183	-0.175	٠.	-0.186	-0.203		٠.	•	-0.203	6 .211	-0 .203	-6 .200	-0 .225	-6.237	-0 .219	-0.220	-6.325	-6.327	e .3/3	7 to . o	96.09	6.4.5 5.4.5	-6.363 - 161	20.00	64.4	404	436	-8.195		-0.217	-0.204	-0.196	-0.204	-0.202	-0.208	-0.223	-9 .296	-0.187	-0.194	
Frequency,	6.424	6.422	6.434	6.434	6.637	6.639	6.424	6.430	6.422	6.455	6.639	6.639	6.416	6.424	6.428	6.422	6.639	6.639	6.639	6.639	6.639	6.639	6.639	6.639	6.639	6.686	6.695	6.691	6.689	9.0	0.000		A 749	6.645	6.639	6.652	6.428	6.424	6.441	6.451	6.637	6.643	6.418	6.412	6.428	
Shaft angle, deg	-1.99	-1.99	-1.99	-1.99	8 . †	8 8. †	4.02	-4.63	14.03	4.63	96.9-	8 8.9	-5.98	-5.98	-5.98	-5.98	8 .80	-8.00	-10.00	-10.00	-10.00	-16.66	-12.00	-12.00	-14.00	-14.00	-16.90	-16.66	-16.90	99.91-	18.00	90.00	00.02	99.6	9	90.0	9	99.9	99.99	00.00	-2.00	-2.00	-1.99	-1.99	-1.99	
Advance	0.350	0.351	0.350	0.349	•	٠	•	0.349	0.348	0.347	0.349	0.351	6.349	6.351	0.349	9.351	0.351	0.350	m	9.352	0.349	9.348	9.349	6.356	9.350	9.340	9.351	9.358	6.356	9.338	9.726	9.336 8.448	9 4	400	100	6.400		9.396		6.398	9.401		6.401	0.400	0.400	
Rotor speed, rpm	999.23	999.23	1000.27	1666.64	998.67	1666.31	48.866	69.666	999.11	1001.90	1666.43	999.84	998.65	939.69	69.666	998.99	1000.43	1666.26	1000.55	1000.08	1000.90	1001.25	1666.08	999.84	999.49	1000.65	1000.55	1000.43	1666.26	1666.96	989.88	1990 1	4	1888.38	900 73	1000.55	900 11	900	1000,85	1001.55	999,02	999.49	998,65	998.18	999.46	
Collective pitch, deg	9.0	9 .0	0 .0	9 .0	9 .0	9 .0	9 .0	9.6	9. 0	9 .0	0 .0	9 .0	9 .0	9 .0	9 .0	0.0	0 .0	9.0	9.0	0.0	0.0	6 .6	.	9 .0	9 .	6 .	6 .	Ø.		9.0	9 .0	. 6	9.6	P 6	• •	9.6	9 6	9.6	6	9	6	6	6	9	· •	
Data point number	83229010	83229011	83229012	83229013	82264082	82264083	83229014	83229015	83229016	83229017	82264084	82264085	83229018	83229019	83229020	83229021	82264086	82264087	82264088	82264089	82265001	82265002	82265003	82265004	82265005	82265006	82265007	82265008	82265009	82265010	82265011	21002720	022000	82265014 82265015	82265816	82265017	0100000	83229023	83229024	83229025	82265018	82265019	83229026	83229027	83229028	
Rotor	ш	Ξ	II	II	-	-	II	II	II	II	-	-	=======================================	Ξ	II	II		-		-	-				.	-	-		} 1	—	,	 -	-, - -	→ 	• -	- I	• =	: -	: 	:=		• •	·	:=	H	

Damping, 1/sec		-6.207	-0.208	-0.198	-6 . 185	-0 .203	-6.183	. 191 191	-0.213	-0.214	-0.218	-0.219	-6.313	9.538	285.09	+ 8 2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	45.5	9.474	-0.471	-0.237	-9.236	4.221	-6.216	-0.217	-0.214	-6.209	9.22/	-6.199	-0.201	-0.205	-0.201	- 4 - 4 - 4 - 4	6 - 6	-6.199	-0.200	-0.208	-0.261	-0.272	-6.417	59.9	•	997 9
Frequency, Hz		6.436	6.670	6.654	6.438	6.436	6.438	6.440	6.643	6.648	6.641	6.645	6.643	9.00.0	0.007 6.688	5 781	6.688	6.717	6.705	6.658	6.646	6.438	6.434	6.654	6.650	6.656	6.432	6.438	6.426	99.9	6.654	0.4.0 A.4.0	6.441	6.434	6.658	6.656	•	•	•	200 000 000 000 000 000 000 000 000 000	٠	900
Shaft angle, deg		-1.99	8 .†	8.7	-3.99	-3.99	9 . †	7.80	98·9	-6.90 -	89 (P	86.69	8 . e) 0.000 0.00	•	14.80	-14.00	-14.00	-16.99	9.00	9 9 9 9	- e	98.	-2.60	•	9. S.	-1.97	-1.97	-1.98	8.7	8.7	;	70.7	•	•	-6.00	8.8 9	•	-16.66		99.51	40 00
Advance rat io		0.398	0.399	9.400	0.402	9.401	9.401	0.396	0.401	6.400	0.402	6.401	6.462	463	9.462	9.401	69:388	9.400	0.396	0.450	6.451	6.448	0.447	0.450	9.446	6.4.0 6.4.0	6.49	6.451	6.449	0.452	6.456 6.456	453	0.448	0.449	0.450	0.448	0.453	0.451	6.447	74.0 74.0	•	97.0
Rotor speed,		1000.04	1001.72	1000.43	1000.15	1000.04	1000.15	1000.27	999.38	1000.08	999.02	999.38	0.00	- 0000	1888.00	1000.31	999.26	1001.37	999.73	1666.43	999.49	69.00	89.68	1666.68	999.61	900.00	09.00 000	1000.04	998.99	1000.66	999.61	75. 666	1000.39	999.92	1000.55	1000.20	1666.78	999.49	1000.08	1000.33	2.000	1000
Collective pitch, deg		9.0	Ø.	9 .0	9 .0	9 .0	9 .9	0.0	0 .0	9 .0	9 .0	9 G	9 6	9 6	9 6	9	0.0	6.0	9 .0	6 .6	5) d	9 6	9.0	9 .0	6	p	9 6	0.0	0.0	8 9 (s e		9.	9.0	0 .0	6 .		•	9 G	9 6		5
Data point number		83229029	82265020	82265021	83229030	83229031	83229032		82265022	6286323	47,000,00 600,000	C70C0770	82265027		82265029	82265930	82265031	82265032	82265034	82265035	8122635	83229036	83229037	82265037	82265038	8226593	83229038	83229039	83229040	82265041	83229842	83229043	83229044	83229045	82265043	82265044	82265045	6220046	82265047	82265040	BOOKER	ないないと
Rotor	;	II.	→.	→ F	:		.	-	→ +		t-	- -	•		-	-	-	-	⊢ 4 1		. .	II	II	,		•	II.	II	II		II	II	II	Ī	٦,	٠,	p		- I	•		

ncy, Damping, 1/sec	25 598	9	•		•	_	-	54 —0.235	P	9	ę ,	•	9	P	9	ę	9	9	9	9	54 - 9.296	9	9	٠. ٩	9	φ' _'	\$		104	-6.363	200.00 400.00	9	36 - 0.301	38 -6.309	24 — 6.307	141 -0.301	136 -0.306	6	45 -0.313	130 -0.305	6		34 -0.307	9	i .
Shaft Frequency,	6.725	ص د	.00	.88 6.65	.00 6.662	.00 6.648	.00 6.648	.00 6.654	9	9	9	6	6.	.	9	9	90	.00 6.652	.00 6.658	.00 6.646	6.654	90.	8.	9	.	ю	6	.06 6.430	.16	5. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	100		90	40.	.6.4	9.9	6.4	96	6.4	9.9	6	65.4	4.6	7 8	5
Advance Shaft ratio angle,	0.450 -14.00		6.500	0.502 -2	0.501 -2	0.505	0.503	6 .5006			0.501 -8.06	_				_	0.550 0.0	9 .552 –2	0.550 -2	6 .551 -4	0.550		_			●.553 -10.0		0.042	6.642	6.642	6.640	9.04		0.043		6.642	0.045	0.046	9.048	0.0482	9.048	9-9-8	0.045	476 6	242
Rotor speed,	1666,78	1666.78	1000.66	999.49	1000.20	999.14	999.14	96.666	1000.31	1000.66	96.666	999.61	999.38	1000.08	1666.98	1001.48	1661.37	999.61	999.84	999.14	999.84	999.84	998.67	1001.37	1000.43	1000.43	1000.78	989.23	999.57	1662.61	1000	0/.088	1 000 1 000	1000.04	60.00	1666.27	10.000	1000.62	1001	59 555	1000	1000	54 666	02.000	
Collective pitch, deg	6	9.0	0.0	9 . 9	0 .0	0.0	0.0	0.0	0 .0	9 . 9	9 . 9	9. •	9 .	9. 9	9 .	6 .0	.	0.0	.	•.	.	6 .0	.	.	•.	9 .0	9 .0	Ø.6	9 (P	9 (10)	9 6	9 6	9 6	9 69 69 19) (S)	9 69	9	9 6	9 69	9 6) (S)) (S)) G) (5
Data point number	80065050	82265953	82265054	82265955	82265056	82265057	82265058	82265059	82265060	82265961	82265062	82265963	82265064	82265965	82265066	82265967	82265968	82265069	82265070	82265071	82265072	82265973	82265074	82265975	82265076	82265077	82265078	83244038	83244039	83245882	62249664	03243003 81340008	00000000000000000000000000000000000000	83250009	83250010	83250011	83244040	83244041	83249007	83249008	83249009	83249010	83250012	0106061	
Rotor	-	۰.		-	-	—	-		-	H	-	-	-	-	-	—	-	-	-	-	-	-	-	-	-	-	-	11	II	Ξ:	→ .	: :	; <u>-</u>		:=	: =	=	: =	-		·	: -	: -	: <u>-</u>	_

Domping, 1/sec	-0.304	-6.305	-6 .304	-0.308	-6.303	-0 .298	-0.304	-0.305	-0.308	-6.307	200.00	9.50	9.36	90.00	200.00	9.706	40.00	192.9	9.00	90.0	900	101	200	-6.305	-6.300	-6.299	-0 .293	-0 .295	-9 .289	-6 .288	-0.295	-0.289	-0.297	-6.291	-0 .295	-0.288	-0.286	-0.285	-0.294	-0.294	-0 .302	-0.298	-0.293	-0 .293	-6 .291
Frequency, Hz	6.426	6.432	6.418	6.426	6.445	6.434	6.424	6.426	6.414	6.441	0.424	0.443	0.44.0	6.432 8.433	6. 122 8. 140	6.4.4 4.24	6. 441	724	474 A	0.10	6.45	8 4 7 8	6.49	6.438	6.432	6.426	6.434	6.449	6.441	6.428	6.432	6.428	6.436	6.426	6.428	6.418	6.443	6.449	6.443	6.447	6.451	6.426	٦.	6.451	6.445
Shaft angle, deg	-3.98	-3.97	16.4	1.01	4.61	4.02	4.02	90.99	9.60	φ. 9. 98	90.90	9.00	90.4) w	999	7.08) (S	70.0	79.67	96.9	9.6	10.01	19.96	-10.01	-10.01	-9.95	-16.60	-16.66	-11.96	-11.96	-14.00	-14.00	-16.04	-16.04	-17.99	-17.99	-20.00	-20.00	90.0	0.05	-2.07	-2.07	-3.96	-3.96	-5.97
Advance ratio	9.046	0.045	0.048	0.049	6.048	0.046	6.045	0.045	9.046	9.946 9.946	9.6	0.04/ 0.04/	9.04	446	9.0	9.040	9.0	6.04	0.047	770	9.045	9 941	946	9.044	0.042	9.046	9.046	6.045	0.044	0.043	0.042	6 .044	0.043	9.044	9.044	6.043	0.044	0.045	0.097	960.0	860.0	660.0	86.0	6.697	6 .698
Rotor speed,	998.88	1000.15	938.76	999.34	1661.68	999.81	998.99	999.11	79.865	1999.27	888.23	000 14	F. 000	70.800 47.800	0000 T	900 46	1000	000	28.85	980.000	1000.27	20 000	1000.15	1000.62	1000.15	939.69	999.81	1001.20	1000.62	999.34	69.66	999.34	1000.04	999.34	999.23	998.53	1000.73	1001.20	1000.04	1000.50	1000.73	998.76	998.53	1001.08	1000.50
Collective pitch, deg	9°.0	3.0	a.0	6.0 0.0	۵. ا	B. 1	9.0 9.0	8 . 8 .	9 (S 6	9 6	9 6) r) F) r) r	9 6		, k) k	9 69) I	9 69	3.0	3.0	0.D	3.0	3.0	3.0	9.0	3.0	g.9	6 .0	3.0	3.0	3.0 0.1	3.0	3.0	3.0	3.0	G.0	3.0	a.0	3.0	a.6
Data point number	83244043	83245003	83249011	83249012	83249013	83230014	83250015	83244044	02244043	02244040	4104040	83249017		83250017	83244947	83245004	83249018	81249828	83249021	81250010	83250020	83244049	83244050	83245005	83245006	83245007	83250022	83250023	83250024	83250025	83250026	83250027	83250028	83250029	83250030	83250031	83250032	83250033	83250034	83250035	83250036	83250037	83250038	83250039	83250040
Rotor	II	II	=:		: :	:	:	7.	h	::	:=	:=	-		<u>-</u>		: ::	: =	-	<u>-</u>	II	II	II	11	11	II	==	II		I	Ξ:	7:	Ξ:	- : - :	Ξ:	Ξ;	Ξ:	Ξ:	Ξ:	-	I	I	:	Ξ:	11

Advance Shaft Frequency, nation angle, deg Hz ratio angle, deg Hz ratio angle, deg Hz ratio angle, deg Hz hz begge -7.96 6.434 6.632 6.693 -7.96 6.434 6.693 -7.96 6.434 6.693 -12.07 -9.95 6.434 6.434 6.693 -12.07 -9.95 6.434 6.434 6.693 -14.04 6.425 6.434 6.693 -14.04 6.425 6.434 6.693 -14.04 6.425 6.434 6.425 6.434 6.425 6.434 6.425 6.434 6.425 6.434 6.434 6.425 6.434	Advance Shaft Frequency, December December 6.099 -5.96 6.434 6.434 6.099 -7.96 6.434 6.436 6.099 -7.96 6.436 6.436 6.099 -7.96 6.436 6.436 6.099 -12.08 6.436 6.436 6.099 -12.08 6.436 6.436 6.099 -12.08 6.436 6.441 6.099 -14.09 6.436 6.436 6.099 -17.09 6.436 6.443 6.099 -16.09 -17.09 6.443 6.099 -16.04 6.443 6.443 6.099 -16.04 6.436 6.443 6.099 -16.04 6.436 6.443 6.099 -16.04 6.436 6.443 6.099 -16.04 6.436 6.436 6.099 -16.04 6.436 6.436 6.149 -4.05 6.436 6.436	
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9 100 -19.97 6.416	6.199 –10.02 6.416	

Damping. 1/sec	-0.283	-0.284	-0.274	-0.285 0.285	907.0	27.5	278	-0.278	-0.272	-0.262	-0.263	-0 .252	-0 .228	-0.239	-6.230	-6.233	-0 .228	6 .23 4	-0.227	-0.284	-6 . 289	-6 .297	-6.275	-6.279	-6.284	-6.2/2	•	6.273	107.0	976	-6.218	-0.226	-0.226	-0.229	-0 .230	-0 .238	-0.229	-0 .233	-0.231	-0 .260	-0.270		•	-0.239
Frequency,	6.424	6.426	6.443	6.443	47t-0	6.430	6.441	•	6.441	6.430	6.441	6.438	6.440	6.432	6.434	6.436	6.438	6.440	6.440	6.434	6.443	•	6.416	6.426	6.433	6.432	6.426	0.45e	0.440	424	6.434	6.440	6.430	6.434	6.440	6.447	6.441	6.443	6.434	6.418	6.420	6.422	6.424	6.436
Shaft angle, deg	-10.02	-11.99	-11.99	11.99	20.67	-12.63		-13.96	-13.96	-16.00	-16.00	-16.00	-18.01	-18.00	-18.01	-18.01	-20.00	-20.00	-20.00	-8.07	8.00	8. 8.	-10.63	-10.00	90	~ (-12.00	Ν,	14.00	۲,	9	ဖ	-16.00	-18.00	-18.00	-18.00	-20.00	-20.00	-20.00	-10.00	-10.00	-10.00	•	-12.00
Advance ratio	9.200	0.200	6 . 199	9 .200	n 0	6. 180 197		6.197	9.196	•	6.199	6 .198	6.197	0.201	6 . 199	0.198	6.199	9.198	0.198	0.248	0.249	0.250	0.249	0.250	0.250	0.250	0.250	9.228	9.729 9.759	9.236	9.259	0.250	0.250	0.250	0.250	0.250	0.250	0.250	0.250	0.300	0.300	0.300	0.300	0.300
Rotor speed,	999.57	999.57	1000.85	1000.73	4000	1000.04	1901 20	1661.32	1001.32	1000.27	1001.32	1001.08	1000.97	1000.15	1000.39	1000.39	1000.39	1000.73	1000.62	1000.04	1000.62	999.92	998.76	1000.00	1000.00	1999.99	1000.00	1999.99	1909.99	90001	1000	1000.00	1000.00	1000.00	1606.60	1000.00	1000.00	1000.00	1000.00	1000.00	1000.00	1000.00	1000.00	1000.00
Collective pitch, deg	3.0	3.0	3.0	ю. Р) H	9 G) (c)	9 6	9.0	3.0	3.0	J.0	J.0	3.0	0.0	3.0	6 :	a.0	3.0	3.0	J.0	ы. Ө.	 9.	0.0 0.0	o. 0	 8.	o. 1	۵. و. و	9 6	9.6	9 6	9	3.0	9.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	J.0	a.0	3.0
Data point number	83252009	83251038	83251039	83251040	63232616	83252012	83252013	83252014	83252015	83252016	83252017	83252018	83252019	83252020	83252021	83252022	83252023	83252024	83252025	83252026	83252027	83252028	83252029	83252030	83252031	83252032	83252033	83252834	63232633	0070700	83252838	83252039	83252040	83252041	83252042	83252043	83252044	83252045	83252046	83252047	83252048	83252049	83252056	83252050
Rotor	11	I	II	H I	7 -	11	: =	II	II	II	II	I	II	H	I	H	I	II	11	H	I	I	Π;	Ξ:	Ξ:	Ξ;	=:	- :		<u> </u>		Π	II	11	11	11	11	11	11	II	.	=	II	II

Domping. 1/sec		-0.235	-0.236	-0.239	6 .228	9 .21 4	-0.270	6.213	-0.211	4.22/	97.79	28.6	194	-0.204	-0.247	-9.246	-0.249	-0.202	-0.212	-0.202	-6.198	50 F	4 2 2	6.179	-0.173	-0.692	-6.663	69.688 69.688	760.0	-6.717	9.714	-0.703	-0.685	-6.693	-9.6 62	9.676	-9.667	-9.788	-0.586	9.719	-8.716	97.75	-0.724
Frequency, Hz		6.434	6.441	6.420	6.426	6.440	6.426	6.438	6.436	6.434	6.434	6. 445 6. 445	6.441	6.441	6.422	6.432	6.438	6.434	6.432	6.441	6.438	6.428	A 433	6.432	6.438	6.453	6.461	6.457	0.44/	6.478	6.465	6.459	6.455	6.443	6.455	6.463	6.449	6.457	6.453	6.447	6.441	6.441	6.457
Shaft angle, deg	ı	-12.00	-12.00	-12.00	-14.00	-14.00	-14.00	-14.00	14.99	-16.66	- 15.96 8.35 8.88	0.01 0.01	20.00	-18.90	-16.99	-16.66	-10.99	-12.00	-12.00	-12.00	-14.98	- 14.00 - 4.00 - 4.00		16.98	-16.00	-2.00	-5.88	26.5	79.4	4 4	76.7-	-7.96	-10.00	-10.00	-12.00	-13.97	-13.96	-16.99	-16.00	-18.65	-18.05	-20.66	-20 00
Advance ratio		9.300	9.388	9.300	9.300	9.366	0.300	0.300	9.300	9.300	9.386	9 . 305.	9	9.300	9.350	0.350	0.350	9.358	0.350	0.350	0.350	9.30	9.336 8.55	9.358	9.350	0.046	0.041	0.044	6.640	9.64/ 9.41	9.046	0.043	0.042	0.044	0.043	0.045	0.045	0.044	0.045	9.046	0.046	0.045	270
Rotor speed, rpm		1000.00	1000.00	1000.00	1000.00	1000.00	1999.99	1909.90	1666.66	1666.66	1909.99	1909 . 000 t	1000.000	1666.66	1000.00	1000.00	1000.00	1969.99	1000.00	1000.00	1000.00	1909.99	0000	1886.88	1000.00	999.11	1000.04	999.57	200 . 000 000 . 000	1991.07	1888.15	93.68	999.34	998.41	999.81	1666.39	999.34	999.92	999.57	999.11	998.76	998.65	200 A 1
Collective pitch, deg		3.0	9.0 9.0	3.0	က စ	3.0	3.0	0.0 0	ю. О	9 (? (9 G	9 6) m	9	9.0	3.0	3.0	3.0	G.0	0.0	ю. В.	5) P) e	9 69	ю. Ю.	6.9	6.0	φ. Θ. α	9 G	9 G	9 6	9.9	6.0	6.6	6.0	6.0	6 .0	0 .0	9 .0	Ø.	Ø.0		S C
Data point number	,	83252051	83252052	83252057	83252053	83252058	83252058	83252059	83252060	83252861	83252062	81057064	83252065	83252066	83252967	83252068	83252070	83252071	83252072	83252073	83252074	832520/5	07222070 84757877	83252078	83252079	83259051	83259052	83259053	83239834	83239855	83259057	83259058	83259059	83259060	83259061	83259063	83259064	83259065	83259066	83259067	83259068	83259069	81250B7B
Rotor		II	II	11	II	II	:	=		:	= :		4 F-	: =		II	II	11	II	II	Ξ:	-	::	1 1	II	11	II	— ;	3:	h	-		II	II	II	II	II	I	II		II:	I	

Domping, 1/sec	-0.663 -0.676 -0.668 -0.678 -0.678 -0.689 -0.689
Frequency, Hz	6.445 6.445 6.445 6.438 6.453 6.453 6.453
Shaft angle, deg	16.04 - 18.04 - 20.00 - 20.00 - 17.98 - 20.00 - 20.00
Advance	0.095 0.096 0.097 0.097 0.151 0.147 0.148
Rotor speed, rpm	998.99 998.36 999.81 998.76 1000.39 1000.27 999.57
Collective pitch, deg	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
Data point number	83259072 83259073 83259074 83259075 83259076 83259077 83259078 83259079
Rotor	

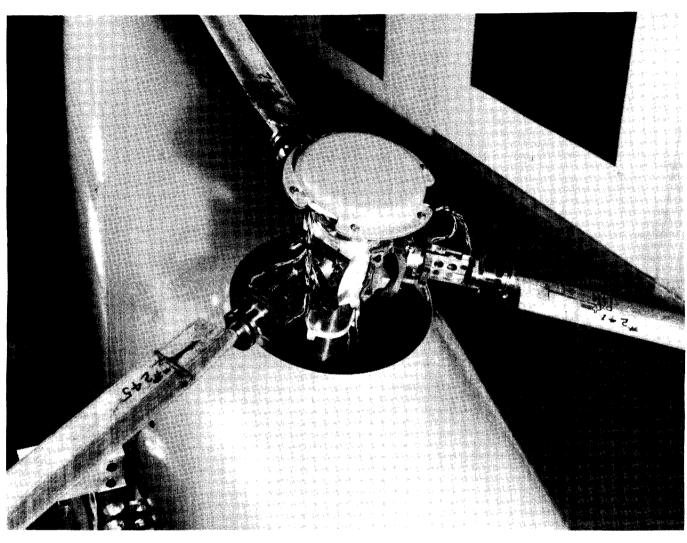


Figure 1.-Model hub and blades.

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BLACK AND WHITE PHOTOSPAPH

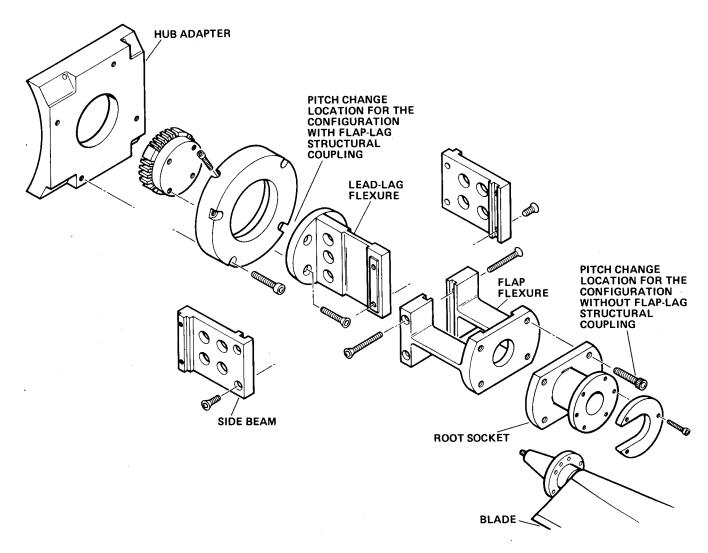


Figure 2.-Exploded view of blade and flexure assembly.

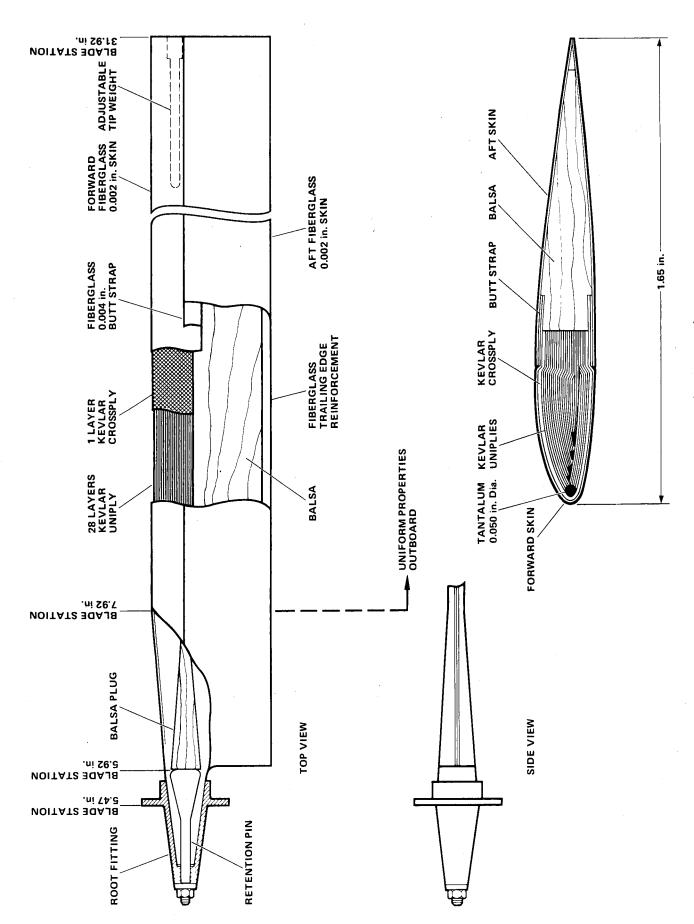


Figure 3.-Rotor blade planform and cross section.

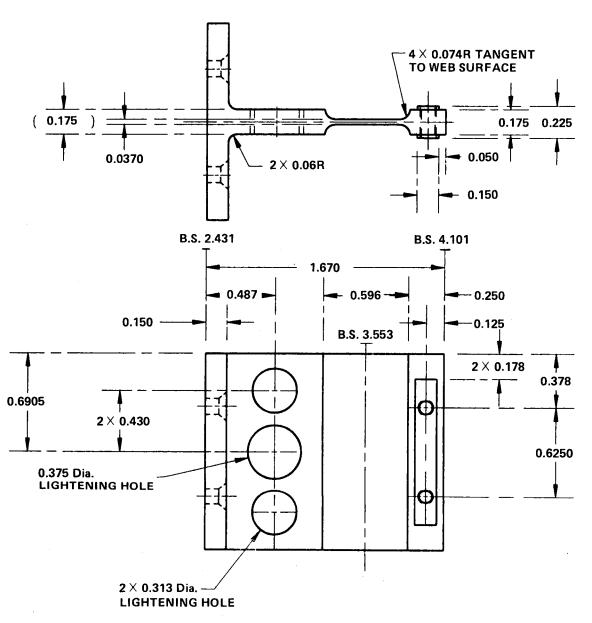


Figure 4.-Lead-lag flexure; 17-4PH H900 steel; dimensions in inches.

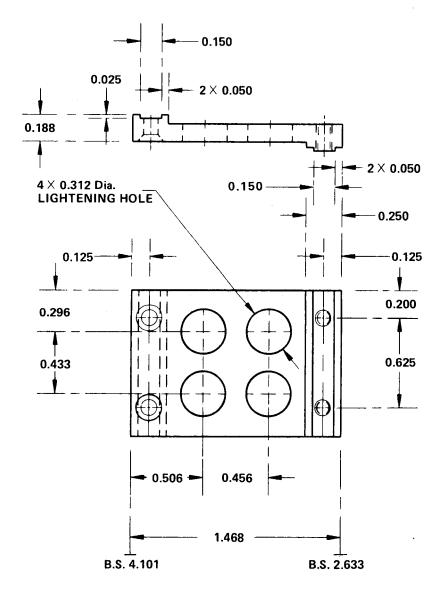


Figure 5.-Side beam; TI-6AL-4V titanium; dimensions in inches.

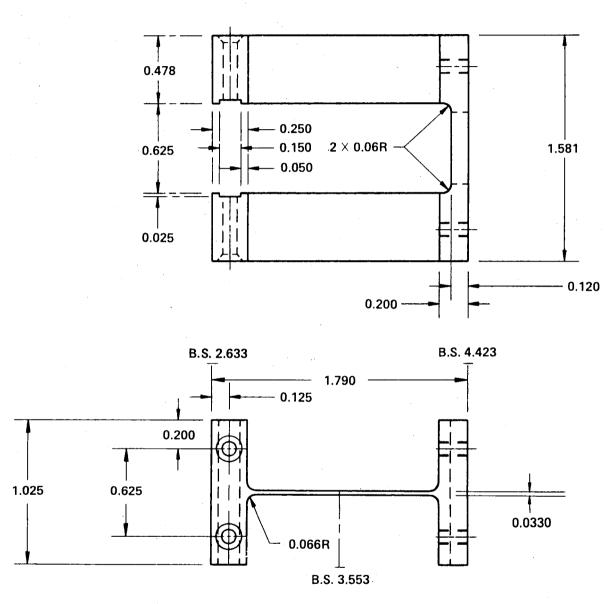


Figure 6.-Flap flexure; 17-4PH H900 steel; dimensions in inches.

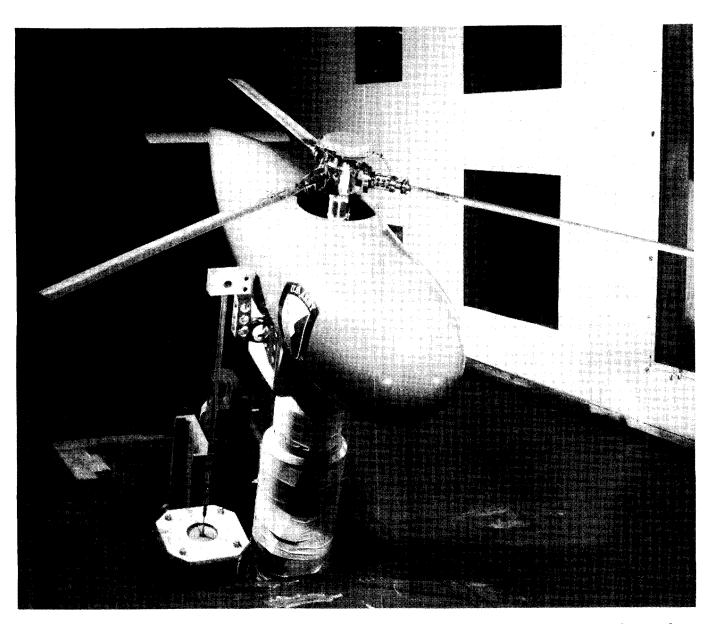
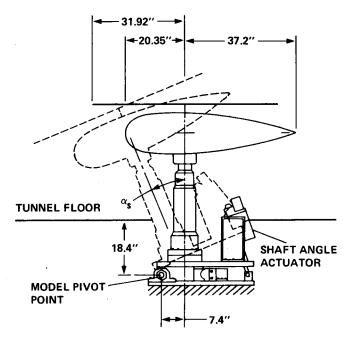
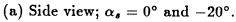
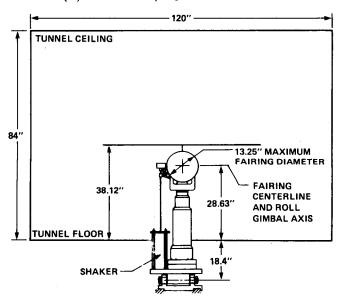


Figure 7.–Model installed in the Aeroflight dynamics Directorate's 7– by 10–foot wind tunnel test section.

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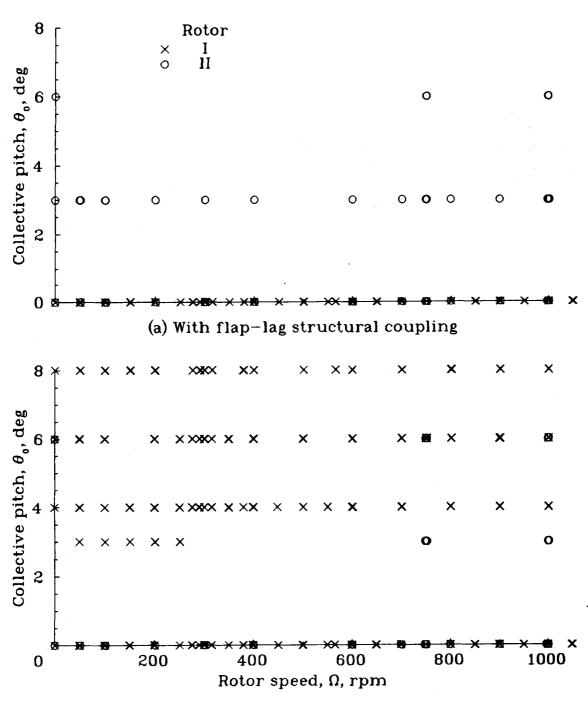






(b) Front view; $\alpha_s = 0^{\circ}$.

Figure 8.-Installation diagram of the model in the Aeroflightdynamics Directorate's 7- by 10-foot wind tunnel test section.



(b) Without flap-lag structural coupling
Figure 9.-Hover test points.

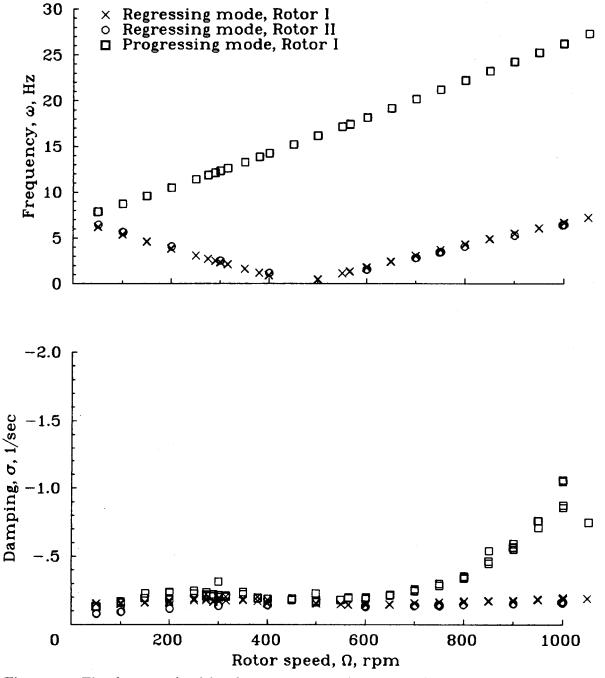


Figure 10.—Fixed system lead-lag frequencies and damping values versus rotor speed in hover; $\theta_0 = 0^{\circ}$.

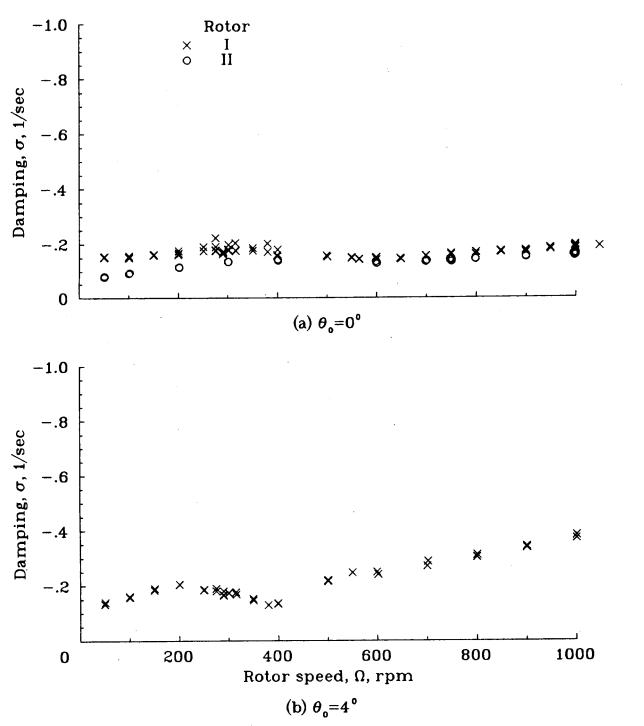


Figure 11.-Lead-lag regressing mode damping versus rotor speed in hover; configuration without flap-lag structural coupling.

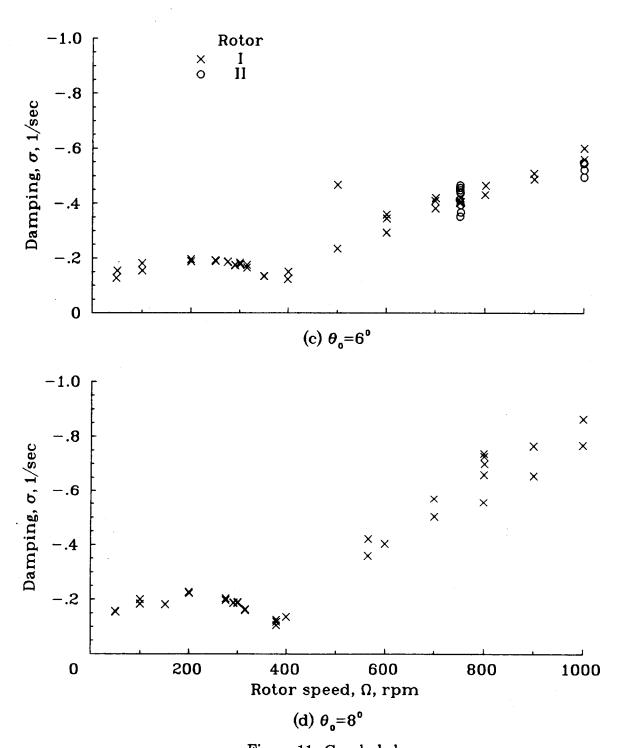


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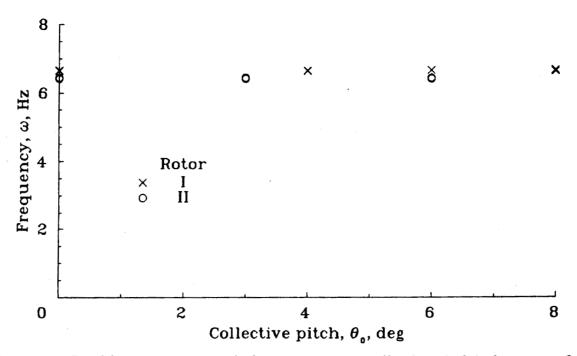
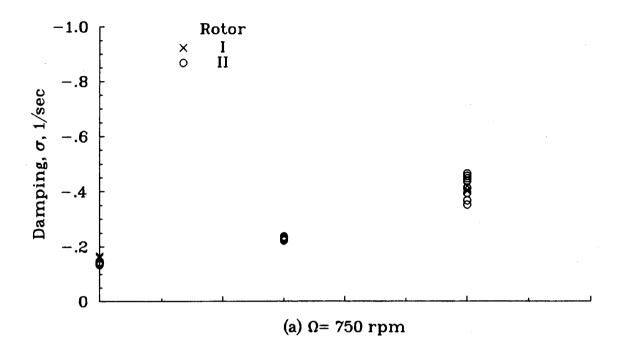


Figure 12.—Lead-lag regressing mode frequency versus collective pitch in hover; configuration without flap-lag structural coupling; 1000 rpm.



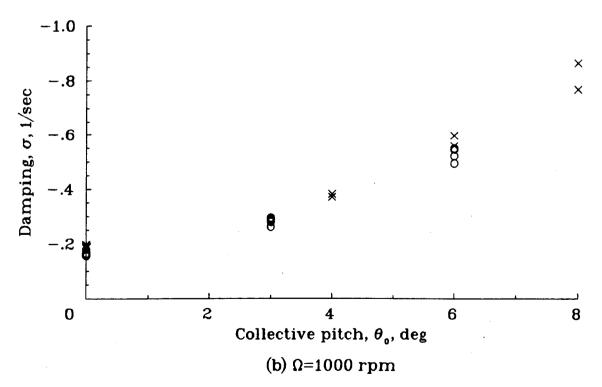
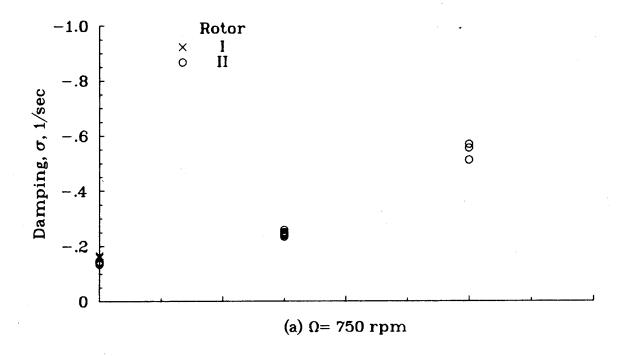


Figure 13.—Lead-lag regressing mode damping versus collective pitch in hover; configuration without flap-lag structural coupling.



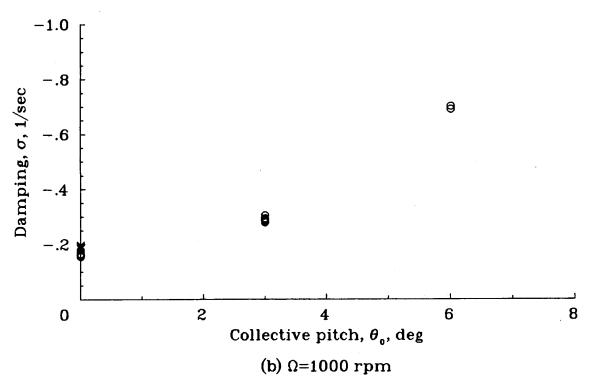


Figure 14.—Lead-lag regressing mode damping versus collective pitch in hover; configuration with flap-lag structural coupling.

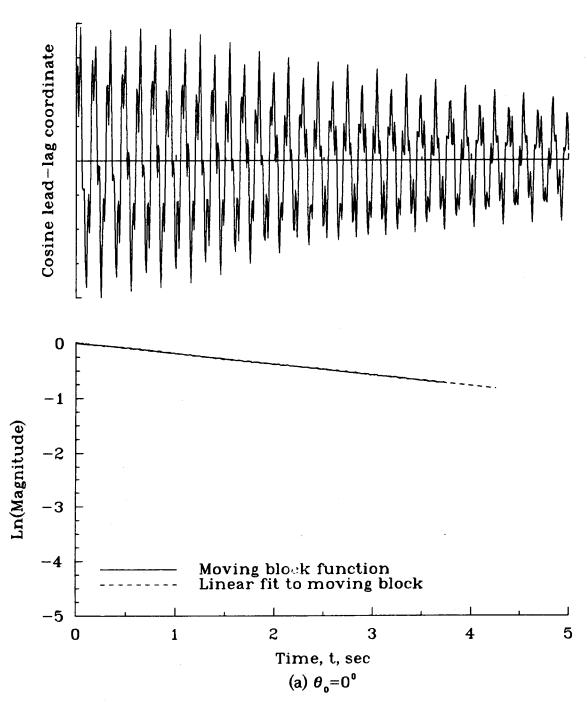


Figure 15.—Representative transient time histories in hover and their moving-block functions at the regressing lead-lag mode frequency; configuration without flap-lag structural coupling.

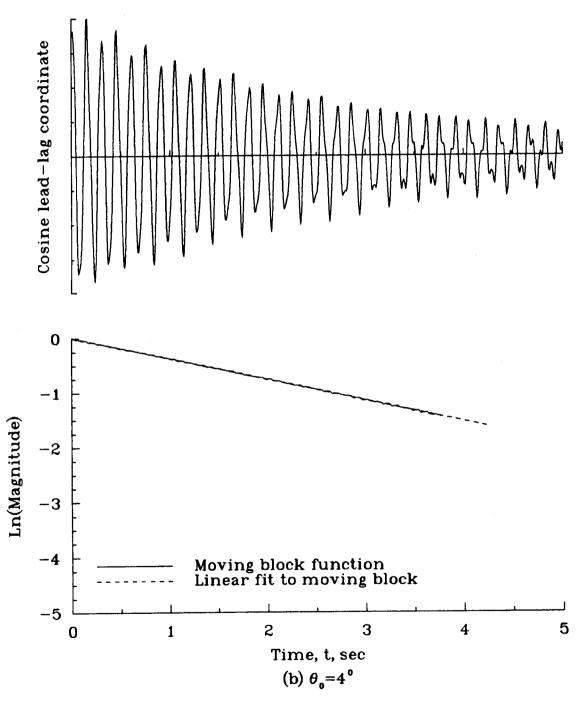


Figure 15.-Continued.

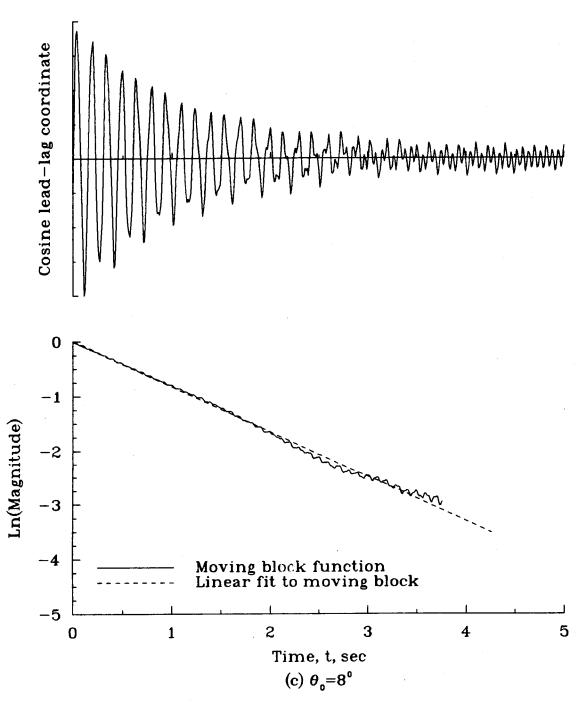


Figure 15.-Concluded.

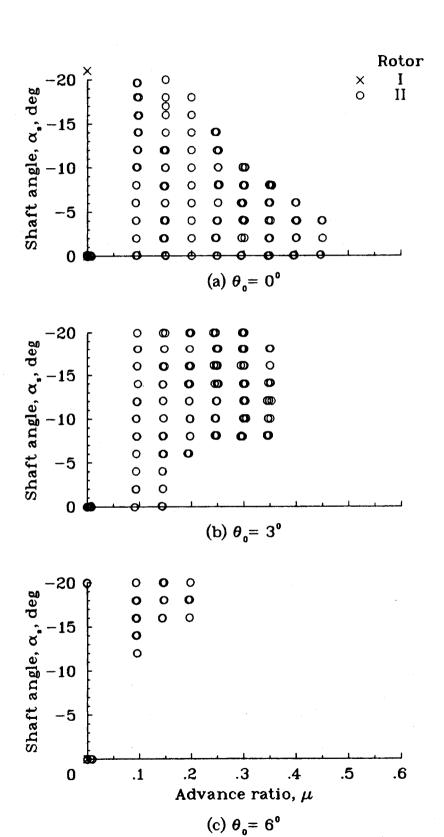


Figure 16.-Advance ratio, shaft angle, and collective pitch conditions tested at 750 rpm for the configuration without flap-lag structural coupling.

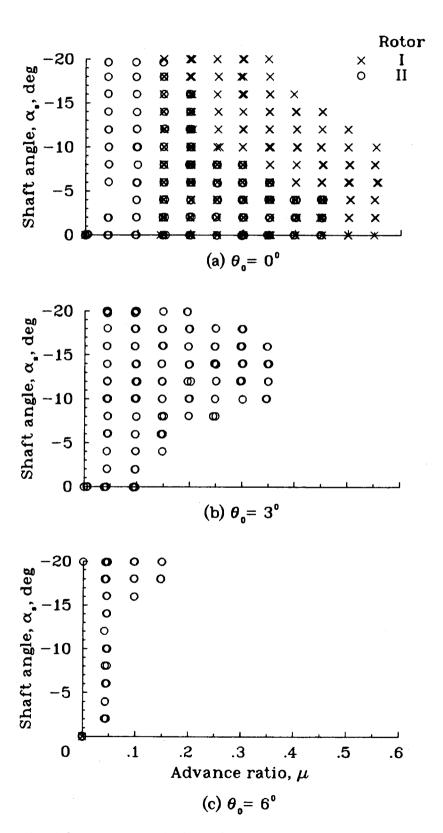


Figure 17.-Advance ratio, shaft angle, and collective pitch conditions tested at 1000 rpm for the configuration without flap-lag structural coupling.

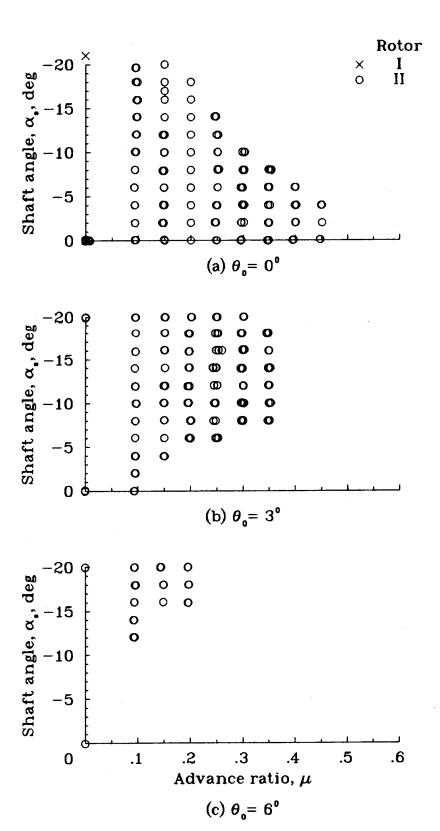


Figure 18.-Advance ratio, shaft angle, and collective pitch conditions tested at 750 rpm for the configuration with flap-lag structural coupling.

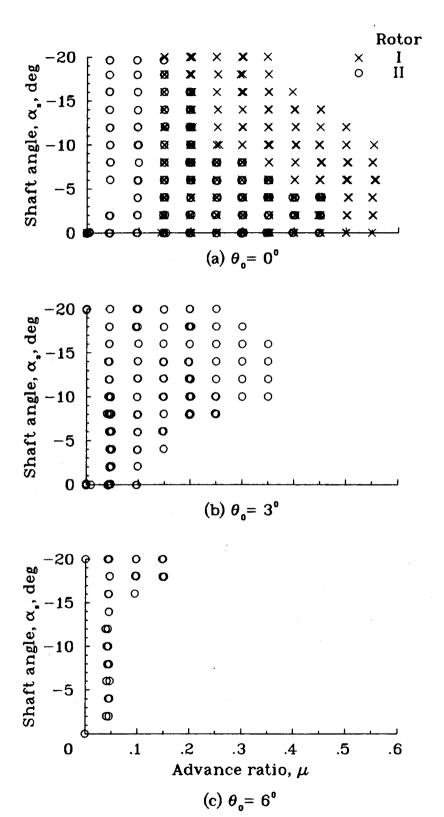


Figure 19.-Advance ratio, shaft angle, and collective pitch conditions tested at 1000 rpm for the configuration with flap-lag structural coupling.

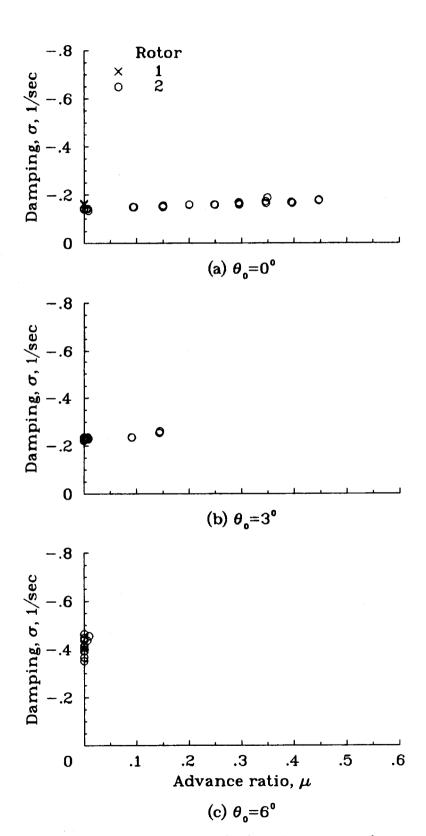


Figure 20.–Regressing lead-lag mode damping versus advance ratio; configuration without structural flap-lag coupling; 750 rpm, $\alpha_s=0^\circ$.

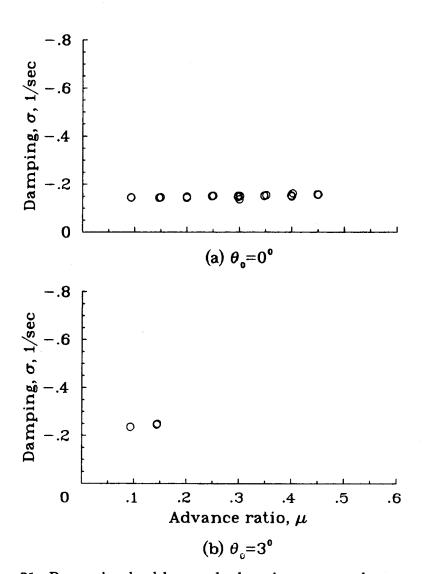


Figure 21.–Regressing lead-lag mode dataping versus advance ratio; configuration without structural flap-lag coupling; 750 rpm, $\alpha_s = -4^{\circ}$.

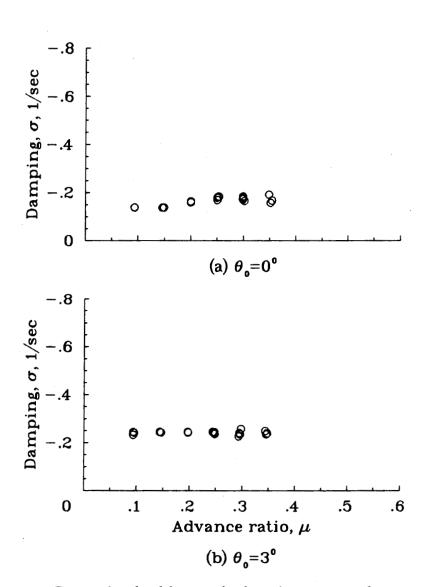


Figure 22.-Regressing lead-lag mode damping versus advance ratio; configuration without structural flap-lag coupling; 750 rpm, $\alpha_s = -8^{\circ}$.

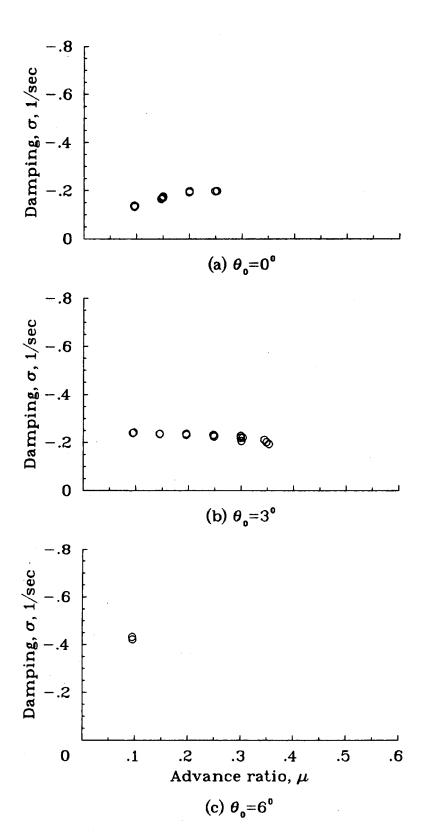


Figure 23.-Regressing lead-lag mode damping versus advance ratio; configuration without structural flap-lag coupling; 750 rpm, $\alpha_s = -12^{\circ}$.

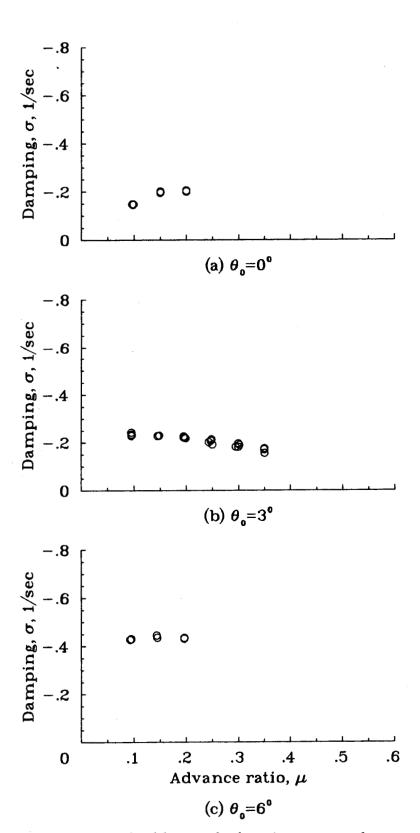


Figure 24.–Regressing lead-lag mode damping versus advance ratio; configuration without structural flap-lag coupling; 750 rpm, $\alpha_s = -16^{\circ}$.

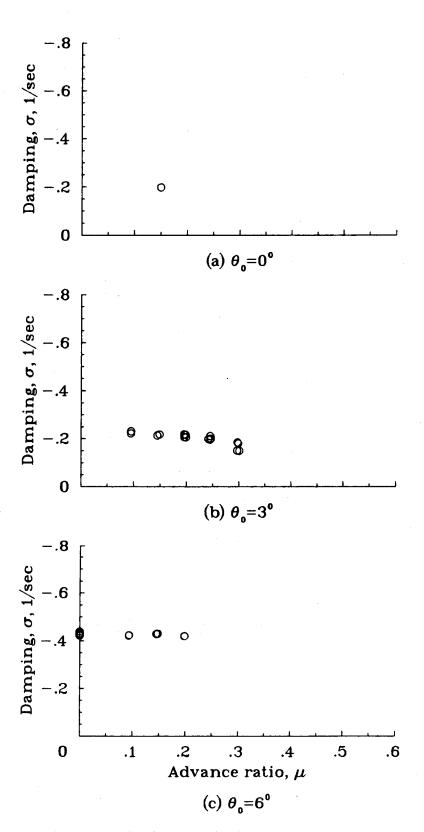


Figure 25.-Regressing lead-lag mode damping versus advance ratio; configuration without structural flap-lag coupling; 750 rpm, $\alpha_s = -20^{\circ}$.

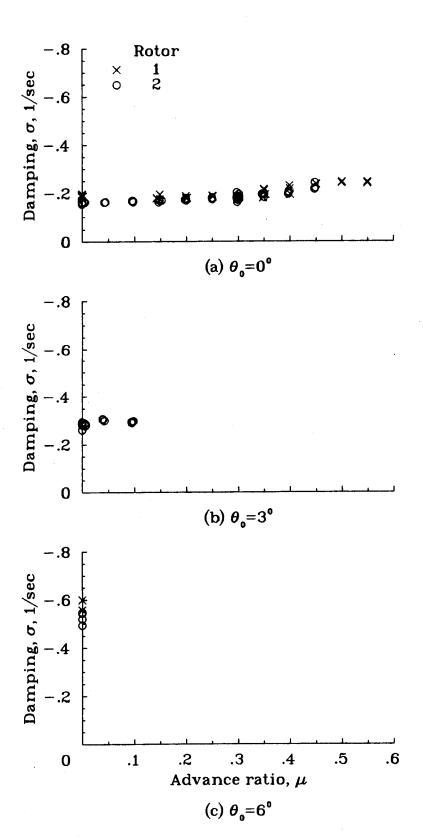


Figure 26.–Regressing lead-lag mode damping versus advance ratio; configuration without structural flap-lag coupling; 1000 rpm, $\alpha_s=0^{\circ}$.

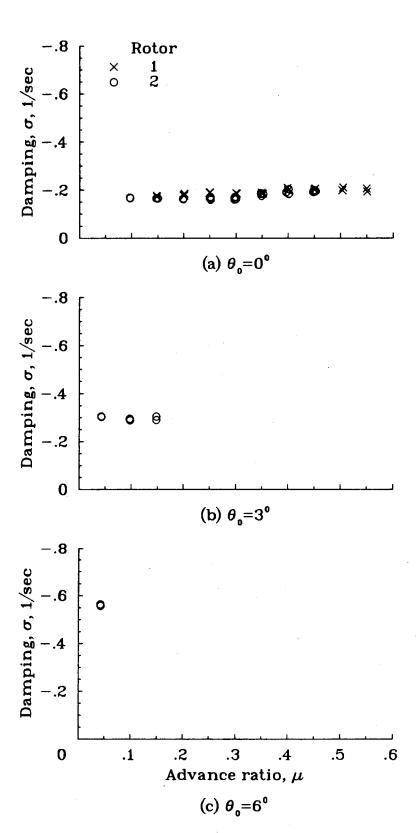


Figure 27.-Regressing lead-lag mode damping versus advance ratio; configuration without structural flap-lag coupling; 1000 rpm, $\alpha_s = -4^{\circ}$.

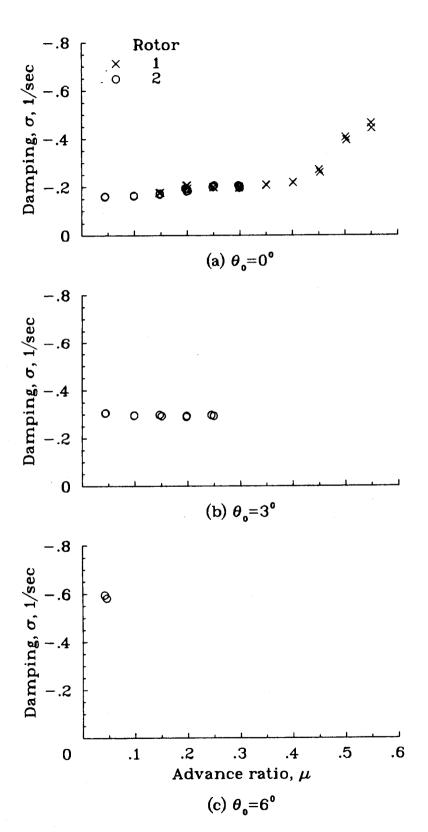


Figure 28.–Regressing lead-lag mode damping versus advance ratio; configuration without structural flap-lag coupling; 1000 rpm, $\alpha_s = -8^{\circ}$.

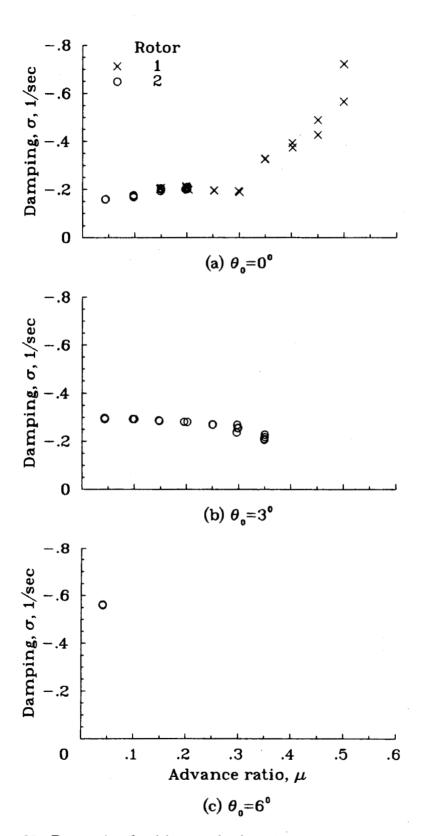


Figure 29.-Regressing lead-lag mode damping versus advance ratio; configuration without structural flap-lag coupling; 1000 rpm, $\alpha_s = -12^{\circ}$.

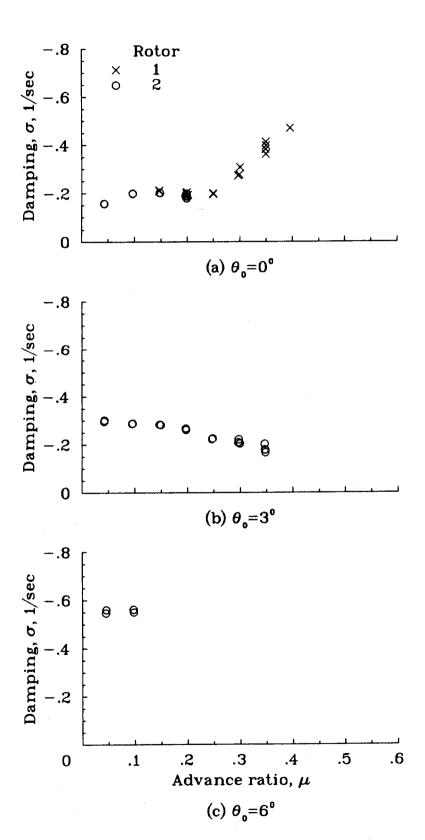


Figure 30.–Regressing lead-lag mode damping versus advance ratio; configuration without structural flap-lag coupling; 1000 rpm, $\alpha_s = -16^{\circ}$.

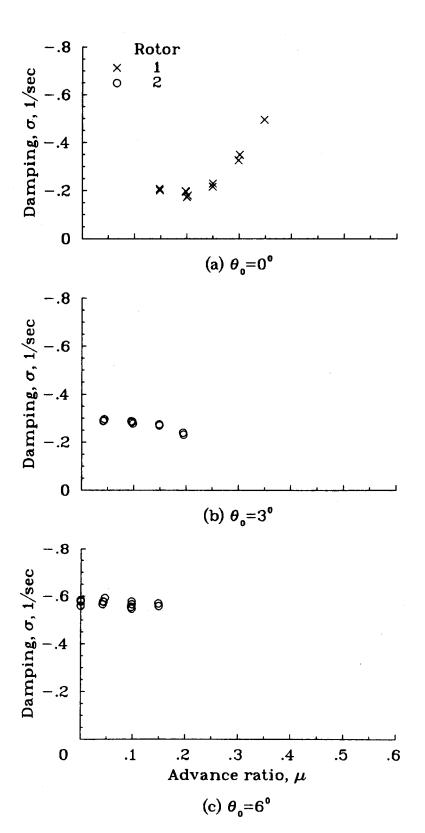


Figure 31.-Regressing lead-lag mode damping versus advance ratio; configuration without structural flap-lag coupling; 1000 rpm, $\alpha_s = -20^{\circ}$.

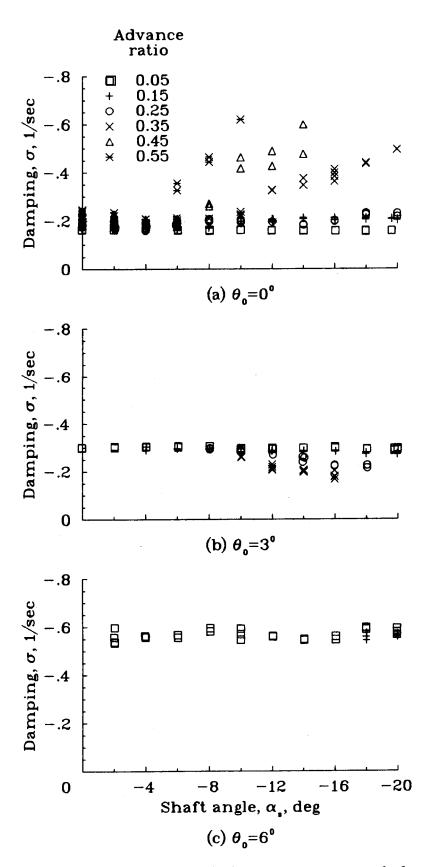


Figure 32.—Regressing lead-lag mode damping versus rotor shaft angle; configuration without structural flap-lag coupling; ; 1000 rpm; both Rotor I and Rotor II data are included without distinction.

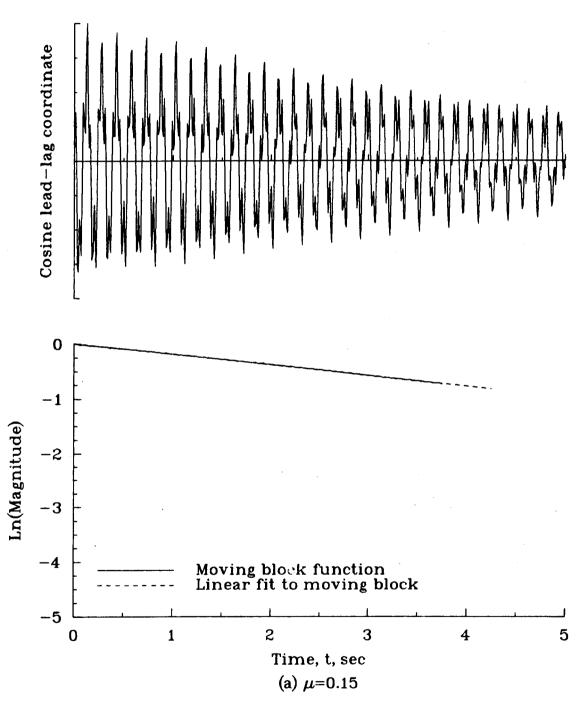


Figure 33.–Representative transient time histories in forward flight and their moving-block functions at the regressing lead-lag mode frequency; configuration without flap-lag structural coupling; $\theta_0 = 0^{\circ}$, 1000 rpm, $\alpha_s = 0^{\circ}$.

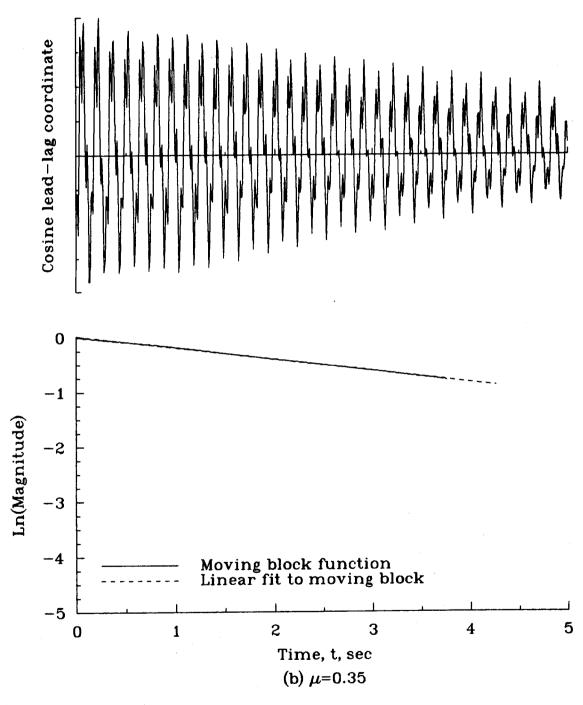


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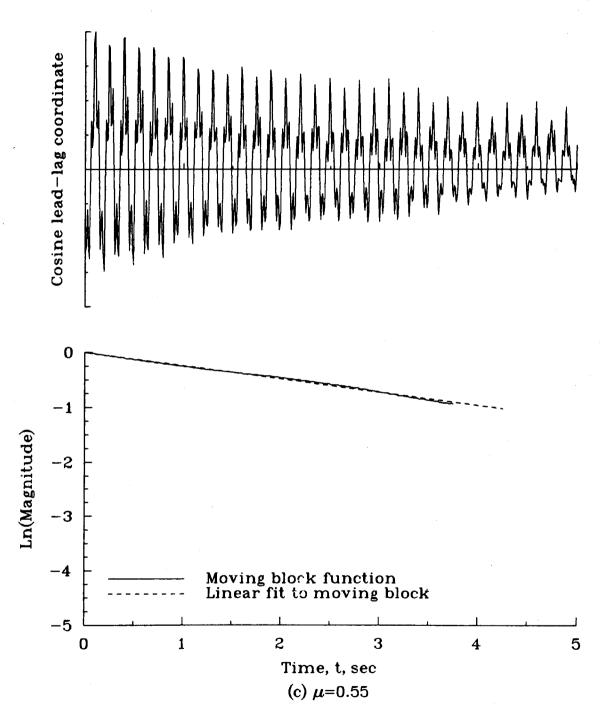


Figure 33.-Concluded.

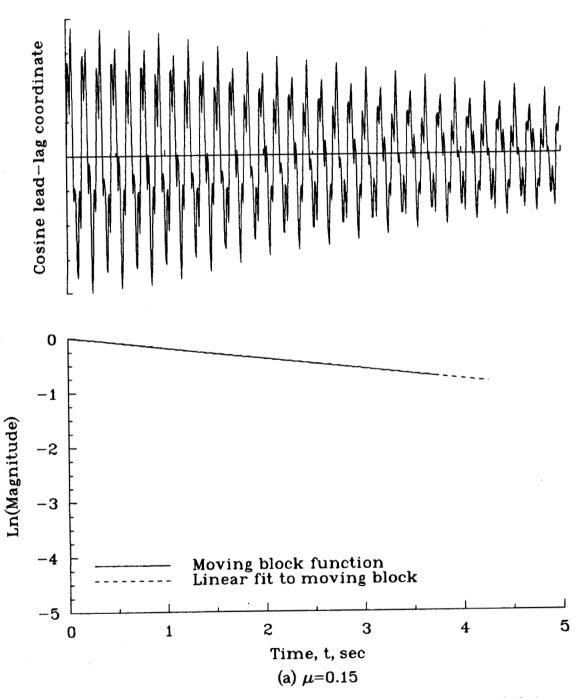


Figure 34.–Representative transient time histories in forward flight and their moving-block functions at the regressing lead-lag mode frequency; configuration without flap-lag structural coupling; $\theta_0 = 0^{\circ}$, 1000 rpm, $\alpha_s = -10^{\circ}$.

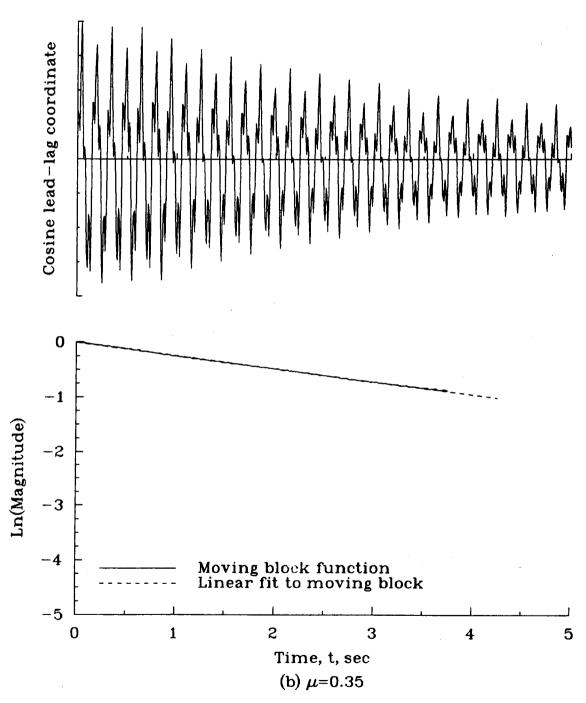


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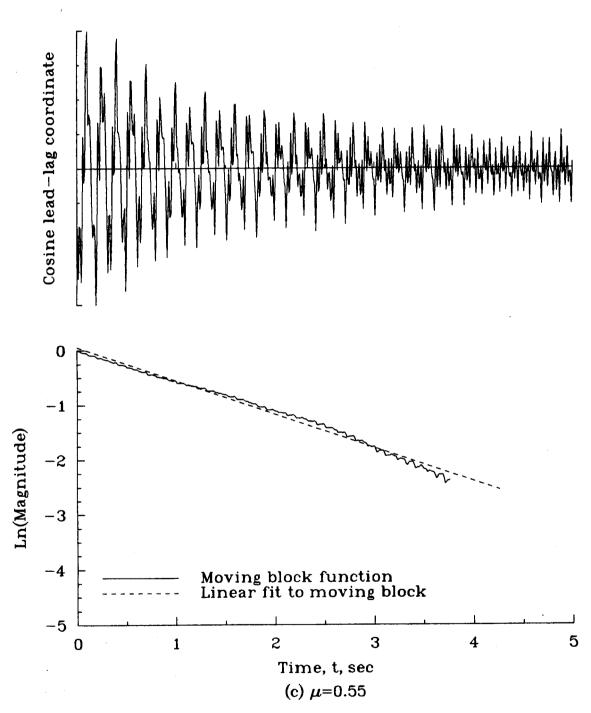


Figure 34.-Concluded.

National Aeronautics and Soace Administration	Report Documentation P	age
1. Report No. USAAVSCOM TR 89-A NASA TM-102189	2. Government Accession No.	3. Recipient's Catalog No.
4. Title and Subtitle		5. Report Date
Flan-Lag Stability Data	for a Small-Scale Isolated Hingeless	April 1989
Rotor in Forward Fligh		6. Performing Organization Code
7. Author(s)		8. Performing Organization Report No.
Michael J. McNulty*		A-89124
•		10. Work Unit No.
O Bodomina Organization No.	o and Address	992-21-01
	e and Address , Moffett Field, CA 94035 and	11. Contract or Grant No.
	Directorate, U.S. Army Aviation ogy Activity, Ames Research Center	
Moffett Field, CA 940		13. Type of Report and Period Covered
2. Sponsoring Agency Name an	d Address	Technical Memorandum
National Aeronautics at Washington, DC 2054	nd Space Administration 6-0001	14. Sponsoring Agency Code
15. Supplementary Notes		
	nael J. McNulty, Ames Research Center, Mett Field, CA 94035 (415) 694-5831 or F	
6. Abstract		
was tested in the Aero the test was to determine ration in forward flight untrimmed at several cas high as 0.55. Two is ration both with and was also conducted.	ess rotor with discrete flap and lead-lag fleflightdynamics Directorate's 7- by 10-Foote experimentally the lead-lag stability of a c. The model tested had no cyclic pitch co ollective pitch angles, at shaft angles from nplane natural frequencies, 0.61/rev and (athout structural flat lag coupling. Conco Representative plots of the frequency and complete tabular data and model prope	ot Wind Tunnel. The purpose of structurally simple rotor configu- ontrol, and was therefore operated of 0° to -20°, and at advance ratios 0.72/rev, were tested for configu- mitant hover testing of the model d damping data are presented to
use in detailed correlat abrupt increase in dam with high flapping load results for hingeless ro	ion exercises. The most prominent feature ping with advance ratio at certain high-sples. The hover data are consistent with previors without kinematic couplings. Overall, to be useful in the development and validation	re of the forward flight data is an beed, high shaft-angle conditions, vious experimental and theoretical, the data quality is very good and

analyses.

17. Key Words (Suggested by Author(s))

Hingeless rotor stability
Helicopter model testing
Helicopter aeroelastic stability
Forward flight, Advance ratio

18. Distribution Statement

Unclassified-Unlimited

Subject Category – 39

19. Security Classif. (of this report)	20. Security Classif. (of this page)	21. No. of pages	22. Price
Unclassified	Unclassified	118	A06